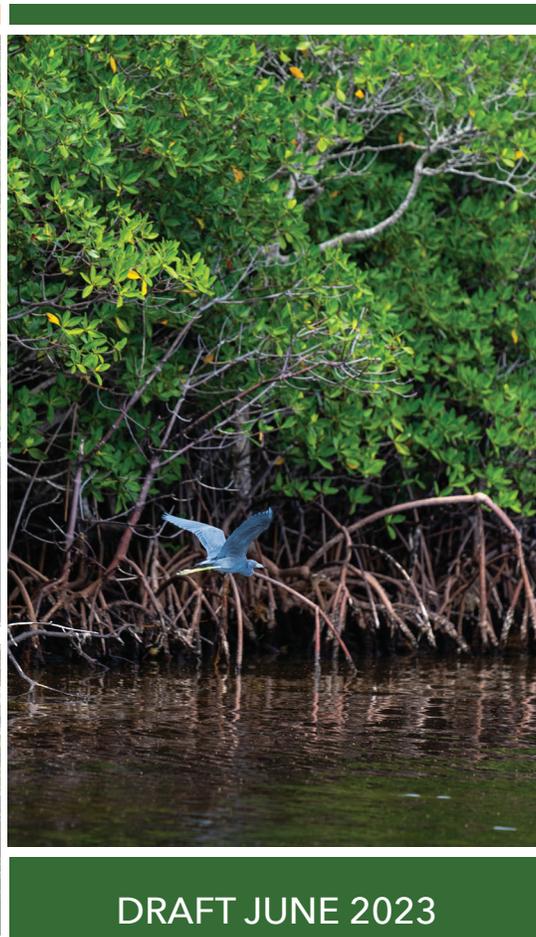




2023 SEA LEVEL RISE AND FLOOD RESILIENCY PLAN



DRAFT JUNE 2023

Building Resilience and Mitigating Risks
to South Florida's Water Resources

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34

Executive Summary

35

36 The South Florida Water Management District (District or SFWMD) is strongly committed to
37 continuing to address the impacts of land development, population growth, and climate change on water
38 resources. Climate change impacts include sea-level rise (SLR), changing rainfall patterns, and
39 evapotranspiration trends. As a regional government agency, SFWMD is responsible for managing water
40 resources in the southern half of the Florida, covering 16 counties from Orlando to the Florida Keys and
41 serving a population of 9 million residents. The District is dedicated to working with our local, state, and
42 federal partners to ensure we provide the best available science-backed data to inform decision making
43 throughout our region. As a key part of the resiliency strategy, the District evaluates the status of its flood
44 control infrastructure, water supply operations and ongoing ecosystem restoration efforts, and advances
45 projects necessary to continue providing flood control, water supply, and ecosystem restoration in
46 anticipation of future climate conditions. In coordination with the Florida Department of Environmental
47 Protection, other State and Federal Agencies, and local governments, the District is making infrastructure
48 adaptation investments that are needed to continue to successfully implement its mission.

49 This plan, which is updated annually, is the first District initiative to compile a comprehensive list of
50 priority resiliency projects with the goal of reducing the risks of flooding, SLR and other climate impacts on
51 water resources and increasing community and ecosystem resiliency in South Florida. This goal will be
52 achieved by updating and enhancing water management infrastructure throughout the Central & South
53 Florida (C&SF) Flood Control System and the Big Cypress Basin and implementing effective, resilient,
54 integrated basin-wide solutions. This list of projects was compiled based upon vulnerability assessments that
55 have been ongoing for the past decade. These assessments utilize extensive data observations and robust
56 technical hydrologic and hydraulic model simulations to characterize current and future conditions, and
57 associated risks.

58 The District's Flood Protection Level of Service (FPLOS) Program has been advancing integrated
59 modeling efforts in critical basins to aid in understanding flood vulnerabilities within the C&SF System and
60 identifying cost-effective implementation strategies to assure that each basin can maintain its designated flood
61 protection level of service under current and projected conditions. In addition, the District's Capital
62 Improvement Plan (CIP) has been incorporating climate change and SLR considerations into the design of
63 critical infrastructure projects. The FPLOS and CIP Programs have been successful at identifying critical
64 resiliency investments that are now being organized and expanded in this document.

65 The list of priority resiliency projects includes investments needed to increase the resiliency of the
66 C&SF System, and Big Cypress Basin flood control infrastructure. These projects represent urgent actions
67 that are necessary to address the vulnerability of the existing infrastructure, including structure
68 enhancement recommendations and other SLR adaptation needs. Project recommendations also comprise
69 basin-wide flood adaptation strategies that are based upon other FPLOS recommendations, and water
70 supply and water resources of the State protection efforts. These projects include adding "self-preservation
71 mode" function to water control structures, enhancing the C-9 canal, construction of the South Miami-Dade
72 Curtain Wall, L31E Levee improvements, and the JW Corbett Wildlife Management Area Hydrologic
73 Restoration and Levee Resiliency project. Each of these projects help to increase the functionality and
74 capacity of the District's flood control and water supply systems and protection of the environment. The
75 Everglades Mangrove Migration Assessment Pilot Study is being proposed to capture the adaptive
76 foundational resilience of the coastal wetlands within the District, and to demonstrate the ability of coastal
77 wetlands to adapt to rising sea levels via enhanced soil elevation change. Additionally, renewable energy

RESILIENCY ACTIONS BEING PROPOSED IN THIS DOCUMENT INCLUDE BUT ARE NOT LIMITED TO THE FOLLOWING:

- Adapt infrastructure to current and future conditions
- Improve canal conveyance, drainage, and inter-basin interconnectivity
- Increase locally distributed and regional storage and infiltration options
- Build situationally appropriate infrastructure (seepage walls, flood barriers)
- Implement “self-preservation” to increase operational capacity and flexibility
- Enhance coastal wetlands and other ecosystem services
- Maximize the integration of green infrastructure and nature-based solutions
- Utilize sustainable energy sources for district facilities and projects
- Continue to expand planning efforts, including H&H modeling, data analysis, monitoring of changing observed conditions and future projections

78 projects are proposed in this plan to help offset new and existing energy requirements. Finally, critical
79 planning projects are presented to continuously advance vulnerability assessments and scientific data and
80 research to ensure the District's resiliency planning and projects are founded on the best available science.

81 This document includes an updated multicriteria ranking approach that was developed to support the
82 assessment of vulnerable areas in South Florida. This ranking approach includes metrics that help to identify
83 the most critical infrastructure and vulnerable areas, while also considering basin-wide resiliency needs.
84 Cost estimates for each proposed project are presented, as well as recommendations to incorporate
85 sustainable sources of energy and utilize the most efficient designs, using both traditional gray infrastructure
86 improvements and nature-based solutions (NBS). This Plan has been updated in 2023 to include additional
87 resiliency project priorities, strategies for NBS, new sustainable energy options, more details about ongoing
88 ecosystem restoration efforts and associated potential carbon storage, and the latest approach being
89 proposed for development of the water supply vulnerability assessment.

90 The District seeks to implement projects that benefit South Florida's communities and environment by
91 working closely with state, tribal, private, and local governments and taking into consideration the needs
92 of socially vulnerable communities and protected environmental areas. In December 2022, the District
93 began hosting quarterly South Florida Resiliency Coordination Forum meetings to further promote
94 collaboration with local, state, federal and tribal partners on water management initiatives related to
95 resiliency; and to engage partners on assessing the impacts of changing climate conditions and water
96 management implications.

97 The District continues to seek for funding alternatives at the State and Federal levels to help fund
98 implementation of project recommendations included in this plan. At the State level, in May 2021,
99 Governor Ron DeSantis signed Florida Senate Bill 1954 which created the Resilient Florida Program,
100 providing significant funding to support flooding and SLR resiliency projects throughout the State. In May
101 2022, Governor DeSantis approved House Bill 7053 which established further efforts towards Statewide
102 Flooding and Sea Level Rise Resilience. In January 2023, Governor DeSantis signed Executive Order 23-
103 06 to direct funding and strategic action to continue to support the Resilient Florida Program. As part of the
104 Resilient Florida Program, the District is currently working with the Florida Department of Environmental
105 Protection to finalize grant agreements for Coastal Structures Enhancement and Self-Preservation Mode,

106 Hardening of S-2, S-3, S-4, S-7, S-8 Engine Control Panels, and L8 FEB/G-539 Pump Resiliency Upgrade,
107 and with Palm Beach County for the Corbett Levee. At the Federal level, the District and USACE are
108 partnering to develop the C&SF Flood Resiliency Study, to recommend adaptation strategies in the
109 communities served by the C&SF Systems. In addition, FEMA mitigation and adaptation funding is under
110 consideration and the District is working to finalize a grant agreement for the award recommendation
111 received from the FEMA BRIC Program for the C-8 Basin Resiliency Project.

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Chapter 1: Our Resiliency Vision

The South Florida Water Management District (District) is committed to reducing the risks of flooding, sea level rise (SLR) and other climate impacts on water resources and increasing community and ecosystem resiliency in South Florida, by updating and enhancing the Central South Florida Project (C&SF Project) and Big Cypress Basin (BCB) infrastructure. This will be accomplished using traditional gray infrastructure improvements and nature-based solutions. The current plan document focuses on the most vulnerable infrastructure, recognizing that the District's entire area of operations will be covered as technical assessments and planning efforts identify additional resiliency projects and priorities each year. The Plan's vision is to reduce risk by implementing effective, resilient solutions and anticipate future conditions, while engaging the public through various outreach activities. The District's Flood Protection Level of Service (FPLOS) and Capital Improvement Program (CIP) programs ensure that projects are assessed, designed, managed, and constructed using innovative techniques, incorporating sustainable sources of energy, and utilizing the most efficient designs available, with consideration of both upstream and downstream systems. The proposed resiliency projects follow all local and Federal threatened and endangered species regulations and seek to restore and preserve wildlife habitat by integrating nature-based solutions. The District seeks to implement projects that benefit the South Florida's communities and environment by working closely with state, tribal, private, and local governments and taking into consideration the needs of socially vulnerable communities and protected environmental areas.



The District's Resiliency Plan is a high-level planning document and is not intended to contain all the technical details and specifications for each proposed project. As projects are moved into implementation, detailed plans, design specifications and technical reviews will follow. Below are descriptions of each of the criteria that, when taken together, illustrate our resiliency vision and our unique role in addressing environmental, water supply and flood protection, in the context of water management operations and infrastructure risks and vulnerabilities.

RISK REDUCTION/ EFFECTIVENESS

The District seeks to reduce risk while maximizing the effectiveness of our projects by advancing robust hydrologic and hydraulic integrated basin wide models through the FPLOS Program. This will allow us to look at maximum stages, bank exceedances and discharge capacity of our canals as well as the flood depths and durations of overland flood inundation. Additionally, coastal structure capacity and peak stages resulting from different storm surge and SLR scenarios are examined.

43 **IMPLEMENTATION RESOURCES**

44 Implementation measures describe how project costs and schedules will be managed, how the project
45 will be implemented, and how innovative techniques will be incorporated. A well-planned resiliency project
46 includes identification of technical and project management staff and other resources needed for successful
47 implementation. Consideration is also given to potential technical, political, and financial challenges and
48 how they can be overcome. Additionally, project costs and schedules and pre- and post-implementation
49 monitoring plans should be well defined.

50 **ANTICIPATED FUTURE CONDITIONS**

51 Future conditions within each project impact area (drainage basin) are important to consider when
52 deciding if a project is viable. It is vital to know when and where the population within a basin is projected
53 to increase, and if land use and development are predicted to shift. Understanding demographics and
54 changes in economic status of the community is also important. Beyond the traditional planning tools, there
55 is a need to address future climate conditions and their impacts, including SLR, frequency and intensity of
56 rainfall extreme events, increasing groundwater elevations, and other related variables. The project should
57 be responsive to any anticipated changes, and these changes should be integrated into the planning, design,
58 and future operation of the project. Each potential project should be informed by and/or connected to
59 planning efforts such as Hazard Mitigation Plans, Climate Adaptation Plans, Comprehensive Plans, and
60 others.

61 **VULNERABLE POPULATION AND CRITICAL INFRASTRUCTURE**

62 Effective resiliency projects have community-wide benefits and should identify the populations that
63 will be impacted, both positively and negatively. Percentage of the population that will directly benefit from
64 the project, including the extent of the project's direct and indirect protection of community lifelines
65 (fundamental services that allow society to function), regionally significant assets, businesses, residents,
66 public services and natural resources are defined. Disadvantaged communities are also identified and taken
67 into consideration. Positive impacts to vulnerable disadvantaged communities are maximized. The District
68 strives to meet these criteria.

69 **LEVERAGING PARTNERSHIPS AND PUBLIC ENGAGEMENT**

70 The District has been engaging partner agencies and the public through the organization of a series of
71 Public Workshops and participation in relevant public events and discussions. In December 2022, SFWMD
72 hosted the first South Florida Resiliency Coordination Forum. These recurring quarterly meetings constitute
73 a fact-finding forum to promote collaboration with local, state, federal and tribal partners on water
74 management initiatives related to resiliency; and engage partners on assessing the impacts of changing
75 climate conditions and water management implications. The Forum promotes regional coordination and
76 partnership opportunities by holding proactive discussions, leveraging technical knowledge, and
77 exchanging information. These meetings are designed to foster a constructive environment to discuss
78 tangible asset-level solutions and support decision making on water resource management.

79 Outreach activities are an important way to engage, learn and gain public support for resiliency projects
80 and leverage partnership with local, regional, state and Federal Agencies. In addition, FPLOS public
81 workshops, prioritized for basins with elevated flood risk where adaptation strategies and mitigation
82 projects need to be collaboratively developed and implemented, give stakeholders with flood control
83 responsibilities an opportunity to share provide input and help guide the selection of projects compatible
84 with local efforts/initiatives. Information and feedback from the public can add value to the District's
85 planning process by introducing a real-world perspective to modeling results. The District is advancing
86 integration and climate resilience strategies in the region through coordination with the public, educational
87 institutions, stakeholders, and federal, state, and local government agencies including the U.S Army Corps

88 of Engineers (USACE), Florida Department of Environmental Protection Office of Resilience and Coastal
89 Protection, Florida Department of Emergency Management, 298 Districts, planning councils, local
90 governments, the Southeast Florida Regional Climate Change Compact, the Southwest Florida Regional
91 Resiliency Compact, and the East Central Florida Regional Resilience Collaborative.

92 **ONGOING ECOSYSTEM RESTORATION EFFORTS**

93 The District is working with USACE and other State and Federal partners to ensure ongoing ecosystem
94 restoration efforts, and mainly the Comprehensive Everglades Restoration Plan (CERP) projects are fully
95 implemented and operational. Restoring and preserving ecosystems is key to building and maintaining
96 resiliency throughout South Florida. These restoration-resiliency efforts have been creating and improving
97 ecosystems, increasing ecosystem health and function, and allowing for increased water management
98 flexibility to reduce saltwater intrusion in coastal groundwater. With improved ecosystem function, these
99 projects have decreased the impact of flooding and SLR on South Florida’s communities.

100 **INNOVATIVE GREEN/NATURE-BASED SOLUTIONS**

101 The District is committed to seeking “green” or nature-based solutions (NBS) in addition to “gray”
102 stormwater infrastructure improvements to increase resiliency. NBS include features such as living
103 shorelines, wetlands, artificial reefs, other urban green infrastructure features and preservation and
104 restoration of existing natural features. Both gray and green features will be necessary to meet the
105 challenges of climate change impacts, including SLR, along with basin-wide solutions to maximize the
106 capacity of flood adaptation and to achieve water quality benefits. District projects will also incorporate
107 sustainable and clean sources of energy whenever possible and utilize the most efficient designs available.

108 **OFFSETTING NEW ENERGY DEMANDS WITH SUSTAINABLE SOURCES**

109 The District is dedicated to improving the energy efficiency of our operations and offsetting new energy
110 demands through renewable energy solutions. By following the latest building codes and using state of the
111 art materials and designs, the District builds efficient and resilient projects (Flood Resistant Design and
112 Construction, ASCE Standard 24). As an initial step towards the goal of offsetting new energy demands,
113 staff are assessing opportunities for implementing solar power projects, as part of a variety of current
114 projects under development.

Chapter 2: The Central and Southern Florida System and Big Cypress Basin

The Central and Southern Florida Project (C&SF) was initially authorized by the Flood Control Act of 1948, and subsequent Acts. It is a large, multipurpose water resources project designed and constructed by the United States Army Corps of Engineers (USACE) in partnership with South Florida Water Management District (SFWMD or District), the project's local sponsor. It was authorized for the purposes of flood protection for urban and agricultural areas; prevention of saltwater intrusion risks to coastal water supply sources; water level control and conservation to ensure water supply for agricultural, municipal, industrial, and ecosystem uses; and preservation of fish and wildlife. The Project was designed to serve a population of 2 million people.

Multiple project phases throughout the years contributed to the development and expansion of the C&SF integrated water management system. Today, the key structural infrastructure of the regional (primary) C&SF system includes approximately 2,175 miles of canals, 2,130 miles of levees/berms, 89 pump stations, and 915 water control structures. The regional system connects to local (secondary) and thousands of neighborhood (tertiary) drainage systems. It's one of the world's largest and most complex water management systems and currently serves a population of approximately 9 million residents.

The C&SF system is facing significant changes that are challenging the purposes of the system. The main drivers of change can be largely grouped into categories of population growth, increased development of land, extreme rainfall events, and sea level rise (SLR) trends. A roughly tenfold increase in the study area population and consequent change in land use over time, compounded by extreme rainfall events and an average of 6 inches of observed SLR, has significantly changed the performance of the C&SF system.

Despite significant infrastructure investments throughout the years, critical components of the C&SF system are showing deficiencies in performance. For example, gravity operated coastal structures convey excess runoff from each respective watershed to the ocean to reduce flood risk, and act as salinity intrusion barriers. Currently, many of these low-lying Coastal Structures cannot discharge during certain high tide periods and/or storm surge events because of insufficient upstream headwater (spillway) elevations. Gate overtopping, due to high tailwater events, has already been documented in the lower east coast region. As part of future conditions assessments, coastal structure operations were simulated under different SLR scenarios, considering both upstream canal overbank risks, as well as reduction in gravity discharge capacity. Based on these advanced modeled outcomes, a number of these coastal structures were characterized as highly vulnerable to SLR, reaching bank-full elevation under a 25-year or less surge condition, and with 0.5 ft or less of sea level increase.

Also, within SFWMD boundaries, the Big Cypress Basin contains a network of 143.6 miles of primary canals, 35 water control structures and three back pumps providing flood control during the wet season and protecting regional water supplies and environmental resources from over-drainage during the dry season. The basin, which is facing similar conditions as described above, includes Collier County and part of Monroe County.

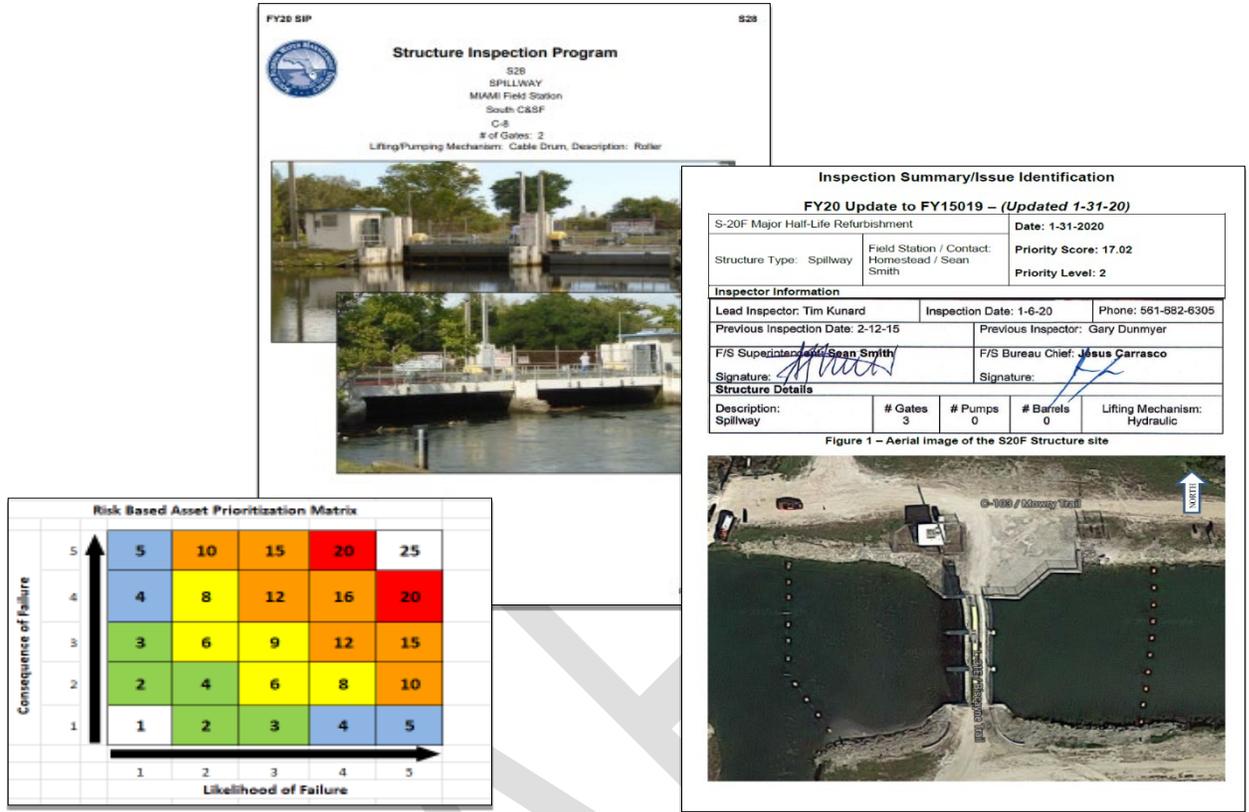
40 Despite these challenges and opportunities, SFWMD is making infrastructure maintenance and
41 adaptation investments that are needed to successfully continue to implement its mission of safeguarding
42 and restoring South Florida’s water resources and ecosystems, protecting communities from flooding, and
43 ensuring an adequate water supply for all of South Florida’s needs. Building Resiliency and Mitigating
44 Risks to South Florida Water Resources and enhancing the C&SF System and Big Cypress Basin are
45 integrated with the District’s Capital Improvement Plan (CIP).

46 The District's CIP infrastructure investments go beyond addressing needs identified in inspection
47 reports. The District is also enhancing the water management system with additional new components and
48 operational capacity, making it possible for the over 70-year-old system to operate successfully today and
49 ensuring the District mission is accomplished. This plan document outlines additional investments to be
50 bundled with the District’s CIP to ensure that we are Building Resiliency and Mitigating Risks to South
51 Florida Water Resources now and into the future.

52 **SFWMD CAPITAL IMPROVEMENT PLAN**

53 Since its creation in 1949, the District has been responsible for managing the C&SF System and Big
54 Cypress Basin. The District has a multimillion-dollar Capital Improvement Plan already in place, with an
55 average annual budget of \$53M. All water control structures are inspected every five to seven years as part
56 of the District’s Structure Inspection Program (SIP). The purpose of the District’s inspection program is to
57 ensure that each facility's equipment and instrumentation can be operated safely and reliably and to
58 prioritize infrastructure investments for the District’s CIP Program. The District commits to setting aside
59 resources each year to implement the CIP for repairing, refurbishing, enhancing, and upgrading pump
60 stations, canals, water control structures, levees, and water storage areas to ensure the District water
61 management infrastructure and facilities are operating at peak efficiency.

62 Inspections cover civil, structural, mechanical, electrical, and underwater components of the structure
63 and each component is rated based on the severity of deficiencies, and on the urgency of recommended
64 corrective actions. The individual component ratings are evaluated together to formulate an overall rating
65 that guides prioritization of corrective actions. Figure 2-1 illustrates examples of the structure inspection
66 program reports and the risk matrix used to calculate the overall rating. The “likelihood of failure” scoring
67 is calculated based on the inspection of physical condition, the ability to operate and maintain the
68 structure/facility as intended and the frequency of operation. The “consequences of failure” scoring is based
69 on the location and size of the structure/facility, accounting for public health, safety, security & services,
70 its financial impact on surrounding land use, upstream/downstream impacts, and its back up operational
71 options. The inspection reports are also used to help evaluate adaptation strategies as part of the Flood
72 Protection Level of Service Program. Structures that receive a critical rating for corrective actions are
73 included as part of future conditions assessments and modifications for SLR and climate change impacts
74 are recommended, in addition to addressing conditions identified in the inspection reports. This process
75 ensures that the Resiliency Program and the regular CIP processes are integrated and improvements at each
76 structure are coordinated. The goal is to not have to revisit the same structure within a short period of time.



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Figure 2-1. Examples of Structure Inspection Program Reports and the Overall Risk Rating Matrix.

Chapter 3: Assessing Flood Vulnerabilities of Water Management Systems: The Flood Protection Level of Service Program

SUMMARY

Initiated in 2015, the South Florida Water Management District's (District or SFWMD) Flood Protection Level of Service Program (FPLOS) allows the agency to evaluate the effectiveness of its flood control assets, including canals, structures, and pump stations to determine their ability to meet and continue to meet the flood protection needs of the region. The Central and Southern Florida Project (C&SF Project) and other basins flood protection systems have many assets that are approaching end of design life, making it critical to implement this program to inform decisions on the flood control infrastructure needs of the region. The District is implementing the FPLOS program at a regional and local scale. The program includes a methodology that helps to prioritize basins to study, and a suite of tools for evaluating structures and canals in selected basins, as well as a framework for establishing the level of service. The program incorporates input from meetings and workshops with local planning and stormwater management efforts, stakeholders, and resource managers. The FPLOS will be implemented in a phased approach on a 8- to 10-year cycle. Each basin will be evaluated, and actions taken as necessary, to ensure that the level of service is maintained. When remediation is needed, the lowest cost measures will be undertaken first, building to full replacement only when necessary. The cycle will provide opportunities to update land development and sea-level information and incorporate new technology and tools. This cyclic approach is the best use of funding and ensures that incremental, near-term measures will be incorporated into any long-term solution. The program is being executed in three stages.

26

Flood Vulnerability Assessment Phase (Phase I)

This stage of the program involves a periodic exploratory investigation of the primary system and related work and studies necessary to identify choke points or deficiencies in the flood control infrastructure with a focus on the primary system. This process is used to identify flood vulnerabilities basin-wide, represented by simulated overland flow inundation. These studies continue in perpetuity and each basin is revisited once every eight to ten years unless significant changes in the flood control system necessitate a more frequent reassessment.

Adaptation and Mitigation Planning Phase (Phase II)

When deficiencies are identified in the system (either current or projected based on factors such as sea level rise (SLR) and future rainfall), an Adaptation and Mitigation Planning study is triggered which executes a search for a solution within the primary system as well as the secondary and tertiary systems. These public planning projects represent collaborative efforts with operators of the secondary and tertiary systems and identifies cost effective courses of action that will, when implemented, bring the flood control system back to design specifications or desired performance for the long term.

Implementation Phase (Phase III)

The final phase includes integration of the recommended projects into this plan document, and prioritization for follow-up design, permitting, real estate acquisition, and construction activities necessary to implement the selected adaptation strategy and course of action,

27

28 The District has taken a comprehensive and high-level approach to addressing the flood protection
29 needs of the region. It is rigorous in its analyses using high quality integrated modeling tools, and pragmatic
30 in its implementation. At its core, this approach is a commitment to an ongoing assessment of the state of
31 the system to ensure that problems are identified before they occur, providing an opportunity to plan and
32 implement adaptations and mitigations strategies before critical conditions materialize.

33 With a goal to reassess every basin within the District at least once every 8 to 10 years, the program
34 initiates two Phase I assessment studies every year, starting with the most at-risk basins. This is determined
35 based on a SLR vulnerability assessment, observed flooding, and known system limitations. These studies
36 answer the key question: are the flood protection assets working and will they continue to work for the next
37 50 years? Another strength of this method is the collaborative approach in search for the appropriate
38 solution. The District engages partners and stakeholders with responsibility for the secondary and tertiary
39 flood control systems to identify the best course of action to mitigate identified deficiencies.

40 Phase II of the FPLOS program includes the assessment of projects to be implemented by SFWMD,
41 along with projects and actions to be included by stakeholders in their implementation vehicles such as
42 Local Mitigation Strategies and local capital projects programs. Working with and incorporating projects
43 planned in the secondary and tertiary system will ensure robust, regionally compatible suites of projects
44 with broad regional support and more attractive to funding, to ensure effective flood control. In addition to
45 evaluating, prioritizing, and sequencing potential solutions, the FPLOS approach addresses uncertainties
46 related to SLR and other climate projections by introducing decision support and facilitation tools and
47 techniques used for decision making under uncertainty. This aspect of the program allows decision makers
48 to make smart near-term decisions that do not foreclose on other options, should longer term projections
49 change from what is currently anticipated. The solutions are comprehensive and could range from a change

50 in operations requiring no additional infrastructure, to major investments in infrastructure including using
51 nature-based solutions whenever possible. The cycle will provide opportunities to update land development
52 and sea-level information and incorporate new technology and tools, to ensure that incremental, near-term
53 measures will be incorporated into long-term solutions.

54 Figure 3-1 below illustrates the latest status of the FPLOS vulnerability assessments (Phase I) and the
55 priority basins, with consideration for existing infrastructure managed by the District. Over the next year
56 and a half, Phase I assessments will be completed for all critical basins in the C-2, C-3W, C-5 and C-6
57 Basins (Miami #3), C-111, Model Lands, and L-31NS Basins (Miami #5), Eastern Palm Beach County and
58 Upper Kissimmee Basin. Adaptation planning studies (Phase II) were completed for the C-8 and C-9 Basins
59 and are ongoing for the C-7 Basin. In parallel, infrastructure atlases have been updated for Palm Beach
60 County and the Upper Kissimmee Basins. Other support studies such as the Low-Lying Tidal Structure
61 Assessment, Biscayne Bay Surge Model, and the Atlas updates for Big Cypress Basin, Broward County;
62 South Miami Dade; North and Central Miami Dade also contribute to further understanding of flood
63 vulnerabilities across the District.

64 Fully integrated and coupled hydrologic and hydraulic models have been developed and implemented,
65 as part of these studies, to determine flood vulnerabilities and to support adaptation and mitigation planning.
66 These advanced models simulate complex surface-subsurface water interactions and operational rules at
67 each system structure, along with a range of storm surge and tidal boundary conditions, for different rainfall
68 return frequencies and duration. Modeling outputs enhance technical understanding of the impacts caused
69 by compound flooding drivers (rainfall, surge/tidal and groundwater), which is critical to identify
70 appropriate and effective resilience needs in coastal urban watersheds in South Florida. An approach for
71 characterizing compound flooding and respective joint probabilities in transition zones is currently being
72 validated.

73 Figure 3-2 and Figure 3-3 illustrate the resulting current and future overall Flood Protection Level of
74 Service generally provided by existing infrastructure within each basin, as summarized in the final reports
75 (summary and conclusions session) for the respective FPLOS Phase I (Flood Vulnerability) assessments
76 completed for Broward and Miami-Dade Counties and for Big Cypress Basin (BCB). The Flood Protection
77 Level of Service is illustrated in these maps by the respective rainfall return frequency event that results in
78 flooding in each basin, simulated as part of the completed FPLOS Phase I Assessments. The overall Flood
79 Protection Level of Service assigned to each basin is a combination of the results from six performance
80 metrics measured within each basin, for current and future conditions, and if both rainfall-induced flooding
81 and storm surge flooding occurs simultaneously, as summarized in Table 3-1. It is important to emphasize
82 that only portions of each basin might be showing inundation, because of the simulated scenarios, meaning
83 that the entire basin might not be inundated under the given return frequency. The overall level of service
84 assigned to each basin represents portions of that basin that will have significant overland flooding
85 simulated under that return frequency. Detailed results, illustrating specific regions within each basin where
86 simulated results are showing overland inundation, are provided in the final FPLOS Phase I Reports.

87 A model crosswalk for the C-8 and C-9 basins and South Miami Dade (C-1, C-100, C-102, C-103) was
88 performed to compare the performance and results of the District's FPLOS and Miami Dade County's
89 modeling frameworks (MIKE SHE-MIKE Hydro and XPSWMM respectively) under current and SLR2
90 conditions. Despite some differences in model assumptions and conceptualization, both models show
91 similar results in terms of stage profiles along the canal prior to the coastal structure and similar flooding
92 conditions when considering depths above 1 foot.

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FPLOS Sea Level Rise Scenarios

The FPLOS Program assesses future conditions sea level scenarios. For that, three scenarios were defined relative to the 2015 or a more current year conditions depending on a project starting year, assumed as current sea level (2015 CSL):

- CSL +1 ft
- CSL +2 ft
- CSL +3 ft

According to Section 380.093 (5) F.S., flood vulnerability assessments should be performed accounting for at least two local sea level rise scenarios, including the NOAA intermediate-low and intermediate-high sea level rise projections, and two planning horizons for the years 2040 and 2070.

In Virginia Key, the 2022 NOAA SLR projections, relative to 2000 are detailed below. Observed change in annual MSL between 2000 and 2015 in this location is 0.073m or 0.24ft.

Intermediate Low 0.23m or 0.75ft (2040); 0.44m or 1.44ft (2070)
 Intermediate High 0.27m or 0.88ft (2040); 0.79m or 2.59ft (2070)

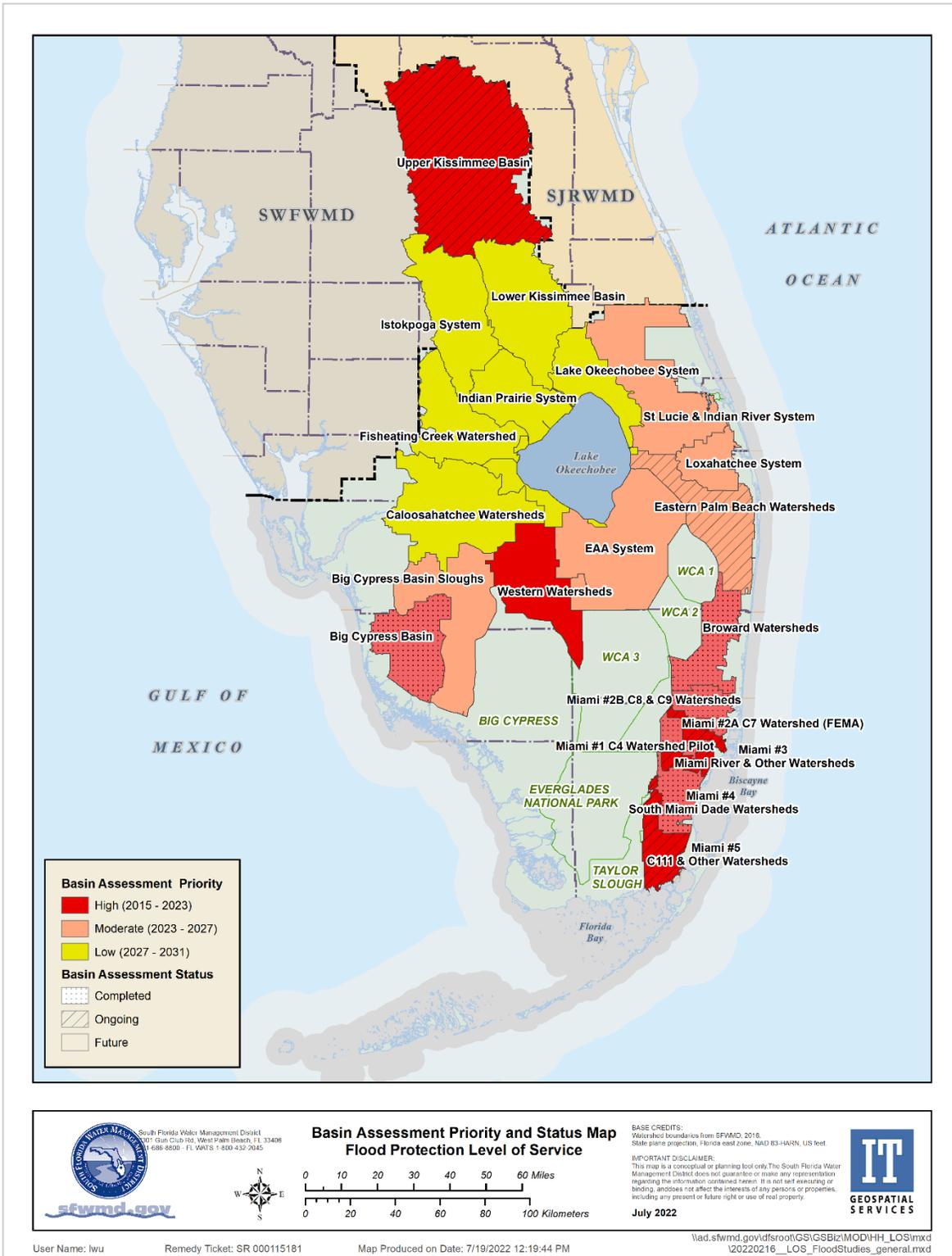
In Key West, the 2022 NOAA SLR projections, relative to 2000 are detailed below. Observed change in annual MSL between 2000 and 2015 in this location is 0.099m or 0.325ft. The Figure below illustrates the NOAA 2022 Projections at the Key West Tidal Station.

Intermediate Low 0.24m or 0.79ft (2040); 0.44m or 1.44ft (2070)
 Intermediate High 0.28m or 0.92ft (2040); 0.80m or 2.62ft (2070)

The table below summarizes the SLR projections relative to 2000, as presented by NOAA and relative to 2015, as adopted in the FPLOS Program SLR scenario formulation:

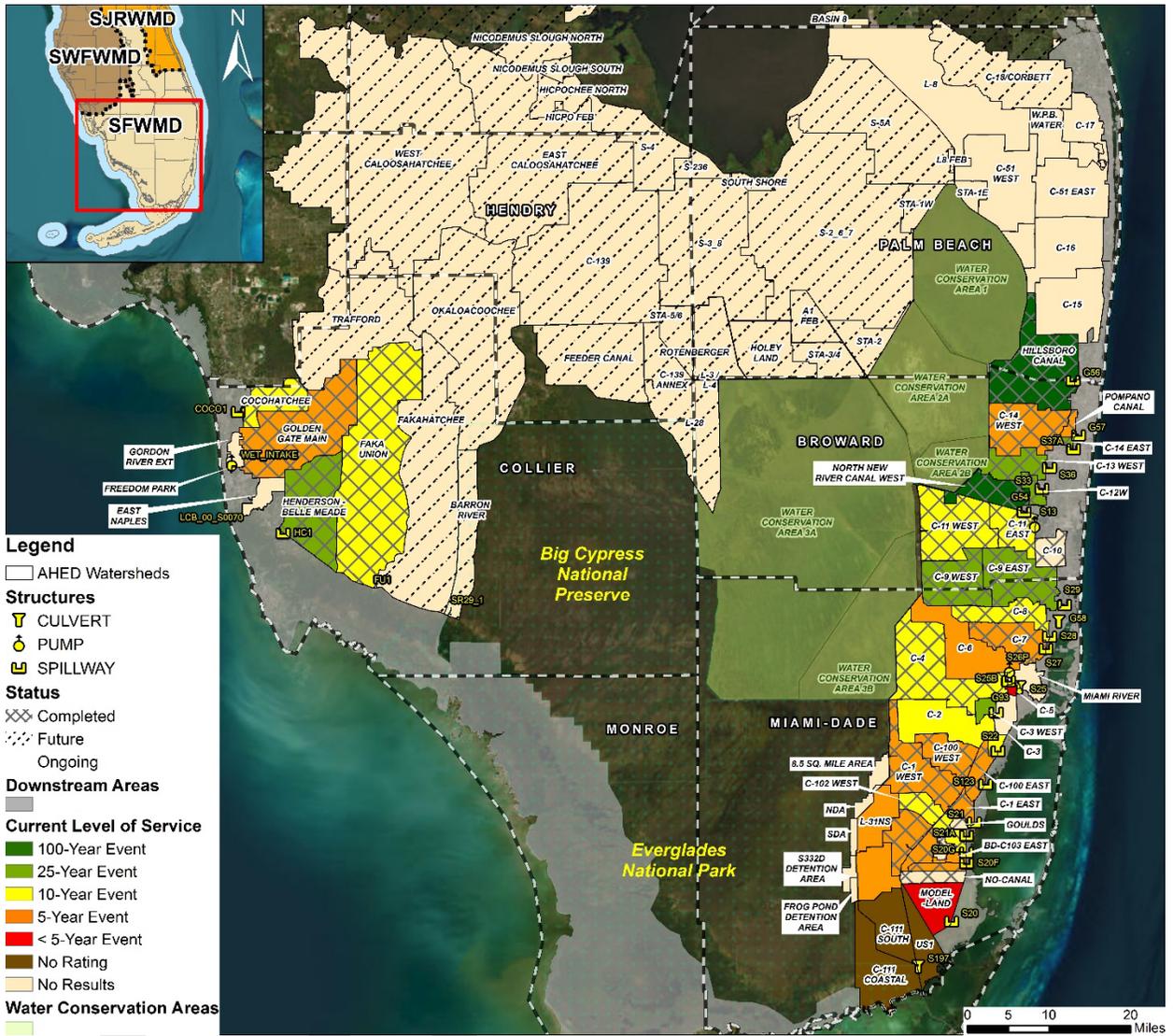
NOAA 2022 SLR Projections	Relative to 2000				Relative to 2015			
	2040 (m)	2040 (ft)	2070 (m)	2070 (ft)	2040 (m)	2040 (ft)	2070 (m)	2070 (ft)
Intermediate Low - Virginia Key	0.23	0.75	0.44	1.44	0.16	0.51	0.37	1.2
Intermediate High - Virginia Key	0.27	0.88	0.79	2.59	0.20	0.64	0.72	2.35
Intermediate Low - Key West	0.24	0.79	0.44	1.44	0.14	0.47	0.34	1.12
Intermediate High - Key West	0.28	0.92	0.80	2.62	0.18	0.60	0.70	2.30

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101 **Figure 3-1.** FPLOS Basin Assessment Priorities and Status of Implementation.
 102 Disclosure: The current map will be updated as the Miami #3 and Miami #5 Basin Assessments are
 103 undergoing and will be completed by September 1st, 2023.

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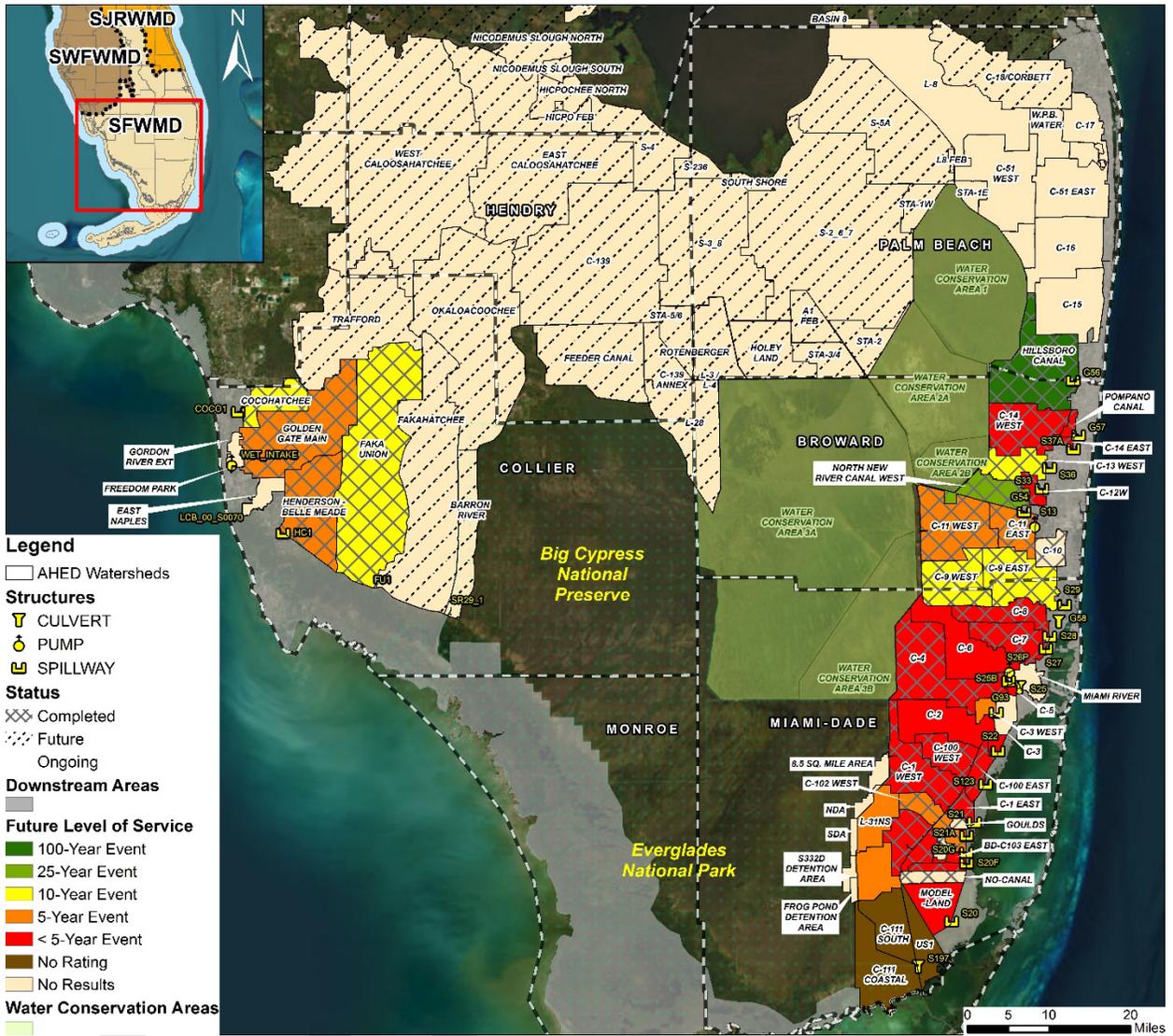
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Figure 3-2. Current Flood Protection Level of Service generally provided by existing infrastructure in critical basins, predominantly located in Broward and Miami-Dade Counties. The Level of Service is represented by the respective rainfall frequency event that results in flooding within areas of each basin, simulated as part of completed FPLOS Phase I – Flood Vulnerability Assessments.

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Figure 3-3. Future Flood Protection Level of Service, under a 2ft SLR Scenario, generally provided by existing infrastructure in critical basins, predominantly located in Broward and Miami-Dade Counties. The Level of Service is represented by the respective rainfall frequency event that results in flooding within areas of each basin, simulated as part of completed FPLOS Phase I – Flood Vulnerability Assessments.

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Table 3-1. Flood Protection Level of Service Summary Assessment for Maximum Stage in Primary Canals (PM1) and Frequency of Flooding (PM5) for current and future conditions.

Basins	PM1				PM5			
	Current Conditions	Future Conditions & 1ft SLR	Future Conditions & 2ft SLR	Future Conditions & 3ft SLR	Current Conditions	Future Conditions & 1ft SLR	Future Conditions & 2ft SLR	Future Conditions & 3ft SLR
C-2 ⁷	10-Year	5-Year	< 5-Year	< 5-Year	25-Year	25-Year	10-Year	10-Year
C-3W ⁷	25-Year	10-Year	5-Year	< 5-Year	25-Year	10-Year	10-Year	10-Year
C-5 ⁷	25-Year	10-Year	< 5-Year	< 5-Year	< 5-Year	< 5-Year	< 5-Year	< 5-Year
C-6 ⁷	25-Year	10-Year	5-Year	< 5-Year	5-Year	5-Year	< 5-Year	< 5-Year
C-8 ¹	10-Year	5-Year	5-Year	5-Year	10-Year	5-Year*	< 5-Year	< 5-Year
C-9 ¹	25-Year	10-Year	10-Year	5-Year	25-Year	10-Year*	10-Year*	5-Year*
Hillsboro ²	100-Year	100-Year	100-Year	100-Year	100-Year*	100-Year*	100-Year*	100-Year*
C-14 West ²	100-Year	25-Year	25-Year	25-Year	10-Year*	5-Year*	< 5-Year	< 5-Year*
C-14 East ²	25-Year	10-Year	< 5-Year	< 5-Year	25-Year	10-Year	< 5-Year	< 5-Year
Pompano ²	100-Year	100-Year	100-Year	100-Year	< 5-Year	< 5-Year	< 5-Year*	< 5-Year*
C-13 West ²	25-Year	25-Year	10-Year	< 5-Year	25-Year	25-Year	10-Year	< 5-Year
C-12 West ²	25-Year	10-Year	< 5-Year	< 5-Year	25-Year*	5-Year	< 5-Year	< 5-Year
North New River West ²	100-Year	100-Year	25-Year	10-Year	100-Year*	100-Year*	25-Year*	10-Year*
C-11 West ²	10-Year	10-Year	10-Year	10-Year	10-Year*	10-Year*	10-Year*	10-Year
C-11 East ²	10-Year	5-Year	5-Year	5-Year	10-Year*	5-Year	< 5-Year*	< 5-Year*
C-4 ³	10-Year	5-Year	< 5-Year	< 5-Year	10-Year*	5-Year*	< 5-Year*	< 5-Year*
C-7 ⁴	< 5-Year	< 5-Year	< 5-Year	< 5-Year	< 5-Year*	< 5-Year*	< 5-Year*	< 5-Year*
C-1 ⁵	C1 & C1N: 5-Year	5-Year or less	5-Year or less	5-Year or less	10-Year	10-Year	< 5-Year*	< 5-Year
	C1N: 10-Year	5-Year or less	5-Year or less	5-Year or less	10-Year	10-Year	< 5-Year*	< 5-Year
C-100 ⁵	5-Year	5-Year	< 5-Year	< 5-Year	25-Year	5-Year*	< 5-Year*	< 5-Year

C-102 ⁵	10-Year	10-Year	5-Year	5-Year	5-Year	5-Year*	5-Year*	< 5-Year
C-103 ⁵	5-Year	5-Year	5-Year	5-Year	5-Year	5-Year*	5-Year*	<5-Year
C-111 COASTAL	100-Year	100-Year	100-Year	100-Year	N/A	N/A	N/A	N/A
US-1	N/A	N/A	N/A	N/A	10-Year	10-Year	10-Year	10-Year
L-31NS (Canal L-31NS)	5-Year	5-Year	5-Year	5-Year	10-Year**	10-Year**	10-Year**	5-Year**
L-31NS (C-102)	10-Year	10-Year	10-Year	5-Year	10-Year**	10-Year**	10-Year**	5-Year**
L-31NS (C-103)	10-Year	5-Year	<5-Year	<5-Year	10-Year**	10-Year**	10-Year**	5-Year**
C-111 AG (C-111)	25-Year	10-Year	10-Year	5-Year	5-Year**	5-Year**	5-Year**	5-Year**
C-111 AG (C-113)	10-Year	10-Year	10-Year	5-Year	5-Year**	5-Year**	5-Year**	5-Year**
C-111 AG (C-111E)	5-Year	5-Year	<5-Year	<5-Year	5-Year**	5-Year**	5-Year**	5-Year**
C-111 SOUTH (C-111)	100-Year	100-Year	100-Year	100-Year	10-Year	10-Year	10-Year	10-Year
C-111 SOUTH (C-111E)	100-Year	100-Year	100-Year	100-Year	10-Year	10-Year	10-Year	10-Year
MODEL LAND (Card Sound Rd)	5-Year	<5-Year	<5-Year	<5-Year	10-Year	10-Year	10-Year	10-Year
MODEL LAND (L-31E Canal)	5-Year	<5-Year	<5-Year	<5-Year	10-Year	10-Year	10-Year	10-Year
Cocohatchee ⁶	10-Year	10-Year	10-Year	5-Year	10-Year**	10-Year**	10-Year**	5-Year**
Golden Gate ⁶	5-Year	5-Year	5-Year	<5-Year	5-Year**	5-Year**	5-Year**	<5-Year**
Henderson Creek ⁶	25-Year	25-Year	25-Year	10-Year	25-Year**	25-Year**	25-Year**	10-Year**
Faka Union ⁶	10-Year	10-Year	10-Year	5-Year	10-Year**	10-Year**	10-Year**	5-Year**

Footnotes:

* The report does not contain sufficient information to confirm the LOS results. The proposed return periods were interpreted based on available information from the FPLOS study, including technical memorandums, canal profiles, flood maps and appendices; thus, the results do not reflect the SFWMD assessment on the LOSas these are subject to technical interpretation and should be further reviewed by localstakeholders.

**The LOSresults are tightly connected with the primary canal system.

**Preliminary results

¹ C-8 and C-9 FPLOS study was completed in 2021

² Broward County FPLOS study was completed in 2021

³ C-4 FPLOS is a study produced by the H&H Bureau as a project deliverable for project 100888 (FPLOS, within the SLR projections) and completed in May 2016. The LOS design events assessed include the 5-year 72-hour, 10-year 72-hour, 25-year 72-hour, and 100-year 72-hour storm events and surge return periods, current sea level and three future sea level rises (+0.34 ft, +0.8 ft, and 2.26 ft) focused on a 50-year planning horizon. The assessment of +0.34 ft SLR scenario suggested a 10-Year LOS, +0.80 ft SLR scenario was reduced to a 5-Year LOS and +2.26 ft scenario to <5-Year LOS. These scenarios were used as reference to produce a consistent FPLOS Summary Table, as most FPLOS efforts apply SLR +1 ft, SLR+2 ft, and SLR+3 ft as sea level rise conditions. For this reason, a SLR +1 ft scenario is defined as a 5-Year LOS, while for SLR +2 ft and +3 ft a <5-Year LOS or “No Answer” may be appropriate.

⁴ C-7 FPLOS is a study funded by FEMA and completed in 2017. The LOS design events assessed include the 5-year 24-hour, 10-year 24-hour, 25-year 72-hour, and 100-year 72-hour storm events and surge return periods, current sea level and three future sea level rises (+0.76 ft, +1.09 ft, and +2.21 ft). Under current condition and the three future sea level rise conditions, the assessment concluded that along downstream of the Spur Canal junction (NW 22nd Avenue), the maximum stages between NW 17th Avenue and N Miami Avenue exceed the canal bank elevations in all events and the stages exceed the canal bank elevation during the 25- and 100-year events along west of the 17th Avenue.

⁵ South Miami-Dade FPLOS study was completed in 2022

⁶ Big Cypress Basin FPLOS study was completed in 2017

⁷ Preliminary Results

133 FPLOS Next Steps

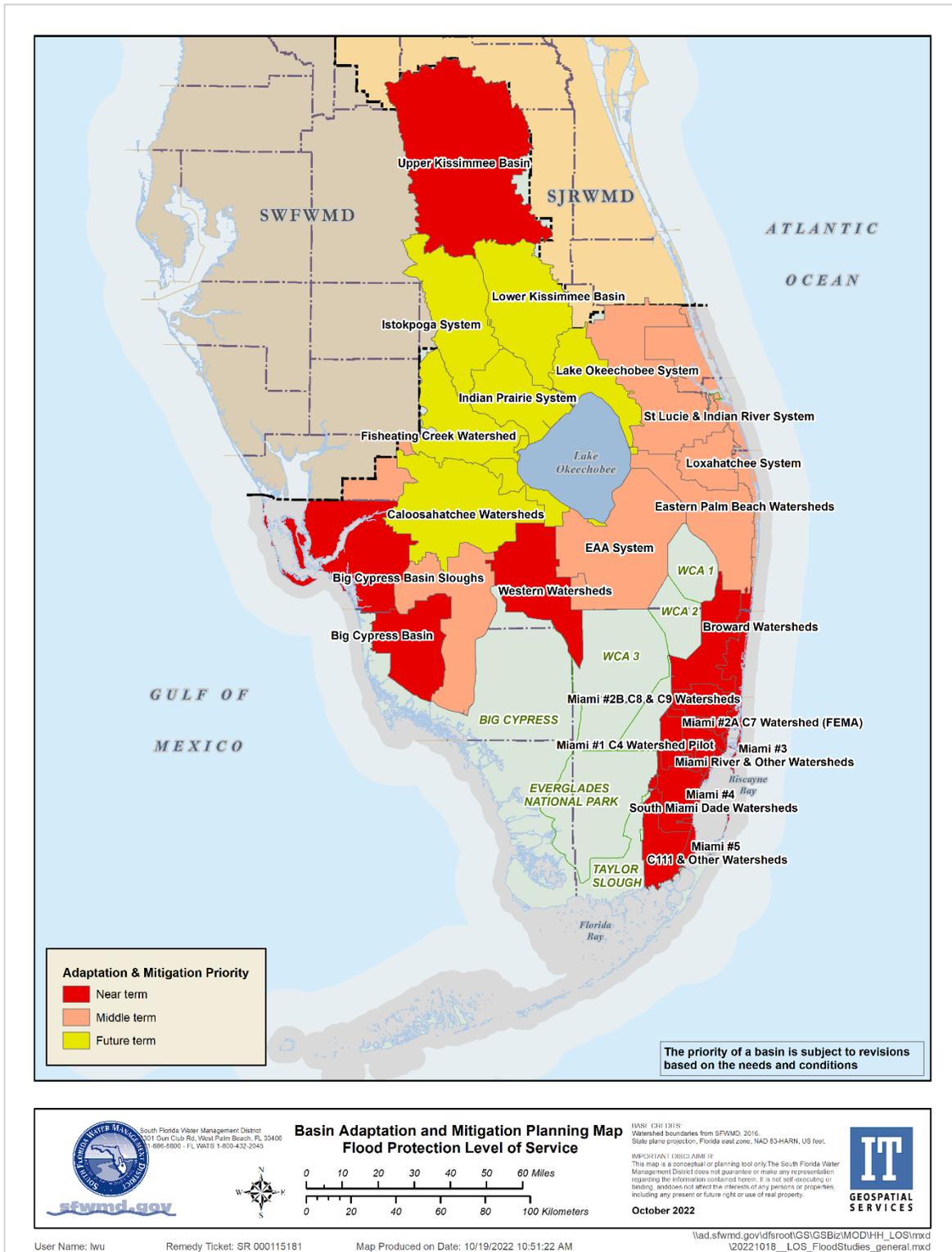
134 As described above, the FPLOS program is designed to allow for two new FPLOS Phase 1 Studies to
135 be initiated each year. Upon completion of the key assessments, or if specific projects or actions require a
136 more frequent reassessment, basins previously investigated will then be revisited to reassess the conditions,
137 considering potential changes to the flood control infrastructure and more refined information on future
138 conditions, including extreme rainfall projections. Flood vulnerability assessments for the St Lucie / Indian
139 River System and Loxahatchee System and the Western Basins are the upcoming Phase I studies included
140 in the FPLOS implementation schedule.

141 This schedule also incorporates the initiation of at least one new Phase II study every year. The C-7
142 Basin Phase II study is the ongoing adaptation planning effort. Figure 3-4 shows the prioritization of basins
143 for identifying adaptation and mitigation strategies across the District. Miami-Dade County, Broward
144 County, Collier County, Lee County and portions of the Upper Kissimmee Basin in Orange and Osceola
145 Counties represent parts of the system where studies are anticipated in the near term.

146 Funding needs to implement the FPLOS program Phase I and Phase II studies is summarized in Chapter
147 10. Over the next five years, it is expected that flood vulnerability assessments will be completed for all the
148 District's basins. Additionally, it is expected that adaptation and mitigation planning studies will be
149 completed for 25% of the District's basins, subject to funding availability.
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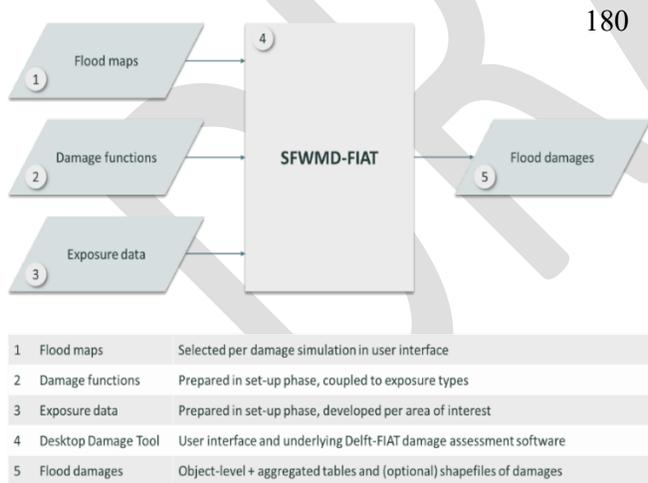
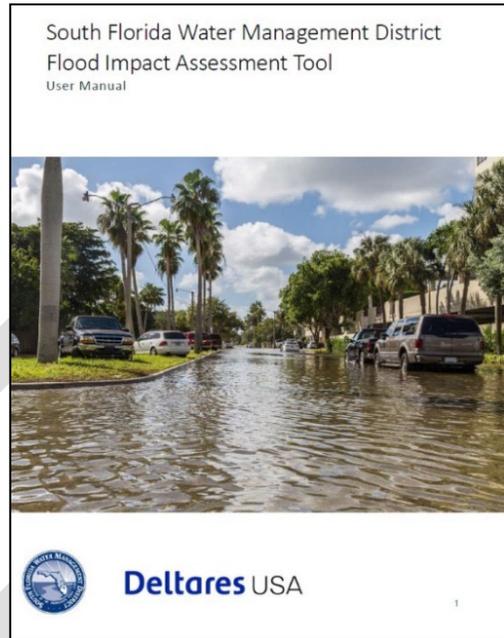
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Figure 3-4. FPLOS Basin Adaptation and Mitigation Planning Map

155 **SFWMD FLOOD IMPACT ASSESSMENT TOOL (SFWMD-FIAT)**

156 The District, as part of its Resiliency and Flood Protection
 157 Level of Service initiatives, has developed a Flood Impact
 158 Assessment Tool (SFWMD-FIAT). This tool helps support
 159 recommendations for flood mitigation and adaptation
 160 measures by providing cost benefits of implementing priority
 161 infrastructure investments. These recommended strategies are
 162 supported by advanced hydrologic and hydraulic modeling
 163 tools and assessments being implemented by the District’s
 164 Flood Protection Level of Service Program – Phase II
 165 (Adaptation Planning) and incorporated into this Plan. The
 166 tool provides the ability to perform future flood damage cost
 167 estimates using multiple flood elevation/inundation scenarios
 168 developed as part of future conditions modeling efforts, for
 169 various return frequencies, to calculate an expected annual
 170 flood damage estimate (Figure 3-5).

171 SFWMD-FIAT can calculate the flood damage costs for
 172 building structures and their contents – multiplied by the
 173 depreciated replacement value by square foot and by the area
 174 of the building footprint to calculate the max potential damage
 175 of the structure - as well as roads and other selected
 176 infrastructure components, for multiple flood inundation scenarios. The user can run damage calculations
 177 for multiple flood inundation scenarios and return periods using a single desktop tool. The tool is user
 178 friendly and versatile, as the economic damage curves and buildings values can be updated. The exposure
 179 data comes from the following official national data sources:



- County Supplied Building Footprints
- SFWMD Normalized Parcel and Land Use
- High Resolution Topo-Bathymetric Data
- Navteq / HERE RoadsHAZUS Occupancy Types and Depreciated Replacement Values

Figure 3-5: Block Diagram of SFWMD-FIAT tool.

185 shapefiles), including overall damage costs associated with combined structures and roads or by
 186 aggregation categories such as sub-basin, land use, tax use, census block, poverty level or critical
 187 infrastructure. The recommended projects within this Plan will have an associated cost-benefit ratio as part
 188 of the next planning round. The SFWMD-FIAT user manual is linked [here](#).

Chapter 4: Nature-Based Solutions

INTEGRATING NATURE-BASED SOLUTIONS

The use of nature-based solutions (NBS) has grown steadily over the past 20 years, supported by calls for innovation in flood risk management (FRM) and resilience planning. Communities, in general, have a strong desire to integrate NBS with traditional gray stormwater infrastructure. Accordingly, major grant programs, such as FEMA BRIC and Resilient Florida, assign higher scores to proposed projects that include NBS, making them more competitive. Additionally, the C&SF Flood Resiliency Study, currently under development with the U.S. Army Corps of Engineers (USACE) and South Florida Water Management District (District or SFWMD), as the non-federal sponsor, requires NBS as a part of FRM alternatives development process. In November 2022, the Federal government committed to ensuring that over \$25B in infrastructure and climate funding can support NBS, and presented a roadmap that includes unlocking funding for NBS, workforce training and updating guidance and policies (White House Council on Environmental Quality et al. 2022) such as:

- Better accounting for nature-based options in benefit cost analyses required by FEMA, USACE and other federal agencies in their regulatory and funding programs.
- Revising floodplain management requirements to consider NBS for all projects that can affect floodplains and wetlands.

The District is committed to seeking NBS in addition to and integrated into existing and planned “gray” infrastructure improvements and leveraging significant experience from the implementation of large ecosystem restoration and water quality efforts. Projects that “slow the flow” by using natural processes such as retention, infiltration, and evaporation/evapotranspiration to reduce runoff will be targeted. Additionally, preservation and restoration of existing natural features will continue to be implemented as an important strategy to increase resiliency.

Different terms and definitions of NBS for risk reduction and adaptation are in use across the variety of organizations that are implementing these features. Related terms, though not necessarily synonymous, include ecological engineering, engineering with nature, living shorelines, natural flood management, and green infrastructure, to name a few. The common element among all of these terms is the focus on working with natural processes for the benefit of people and ecosystems. For instance, Engineering With Nature (EWN) is an initiative of the USACE enabling more sustainable delivery of economic, social, and environmental benefits associated with water resources infrastructure. EWN intentionally aligns natural and engineering processes to deliver economic, environmental, and social benefits efficiently and sustainably through collaborative processes (Bridges et al. 2018 and 2021).

Nature-based solutions are defined as project features that use or mimic natural processes to maximize benefits. These features can be used to conserve or restore ecosystem services and/or enhance natural processes in engineered systems. Application of NBS often generate social, economic, and environmental co-benefits that improve human living conditions. Green infrastructure refers to natural or semi-natural systems that provide water resource management options comparable to traditional “gray” infrastructure. Green and gray features can be combined to enhance overall system resiliency. NBS and green infrastructure can be used to enhance flood protection against sea level rise (SLR) and increased extreme rainfall caused by climate change, as well as manage water supply and improve water quality. Both gray

42 and green infrastructure will be necessary to meet the challenges of climate change impacts, including SLR,
43 along with basin-wide solutions to maximize the capacity of flood adaptation as well as achieve water
44 quality and water supply benefits.

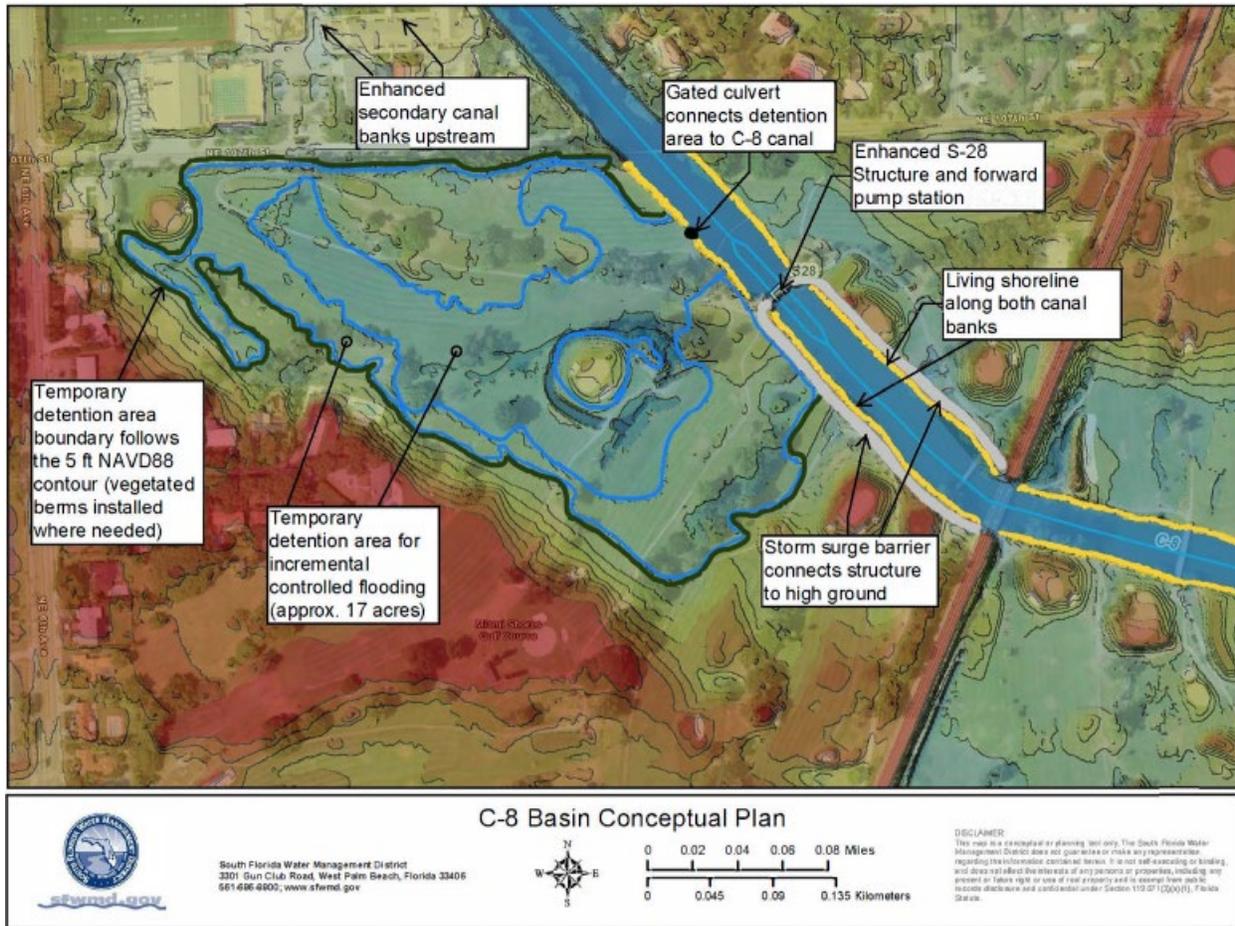
45 Nature-based solutions include features such as bioswales, raingardens, living shorelines, wetlands and
46 artificial reefs that reduce stormwater flooding and storm surge impacts by absorbing wave energy and/or
47 storing excess stormwater. Green urban infrastructure features include green and blue streets that are
48 designed to collect, store, and slow stormwater runoff. Green and blue streets have porous surfaces that
49 help to increase infiltration and direct runoff to trees planted in porous structural soil to increase storage
50 and evapotranspiration, as well as improve water quality. Scaled up, these features have the potential to
51 reduce flooding by using the natural water pumping (evapotranspiration) capacity of trees and other
52 vegetation to slow the flow and provide enhanced storage, detention, retention, and infiltration options.
53 Additionally, NBS also provides a multitude of water resources benefits by reducing net irrigation demand
54 for green spaces, and increasing retention and infiltration of surface water, which naturally recharges
55 aquifers and assists in preventing saltwater intrusion in coastal areas (see chapter 9).

56 **C-8 Basin Resiliency Project**

57 An example of a project that is proposing to use a combination of NBS and gray infrastructure is the
58 District's C-8 Basin project in Miami-Dade County. The C-8 Canal is the primary flood control feature that
59 receives and conveys basin floodwaters by gravity through the S-28 Coastal Structure to sea. The objective
60 of the project is to reduce flood risk as sea-levels rise and provide ancillary water quality benefits, by
61 restoring the basin's flood protection level of service and enhancing quality of life in the region. The project
62 includes a combination of structural measures and NBS (Figure 4-1), as follows:

- 63 • Replacement of the S-28 Structure with an enhanced structure and elevated components to
64 withstand the impacts of SLR and climate change.
- 65 • Installation of a forward pump station adjacent to the S-28 structure to maintain basin discharge
66 levels as sea levels rise.
- 67 • Construction of a flood barrier tying the S-28 Structure to higher ground elevations to assist in
68 mitigating the impacts of SLR, storm surge and saltwater intrusion.
- 69 • Enhancement of secondary canal banks to improve flood control throughout the basin.
- 70 • Construction of a temporary floodwater detention area utilizing vegetated berms and other green
71 infrastructure components, on a portion of the Miami Shores Golf Course near the S-28 Structure
72 to provide temporary storage of floodwaters and reduction of stormwater runoff volumes during
73 extreme rainfall events and provide ancillary water quality benefits.
- 74 • Installation of living shoreline along the C-8 Canal to assist in enhancing overall water quality
75 and aquatic habitat.

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Figure 4-1. Conceptual plan for the C-8 Basin.

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The strategy to reduce peak runoff in this densely urbanized basin includes the implementation of a series of distributed storage solutions as exemplified by the proposed project features, serving as pilot examples for the region. Ancillary benefits, include improved fish and wildlife habitat, improved land value due to reduced flood risk and enhanced aesthetics, prevention of canal bank erosion, water quality benefits, and increased opportunities for recreation.

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A more comprehensive list of examples of NBS that may be applied in South Florida are shown in Table 4-1 below. The table can be useful for identifying potential NBS for each water management/District mission type. The location of the proposed NBS feature and corresponding gray infrastructure that can be either replaced or enhanced by the NBS feature are identified.

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Table 4-1. Nature-Based Solutions/Green Infrastructure that may be applied in South Florida (adapted from UNEP-DHI/ICUN/TNC (2014, Table 1, p.6)

Water Management Topic/ District Mission		Green Infrastructure/Nature-Based Solution	Location				Corresponding Gray Infrastructure (at the primary service level)
			Watershed	Floodplain	Urban	Coastal	
Flood control	River/canal flood control	Reconnecting rivers/canals to floodplain		■			Levees and water control structures
		Wetland restoration/conservation	■				
		Constructed wetlands	■				
		Living shorelines/riparian buffers					
	Urban stormwater runoff	Green spaces (bioretention and infiltration)			■		Urban stormwater infrastructure
		Detention / Storage with associated “let it grow” strategies			■		
		Enhanced Infiltration / Groundwater recharge/storage			■		
		Permeable surfaces			■		
		Green roofs			■		
	Coastal flood control	Protecting/restoring mangroves, marshes, and dunes				■	Sea walls/forward pumps
Protecting/restoring reefs					■		
Water Supply		Reconnecting rivers/canals to floodplain		■		Impoundments, reservoirs, water distribution systems	
		Wetland restoration/conservation	■				
		Constructed wetlands, other detention/storage options	■				
		Enhanced Infiltration / Groundwater recharge/storage			■		
		Green spaces (bioretention and infiltration)			■		
		Permeable surfaces			■		
Water Quality	Water purification	Reconnecting rivers/canals to floodplain		■		Water treatment plant	
		Wetland restoration/conservation	■				
		Constructed wetlands	■				
		Green spaces (bioretention and infiltration)			■		
	Erosion control	Permeable surfaces			■		Reinforcement of banks/riprap
		Living shorelines/riparian buffers		■			
		Reconnecting rivers/canals to floodplain		■			
		Living shorelines/riparian buffers		■			
	Biological control	Reconnecting rivers/canals to floodplain		■			Water treatment plant
		Wetland restoration/conservation	■				
Constructed wetlands		■					
Living shorelines/riparian buffers			■				

97 **Process For Assessing And Implementing Nature-Based Solutions**

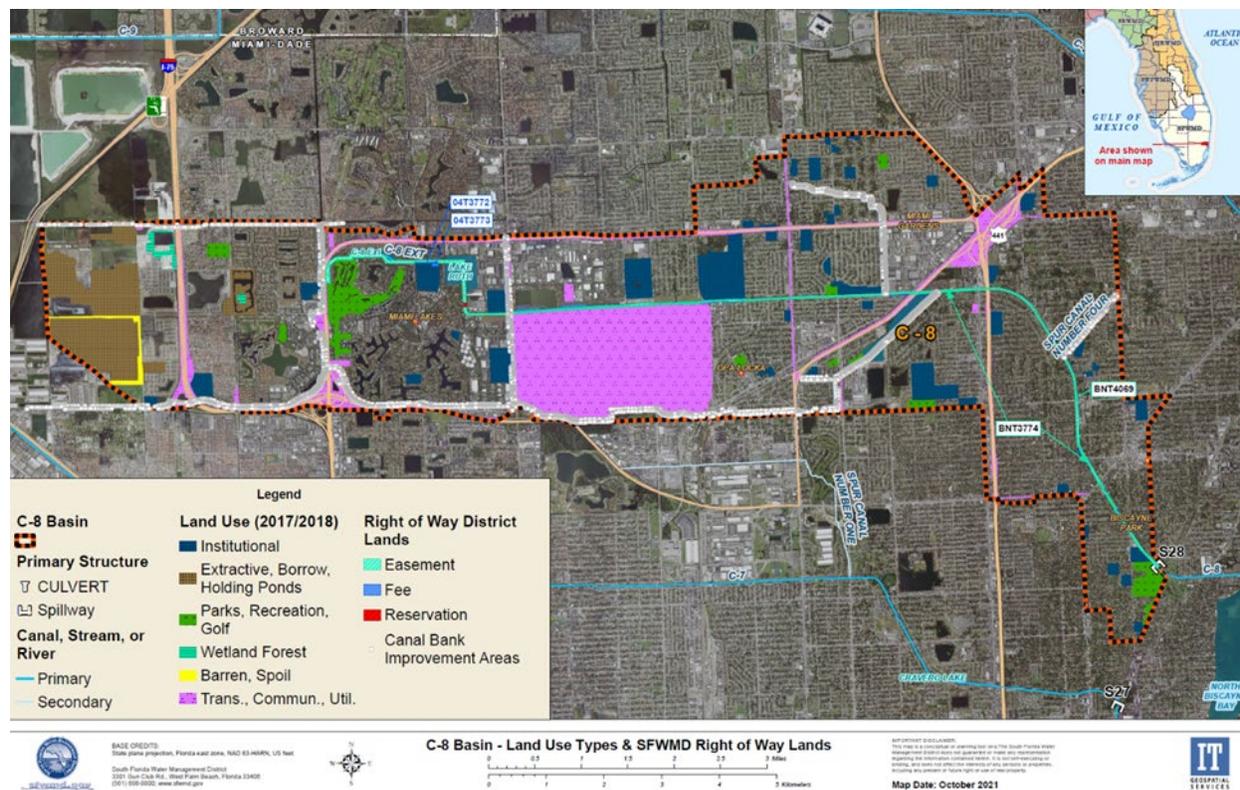
98 The initial step for assessing and implementing nature base solutions, as being proposed in this plan
99 document, is to map available opportunities within a given basin through the analysis of land use maps
100 (Figure 4-2) for the subject basin (step 1). A modeled flood layer can be added to the map to help identify
101 portions of the basin that are more vulnerable to flooding. The map can also help to identify all lands within
102 the basin that could potentially be used for implementing NBS. These lands can include multiple types of
103 land uses, such as institutional, extractive/borrow/holding pond areas, parks and recreation, wetlands, spoil
104 areas, and District-owned Right-of-Way lands. Each parcel identified on the land use map can then be
105 examined to determine ownership, size, elevation, and proximity to the flood control system.

106 Step two involves selecting suitable NBS that can be implemented on the parcels identified as potential
107 sites for NBS. For example, in the case of the C-8 Basin project, a municipal golf course was selected as a
108 potential site for a temporary detention area for low recurrence interval storm events. Once NBS have been
109 selected, an NBS implementation processes can be designed (step 3), and all stakeholders can be engaged
110 to negotiate partnership opportunities and land use agreements (step 4). From there, project planning,
111 funding and ultimately implementation can proceed (step 5). Step 6 includes designing and implementing
112 a monitoring program to evaluate the success of the NBS in providing benefits and co-benefits such as
113 increased flood protection, water supply and/or water quality improvements. Finally, if the NBS proves
114 successful in providing significant benefits, the NBS can be upscaled and applied throughout the basin
115 and/or regionally across basins. These seven steps are summarized below:

116

117

1. Identify Opportunities (such as available land)
2. Select and assess NBS and related actions
3. Design NBS implementation processes
4. Engage stakeholders, communicate co-benefits, and establish partnerships
5. Implement NBS, upon funding strategy definition
6. Monitor and evaluate co-benefits across all stages
7. Transfer and upscale NBS



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119 **Figure 4-2.** Land use types and SFWMD Right of Way lands within the C-8 Basin in Miami-Dade County.

120 **Process for Evaluating NBS - Estimating Direct and Indirect Benefits**

121 The process for evaluating the NBS benefits can use multiple tools that may include simple objective
 122 comparisons, professional estimates, standard engineering methods, empirical methods, combined
 123 hydrologic and hydraulic (H&H) models, and/or stand-alone hydraulic models. Each project, whether
 124 nature-based or gray infrastructure, should be evaluated for its ability to meet project objectives and the
 125 primary problem(s) it is intended to solve (flood control, water supply, water quality, environmental
 126 restoration, or combination thereof). Once the assessment for the project’s main intended purpose is
 127 confirmed, the project may also be evaluated relative to more comprehensive benefits related to District’s
 128 missions and incorporating stakeholder projects and components. The evaluation of NBS will also include
 129 considerations of operational impacts associated with the feasibility of project implementation to
 130 maintenance activities and impacts to the regulatory classification of NBS assets relative to the project
 131 design objective, in cases where NBS are paired with gray infrastructure.

132 This section provides a general assessment of methodologies for projects with flood control benefits.
 133 Evaluations and tools selected are dependent upon the scale of the problem and the scale of the proposed
 134 improvement project. For instance, a basin-wide H&H model and/or regional simulation model are tools
 135 that can provide a good evaluation of a large-scale storage or constructed wetland project. Standard
 136 calculations and additional modeling within the project impact area might be used to identify and implement
 137 NBS and green infrastructure. However, some NBS projects may be too small to be entered into a regional
 138 scale model capable of estimating the benefit of more localized projects. In this example, the tools selected
 139 to evaluate the flood damage reductions of the proposed project may need to be professional estimates
 140 calculations in lieu of modeling. Examples of assessment methodologies for flood control projects are listed
 141 in Table 4-2.

142

143 **Table 4-2.** Examples of assessment methodologies for flood control projects.

Water Management Topic		NBS	Corresponding Gray Infrastr. Solution	Assessment Methodology Examples (scale dependent)
Flood Control	River/canal flood control	Reconnecting rivers/canals to floodplain	Levees and water control structures	<ul style="list-style-type: none"> • H&H model for large scale projects • Standard engineering method to quantify additional storage
		Wetland restoration/conservation		<ul style="list-style-type: none"> • Standard engineering method to quantify additional storage
		Constructed wetlands/Flow Equalization Basin		<ul style="list-style-type: none"> • H&H model for large scale projects • Standard engineering method to quantify additional storage
		Living Shorelines/riparian buffers		<ul style="list-style-type: none"> • Hydraulic models for large scale projects • Professional estimates • Empirical Methods
	Urban stormwater runoff	Green spaces	Urban stormwater infrastructure	<ul style="list-style-type: none"> • Standard engineering calculations and impact area specific modeling • Empirical Methods
		Permeable surfaces		<ul style="list-style-type: none"> • Standard engineering calculations and impact area specific modeling • Empirical methods
		Green roofs		<ul style="list-style-type: none"> • Professional estimates • Empirical methods
	Coastal flood control	Protecting/restoring mangroves, marshes, and dunes	Sea walls/forward pumps	<ul style="list-style-type: none"> • Hydraulic models for large scale projects • Professional estimates
		Protecting/restoring reefs		<ul style="list-style-type: none"> • Empirical methods

144 Performance Metrics for NBS

145 Performance metrics (PMs) are very useful tools for assessing a project's success, in addition to
 146 estimation of benefits. A performance metric is an element or component of the natural system or human
 147 environment that is expected to be influenced by the project to be evaluated or monitored as representative
 148 of a class of responses to implementation of the project. They are project-specific and should be integrative
 149 of multiple aspects of the expected project result.

150 PMs accomplish two evaluation goals 1) evaluation of expected project performance and 2) assessment
 151 of actual project performance. The first occurs during the project planning phase to assess the viability and
 152 cost/benefit of the project. The second monitors the implemented project over time and compares actual
 153 outcome to expected outcome. The PMs for the two goals may be and likely will be different.

154 Identifying appropriate PMs, as summarized in Table 4-3 requires data collection both before and after
 155 project implementation and a general understanding of the innerworkings of the system. For example, for
 156 the C-8 Basin project, a potential PM would be turbidity of the water column. It is an integrative measure
 157 of basin runoff, erosion, and a water quality parameter that impacts aquatic habitat. To assess the project's
 158 success, turbidity data under multiple conditions (before and after rain events) both before and after project
 159 implementation will be needed. In addition, a suite of additional parameters will need to be collected to
 160 fully assess the impact of the project. With this information the following evaluations can be made:

- 161 1. Estimate direction and magnitude of change in performance metric from current state over the
 162 expected timeframe of benefit.
- 163 2. Compare current performance measure status with its desired trend and target.
- 164 3. Evaluate consistency of monitoring results with anticipated results.
- 165 4. Determine if unanticipated events are indicated.
- 166 5. Describe how these events are affecting desired outcome.

168 **Table 4-3.** Potential PMs for NBS projects, likely availability of data pre-project, and the relative effort
 169 of data collection post-project.

Performance Metric	Pre-project data availability	Post-project data collection effort
Salinity	High	Low
Turbidity	Medium	Low
Chlorophyll a	Medium	Medium
Nutrients	Medium	Medium
Flooding Frequency and Duration	Medium	Medium
Stage	High	Low
Flow	High	Low
Evapotranspiration	High	Medium
Biological Health & Biodiversity	Medium	Medium
Floodplain Connectivity	High	High
Wildlife utilization	Very low	High
Bank Stability	Low	Medium
Shoreline Change	Medium	Medium

170 **Resiliency Projects with Nature-Based Solutions**

171 Nature-based solutions are an important component of resiliency projects as they provide multiple benefits
172 for both people and the environment. Projects in this plan document that include NBS are listed below and
173 are detailed in Chapter 9. As we continue to develop priority resiliency projects, NBS will be incorporated
174 into traditional “gray” infrastructure to make our system more resilient. NBS are becoming increasingly
175 important in building resilient communities, as they offer a cost-effective and sustainable way to mitigate
176 the impacts of climate change and improve the ability of cities to withstand and recover from natural
177 disasters. These solutions leverage the power of nature, such as wetlands, forests, and green spaces, to
178 provide a range of ecosystem services that enhance the resilience of communities. For example, they can
179 reduce the risk of flooding by absorbing excess water, prevent erosion, filter pollutants, and provide shade
180 to reduce urban heat island effects. Moreover, NBS all have co-benefits such as improving air and water
181 quality, supporting biodiversity, and enhancing the overall livability of urban areas.

- 182 1. Building Resiliency with Green and Gray Infrastructure, C-7 Basin of Miami-Dade County
- 183 2. Building Resiliency with Green and Gray Infrastructure, C-8 Basin of Miami-Dade County
- 184 3. Building Resiliency with Green and Gray Infrastructure, C-9 Basin of Broward and Miami-Dade
185 County
- 186 4. C-9 Canal Widening and Enhancement with Nature-Based Features Project
- 187 5. EMMA
- 188 6. MEME
- 189 7. Corbett WMA Hydrologic Restoration and Levee Resiliency

Chapter 5:

Ecosystem Restoration Projects and Resiliency

ECOSYSTEM RESTORATION EFFORTS

The South Florida Water Management District (District of SFWMD) has several programs that facilitate ecosystem restoration either directly or indirectly. One of the most important, the Comprehensive Everglades Restoration Plan (CERP, or the Plan), is designed to restore, preserve, and protect the South Florida ecosystem while providing for other water-related needs of the region including water supply and flood protection. Restoration aims to achieve and sustain the essential hydrological and biological characteristics that defined the Everglades ecosystem. To ensure project objectives are met, project-level performance measures and monitoring plans, and system-wide performance measures and monitoring under the CERP's interagency Restoration, Coordination, Verification (RECOVER) program will assess ecosystem response to project implementation. With the uncertainty of impacts to these ecosystems from increases in precipitation, sea-level rise (SLR), and other effects of climate change, monitoring is critical to identifying adaptive management opportunities and to ensure the whole system is resilient in the long-term. Each CERP project has individual components with varying objectives including wetland restoration, water storage, and water quality treatment; improved/reconnected hydrology and movement of freshwater for both environmental and human uses; and improved or restored habitat.

Another program, specific to the Everglades, is Restoration Strategies for Clean Water for the Everglades. This program's goal is to reduce phosphorus loading to the Everglades so that the historic plant and animal community may be restored. This is accomplished in two ways, by modifying and expanding existing Everglades Stormwater Treatment Areas (STAs) and by research to better understand phosphorus removal processes for improved management of the STAs. Everglades STAs are large, constructed wetlands designed to maximize phosphorus removal from surface water and will total approximately 64,000 acres when Restoration Strategies is complete. STAs not only provide clean, low-nutrient water to the Everglades, they also provide significant carbon sequestration through peat accumulation.

The Northern Everglades and Estuaries Protection Program (NEEPP) focuses on protecting the watersheds of Lake Okeechobee, the Caloosahatchee River and Estuary, and the St. Lucie River and Estuary. Projects focus on improved water quality and water delivery to sensitive ecosystems. This includes working closely with Florida Department of Environmental Protection and Florida Department of Agriculture and Consumer Services to implement nutrient source control measures to help meet total maximum daily loads (TMDLs) established for these water bodies.

Current and future projects will work in conjunction with other infrastructure projects, habitat restoration, and operational plans. These include Foundation Projects such as Kissimmee River Restoration, Modified Water Deliveries to Everglades National Park, C-111 South Dade Project, and Tamiami Trail Next Steps. The projects restore water flow, water quality, and habitat to critical areas of the District and improve our resiliency to climate change.

All of these programs working system-wide, along with nature-based solutions (NBS), as introduced in the previous chapter, help restore our ecosystems, create healthy environments, and make them more resilient to climate change. Each, in their own way, provides ecosystem services that will bolster south Florida from the negative impacts of SLR, changing rainfall patterns and water availability, flooding, and loss of habitat. Below are examples of specific projects that fall under these programs.

42 **NORTHERN ESTUARIES AND EVERGLADES**

43 Along the Atlantic Coast, the Indian River Lagoon-South Project includes the C-23, C-24, C-25, and
44 C-44 Reservoirs and STAs for water storage and treatment of St. Lucie Watershed runoff. Water quality
45 improvement and reduction of damaging freshwater flows will provide more suitable conditions (e.g.,
46 salinity) for aquatic organisms including seagrasses and oysters, which are critical for creating buffer zones
47 for storm surge and wave erosion. On the Gulf Coast, the C-43 Reservoir and associated projects will
48 provide the same benefits to the Caloosahatchee River and Estuary.

49 North, east, and west of Lake Okeechobee are water storage and water quality improvement projects
50 that will reduce nutrient loading and improve water delivery to the Lake. Water clarity and depth are key
51 components to a healthy submerged aquatic vegetation habitat critical for lake organisms. Lake levels also
52 drive the amount of water sent east, west, and south, which impact the estuaries and the Everglades health.
53 Some projects include the Nubbin Slough STA, Lower Kissimmee Basin Stormwater Treatment, and
54 Grassy Island Flow Equalization Basin (FEB).

55 South of Lake Okeechobee, Restoration Strategies is improving STA performance to reduce
56 phosphorus loading to the Everglades. At its completion in 2025, 6,500 additional acres of STA will have
57 been built and an additional 116,000 acre-feet of water storage will be available in FEBs. In addition, the
58 treatment area in existing STAs will be increased through land leveling efforts. Alongside these projects,
59 District scientist have implemented a robust Science Plan designed to evaluate the mechanisms of
60 phosphorus removal to improve STA performance and management decision making. To date, scientists
61 have completed nine of 21 studies. All studies will be completed at the end of 2024.

62 **CENTRAL AND WESTERN EVERGLADES**

63 The Central Everglades Planning Project (CEPP) includes the A-2 Reservoir (otherwise known as the
64 Everglades Agricultural Area (EAA) Reservoir) and A-2 STA to store and treat Lake Okeechobee
65 Regulatory Releases prior to sending flows to the Everglades; CEPP North to restore flows into
66 northwestern Water Conservation Area (WCA) 3A, move water south, and construct tree island habitat;
67 CEPP South to improve connectivity between WCA-3A/3B and northeast Shark River Slough; and CEPP
68 New Water, to retain groundwater seepage from CEPP flows into northeast Shark River Slough. Providing
69 increased hydration with low-nutrient water will result in greater peat formation, and thus carbon storage
70 and increased marsh platform elevation to reduce impacts of SLR. Additionally, the Fish Habitat
71 Assessment Program (FHAP) monitors seagrasses in Florida Bay, following trends in salinity resulting
72 from insufficient freshwater baseflow.

73 The Western Everglades Restoration Project (WERP) will re-establish ecological connectivity, reduce
74 the severity and frequency of wildfires, and restore low nutrient conditions through alterations to existing
75 canals and levee to allow for sheetflow. Water will move from the Western Feeder Canal towards Big
76 Cypress National Preserve restoring freshwater flow paths, restoring water levels, and providing
77 connectivity for flora and fauna. The reduction in severity and frequency of wildfires and increased water
78 availability will assist with carbon capture and the sustainability of the ecosystem.

79 The Picayune Strand Restoration Project (PSRP) is removing historic roads and restoring sheetflow
80 across 55,000 acres of natural habitat, and maintaining flood protection for adjacent communities, with
81 connections to downstream linkages to other systems e.g., Everglades National Park, Collier Seminole State
82 Park, Ten Thousand Islands National Wildlife Refuge, and Fakahatchee Strand State Preserve. Improved
83 freshwater delivery to estuaries such as Faka Union Bay and Pumpkin Bay will improve habitat for oysters
84 and seagrass beds, critical for storm protection against erosion.

85 SOUTHERN EVERGLADES

86 Broward County Water Preserve Areas reduce groundwater seepage from Water Conservation Areas
87 3A & 3B, improves water supply, and prevents saltwater intrusion. Biscayne Bay Coastal Wetlands (Phase
88 1; BBCW) rehydrates coastal wetlands, reducing freshwater point source pollution releases, and
89 redistributes surface water into Biscayne Bay. The Biscayne Bay and Eastern Everglades Restoration
90 (BBSEER) project is currently in the planning phase and will include the C-111 Spreader Canal West and
91 BBCW Phase II to improve the quality, quantity, and distribution of freshwater to Biscayne Bay, improve
92 glades habitat in the Model Lands and Southern Glades, and improve resiliency of coastal vegetation and
93 habitat as they face changes in sea-level. An Adaptive Foundational Resilience (AFR) Performance
94 Measure is being developed as a landscape-scale, holistic evaluation of the native mangrove and coastal
95 marsh vegetation's ability to adapt to saltwater intrusion due to SLR by responding to the increased
96 sheetflow volumes, reduced porewater salinities and improved hydroperiods predicted to occur with
97 BBSEER restoration. There are two pilot studies needed to demonstrate how to implement the AFR
98 throughout Florida. One is a small-scale multi-plot assessment of how mangroves will respond to a variety
99 of drivers, but with a focus on nutrients and the possible use of re-use water for restoration. This pilot is
100 called: Mangrove Experimental Manipulation Exercise or MEME. The other pilot study is a large-scale
101 assessment of Thin Layer Placement in Scrub Mangroves with a focus on using clean dredge material for
102 enhanced elevation and soil accretion to enhance flood protection and foster natural adaption to SLR. This
103 pilot is called: Everglades Mangrove Migration Assessment (EMMA).

104 Here are the questions that these two pilot studies, described in **Chapter 9**, will address, when sources
105 of funding are identified:

106 Q1: Does phosphorus or level of planting density amendment contribute to the greatest
107 ecosystem service value (plant production, nutrient accumulation, and C sequestration) and
108 resilience (increase in sediment elevation that exceeds rate of SL) with shallow sediment
109 amendments?

110 Q2: Does phosphorus enhance ecosystem service value and resilience the same
111 regardless of planting density?

112 Q3: How does phosphorus and level of planting density amendment influence ecosystem
113 service value and resilience with a moderate level sediment amendment under different
114 salinity conditions?

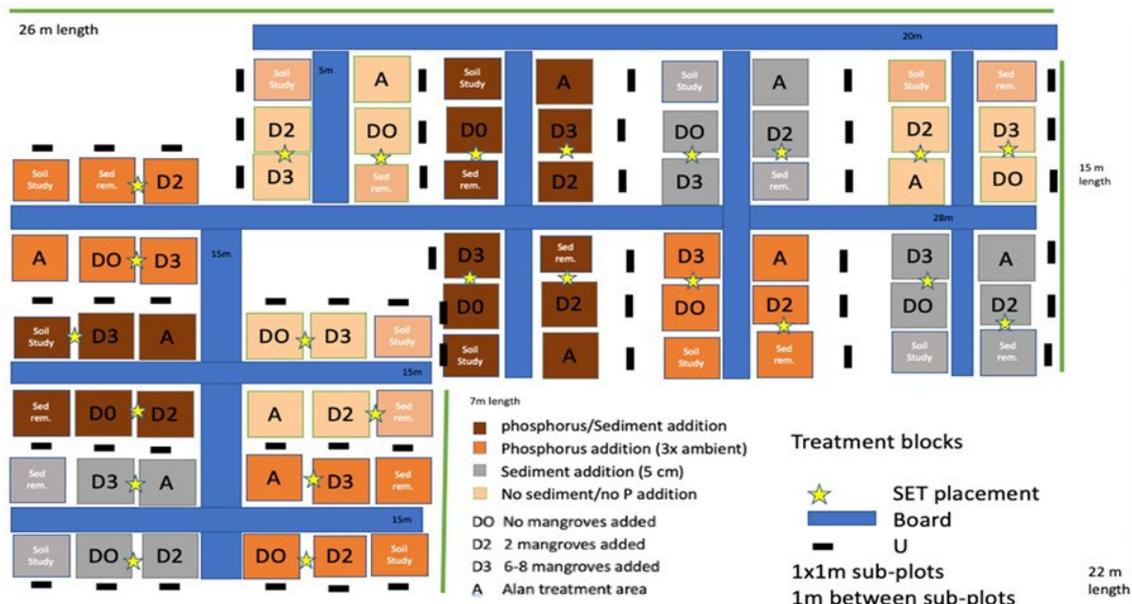
115 Q4: What combinations of sediment, phosphorus and plant density amendments confer
116 the greatest ecosystem service value and resilience Do these vary with salinity condition?

117 To plan for a sustainable South Florida ecosystem, it is important to identify ecological vulnerabilities
118 to SLR and ask how we might direct water management to minimize saltwater intrusion, peat collapse
119 (Sklar et al, 2019) and land loss. SLR projections for the next 50 years will threaten the structure and
120 function of coastal wetlands in South Florida and there is agreement among coastal scientists that sea level
121 is rising at rates that will inundate most lowlands distributed along the coasts (Ross et al 2000; Sweet et al,
122 2017, Sklar et al, 2019; Sklar et al, 2021).

123 These demonstration-scale pilot studies are nature-based management measures to increase coastal
124 mangrove elevation and enhance net belowground storage of carbon. They will document the efficiency
125 and effectiveness of Thin Layer Placement to increase the adaptive capacity of Florida's coastal wetlands
126 and keep up with SLR. It will assess the value of reuse water. Results are applicable to areas throughout
127 the Gulf and Atlantic Coasts of Florida, where direct preservation, enhancement, and restoration of
128 mangrove and other vegetative communities, will build coastal resiliency, reduce storm surge damage, and
129 create habitat for a large variety of fish and wildlife species.

130

131
132
133



134

BISCAYNE BAY

135

136 The SFMWD acknowledges the delicate and valuable ecology of Biscayne Bay and the need for short-
 137 term and long-term efforts from State, regional and local governments to address the effects from freshwater
 138 releases on water quality and ecology of the bay. The District is engaged in multiple ongoing efforts to
 139 specifically address these issues. These efforts range from assessment of flood control operation impacts
 140 on water quality of the bay to tool development through a DEP funded grant with Tulane University to
 141 develop a comprehensive hydrodynamic model with water quality capability for simulating impacts of
 142 freshwater flows on quality in the bay and effect of multiple potential adaptation strategies.

143 The District, working with other agencies with a shared interest in addressing water quality in the Bay,
 144 is committed to identifying and implementing strategies that increase the resiliency of the entire flood
 145 control system through a coordinated effort with our partners and reducing the reliance on infrastructure in
 146 natural areas through long-term restoration. The District will partner with Miami-Dade County on the S-27
 147 Coastal Structure Resiliency project to ensure that the proposed infrastructure projects adhere to the
 148 recommendations of the Biscayne Bay Task Force and prioritize Biscayne Bay health and resilience through
 149 monitoring. The District is also partnering with Miami-Dade County and FDEP to identify and pilot
 150 innovative technologies that can be implemented to target nutrient removal, ultimately protecting the health
 151 of water systems upstream and downstream of District conveyance structures. Together, these projects
 152 along with NBS and Green Infrastructure, as recommended by the Biscayne Bay Task Force create multi-
 153 faceted pathways that deliver protection to Biscayne Bay.

154

ECOSYSTEM RESTORATION PROJECTS BENEFITS AND POTENTIAL CARBON SEQUESTRATION

155
156

157 As summarized above,
158 comprehensive restoration efforts have
159 been underway for the past 20 plus years
160 by the District, in collaboration with
161 local, state, and federal partners, to
162 protect and restore South Florida's
163 ecosystems. These systems are
164 represented by four watersheds:
165 Kissimmee River, Lake Okeechobee,
166 Everglades, and Coastal Systems. The
167 restoration of these vital parts of South
168 Florida's ecosystems have been
169 supporting the region's overall
170 resiliency and the District's ability to
171 better manage water for the benefit of
172 people and the environment, with
173 consideration of anticipated SLR and
174 extreme weather events into the future.



175 These efforts will continue to increase the ecosystem's future resiliency in the face of warmer temperatures
176 and other climate change impacts.

177 In particular, the restoration of beneficial freshwater flows throughout the system slows down saltwater
178 intrusion, promoting more sustainable aquifer recharge rates, healthier estuaries and bays, more stable
179 coastlines, reduced marsh dry outs and greater coastal resiliency. Ecosystem restoration also results in
180 increased quantity and quality of freshwater flow to and within the Everglades, higher flexibility and storage
181 options to address water management seasonal needs, increased wetland acreage, and increased
182 connectivity to coastal ecosystems. These initiatives also help mitigate the effects of climate change through
183 carbon capture and storage in peat soils.

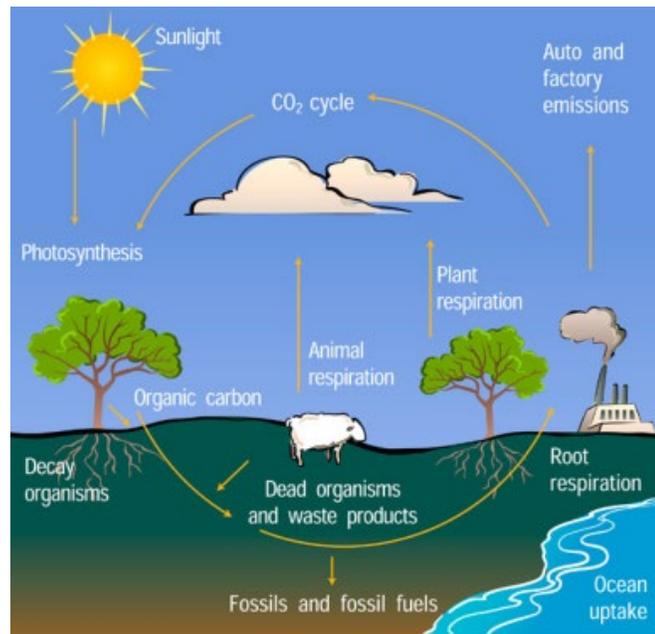
184 In addition to emphasizing the importance of continuing ecosystem restoration efforts and account for
185 their resiliency benefits, these efforts might seek to maximize the carbon uptake and storage capacity of
186 wetlands and coastal ecosystems. The restoration and preservation of natural systems enhances organic
187 carbon storage by reinstating the sedimentary biogeochemical conditions and soil stability in disturbed sites
188 and increasing the living biomass and its capacity to sequester carbon dioxide (CE Lovelock et al., 2017).
189 Restoration of historic flows to the Everglades, as part of CERP and the creation and improvement of
190 Everglades STAs through Restoration Strategies, has a large carbon uptake potential by mitigating for
191 seagrass die-off, peat collapse, loss of ridge and slough habitat, subsidence, and restoration of agricultural
192 lands back to wetlands. Ecosystems within the restoration project footprint that can uptake and store
193 atmospheric carbon include STAs, WCAs, mangrove forests, and submerged aquatic vegetation beds,
194 including seagrass.

195 MONITORING APPROACH

196 Currently, the District does not collect
 197 carbon data as a matter of routine. To dial in
 198 the carbon uptake and storage calculations,
 199 data collection efforts would need to be
 200 employed for each of the restoration projects
 201 to better represent their associated mitigation
 202 benefits and estimate resilience benefits.
 203 These include the following:

- 204 • Soil carbon characteristics: measure
 205 soil bulk density and carbon
 206 concentration at multiple depth
 207 increments to capture short-term and
 208 long-term carbon storage.
- 209 • Soil accretion: use surface elevation
 210 tables and feldspar marker horizons
 211 to measure soil surface changes and
 212 vertical accretion.
- 213 • Eddy Flux Towers: An Eddy flux
 214 tower, also known as an eddy covariance tower, is a tall tower equipped with sensors that
 215 measure the exchange of gases, such as carbon dioxide, methane, and water vapor, between the
 216 atmosphere and the land surface below. The tower has an anemometer (wind speed sensor) and
 217 a sonic anemometer (measures wind speed and direction) at the top that measure the turbulence
 218 of the air as it moves past the tower. These measurements allow scientists to calculate the
 219 vertical and horizontal movement of gases. By combining these measurements with the
 220 turbulence data, scientists can calculate the rate of exchange of these gases between the land
 221 surface and the atmosphere. This information is important for understanding the role that
 222 ecosystems play in regulating the Earth's climate. For example, the rate of carbon dioxide
 223 uptake by plants during photosynthesis can be measured using an eddy flux tower, allowing
 224 scientists to track how much carbon dioxide is removed from the atmosphere by plants.
- 225 • Remote sensing data: The District is actively investigating the potential for using satellite,
 226 radar, and lidar imagery to capture changes in plant biomass and land cover to determine the
 227 potential for carbon uptake. The use of satellite and radar imagery can provide a
 228 complementary approach to enhance the District's current planning projects for carbon
 229 monitoring and further improve the accuracy and efficiency of carbon monitoring.

230 Employing these measurements across District restoration projects will provide accurate assessments
 231 of carbon capture and storage associated with the different ecosystem restoration efforts currently
 232 undertaken by the District and its partners, and better estimate their benefits to climate resiliency. A full
 233 description of the carbon monitoring plan can be found in Chapter 10 – Priority Planning Studies. This
 234 monitoring plan was developed in partnership with the Everglades Foundation and Florida International
 235 University.

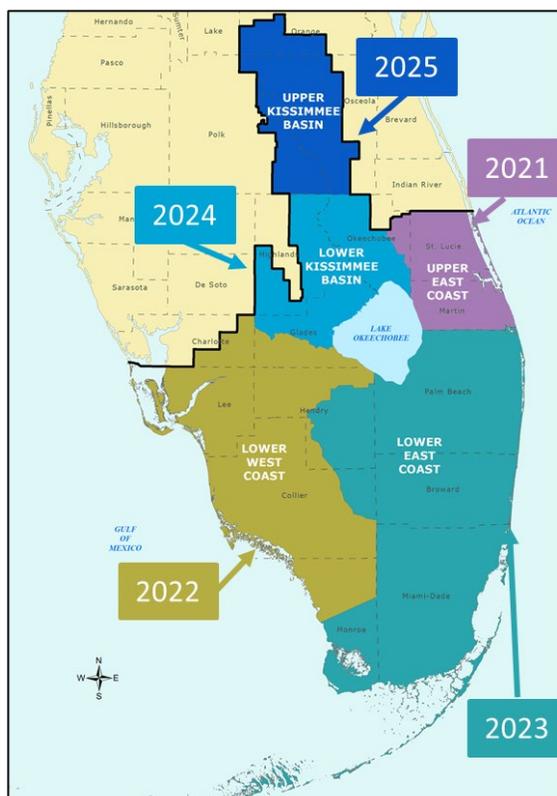


Chapter 6: Water Supply Resiliency

UNDERSTANDING OUR VULNERABILITIES

The South Florida Water Management District (District or SFWMD) is implementing initial efforts to better understand what our water supply vulnerabilities are as they relate to sea level rise (SLR), changing rainfall patterns and drought occurrences, increase in evapotranspiration rates and other related climate change impacts. These efforts include water supply planning, groundwater modeling, water resource protection, water conservation, alternative water supply development, regional and subregional water management, and saltwater interface mapping.

The SFWMD conducts water supply planning for five regions (Figure 6-1) encompassing the District: Upper Kissimmee Basin, Lower Kissimmee Basin, Upper East Coast, Lower East Coast, and Lower West Coast. Water supply plans (Plans) are developed in coordination with stakeholders and the public and look at least 20 years into the future and are updated every five years to stay current with growth trends. These Plans evaluate current and future water demands and identify water sources and strategies to meet these needs while sustaining water resources and the environment. These Plans help local governments and utilities in their facility and comprehensive planning efforts. Water supply plans include population and demand estimates and projections for at least a 20-year planning horizon, water source options, water resource evaluation and protection, proposed projects, and future water supply direction. As it is related to SLR, these Plans and projections consider saltwater intrusion, and future plans will evaluate SLR scenarios in a more comprehensive manner, through the development of a variable density groundwater modeling effort (see Water Supply Vulnerability Assessment in Chapter 10).



23

24 **Figure 6-1.** Regional Water Supply Plan Update Schedule and Respective Planning Areas.

25 To support water supply plans and other initiatives, the District has several groundwater models that
 26 simulate groundwater withdrawals and identify potential impacts to water resources. Currently, fresh
 27 ground water system models can evaluate drawdowns associated with those withdrawals. The East Coast
 28 Surficial Model (ECSM) is a density-dependent groundwater model that is currently under development by
 29 the District and will allow model runs to explicitly simulate the effects of SLR and potential movement of
 30 the saltwater interface, and climate change on the surficial groundwater system. The ECSM includes most
 31 of the LEC planning region and the entire Upper East Coast (UEC) planning region and will be completed
 32 in 2024. In addition, the Lower West Coast (LWC) planning region is included in the District's Lower West
 33 Coast Surficial/Intermediate Aquifer Systems Model (LWCSIM). In the future, following the completion
 34 of the ECSM, it is envisioned that the LWCSIM will be upgraded to be density dependent as well.

35 A Water Supply Vulnerability Assessment (WSVA) will utilize existing surface and groundwater
 36 modeling tools to evaluate the effects of SLR and climate change (e.g. rainfall and evapotranspiration
 37 patterns) on our water supplies (See Chapter 10). The outputs of the model runs will identify potential
 38 impacts to water resources and areas the District needs to focus identification of strategies and projects that
 39 can increase water supply resilience. The WSVA will be initiated later in 2023, with data preparation tasks,
 40 and has a 2-year estimated duration to complete. The WSVA will look beyond the traditional water supply
 41 planning efforts and 20-year planning horizon and incorporate additional climate scenarios and a longer
 42 planning horizon. This more detailed evaluation into the vulnerability of our water supply sources can help
 43 inform the development of new projects that will enhance the South Florida Region's water supply
 44 resiliency. This is part of an overall effort to help the District understand and plan around the complexities
 45 that factor into the current and future resilience of our water supplies.

46 RESPONDING RESILIENTLY

47 In parallel to assessing water supply vulnerabilities, and with the goal of ensuring that South Florida
 48 has consistent and safe water supply for current and future generations, the District has been employing
 49 three overarching project strategies: protecting existing water sources, investing in alternative water supply
 50 sources, and capturing excess water or wet-weather flows. These strategies are currently incorporated as
 51 part of water supply plan development among other District planning efforts.

52 Subsequent sections highlight existing resiliency-related projects within the District boundaries. Many
 53 of the projects highlighted below achieve the goals of more than one of the above strategies. They may also
 54 have originated from within different District responsibilities, though they are highlighted here to
 55 emphasize the effect they have on making South Florida's water supply systems more resilient.

56 PROTECTING EXISTING WATER SUPPLY

57 Protecting our existing water supplies is a resiliency strategy that ensures continual and safe water
 58 supply. In this section we'll highlight four of the District's protection focused strategies: Saltwater Interface
 59 Monitoring; Salinity Control Structures and Canal Operations (Figure 6-2); Regulatory Controls and Water
 60 Conservation.

61 The District develops saltwater interface maps at five-year intervals in our coastal aquifers based on
 62 salinity data from available monitor wells to determine the approximate location of the saltwater interface
 63 and any changes. These maps are published on the District's Website and presented in public workshops.
 64 The District also publishes chloride data and the saltwater interface maps on the [Resilience Metrics Hub](#).

65 The District maintains
 66 canal and groundwater levels
 67 in the regional water
 68 management system during the
 69 wet and dry seasons to ensure
 70 water supply demands needs
 71 are met, from urban demands
 72 to natural system.

73 Optimization of canal and
 74 groundwater levels through the
 75 operation of the District's
 76 salinity control structures
 77 minimize further inland
 78 movement of saltwater along
 79 the coast. The existing coastal
 80 structures were designed and
 81 built in the 1950s and are
 82 operated to maintain a pre-
 83 determined freshwater level in
 84 the canals, which locally
 85 increases the freshwater
 86 levels in the aquifer further

87 assisting with minimizing saltwater intrusion, especially during the dry season. Enhancements to Coastal
 88 Structures are being proposed as an important mechanism for salinity control in water supply management.
 89 The coastal Structures priority projects proposed in this plan (Chapter 9) will improve operational capacity
 90 and flexibility to further protect water supply sources into the future.

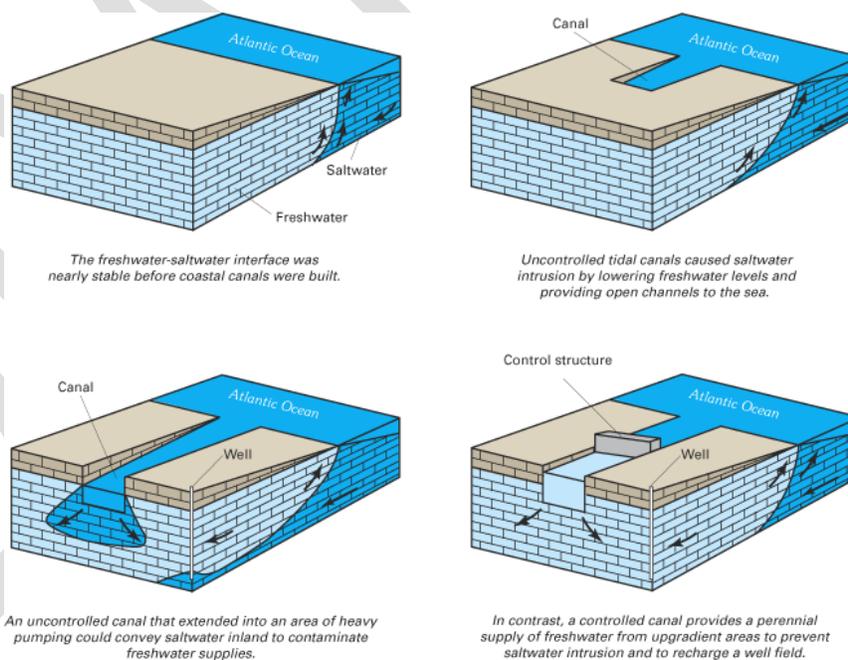


Figure 6-2. Diagram depicting the impact of canals and structures on saltwater intrusion.

91 Regulatory Control occurs through water resource protection rules such as Minimum Flows and Minimum
 92 Water Levels (MFL), Water Reservations, and Restricted Allocation Areas (RAA). These have been
 93 adopted for several water resources in the District, including Lake Okeechobee, Kissimmee River, Biscayne
 94 Bay, Loxahatchee River, St. Lucie Estuary and others. The District's regulatory programs are designed to
 95 support reasonable-beneficial uses of water, while implementing criteria needed to protect water resources
 96 from harm.

97 MFLs are defined as the minimum flows or minimum water levels, adopted by the District Governing Board
 98 pursuant to Sections 373.042 and 373.0421, Florida Statutes, at which further withdrawals would be
 99 significantly harmful to the water resources or ecology of the area. A water reservation is a legal
 100 mechanism, authorized by Section 373.223(4), Florida Statutes, to set aside water from consumptive uses
 101 for the protection of fish and wildlife or public health and safety. When a water reservation rule is in place,
 102 the volume and timing of water at specific locations is protected for the natural system.

103 Restricted Allocation Areas designated by
 104 the District are one regulatory mechanism
 105 designed to limit future uses beyond that
 106 which is already permitted to prevent harm
 107 to water resources. An example is the
 108 Lower East Coast Restricted Allocation
 109 Area Rule (2007), designed to protect
 110 existing supplies and prevent further harm
 111 to natural systems, as regulatory
 112 components of the Northwest Fork of the
 113 Loxahatchee River MFL and Everglades
 114 MFL recovery strategies. The RAA limits
 115 the allocation of water from these
 116 waterbodies to a base condition water use
 117 as described in the Applicant's Handbook
 118 (SFWMD 2021a).

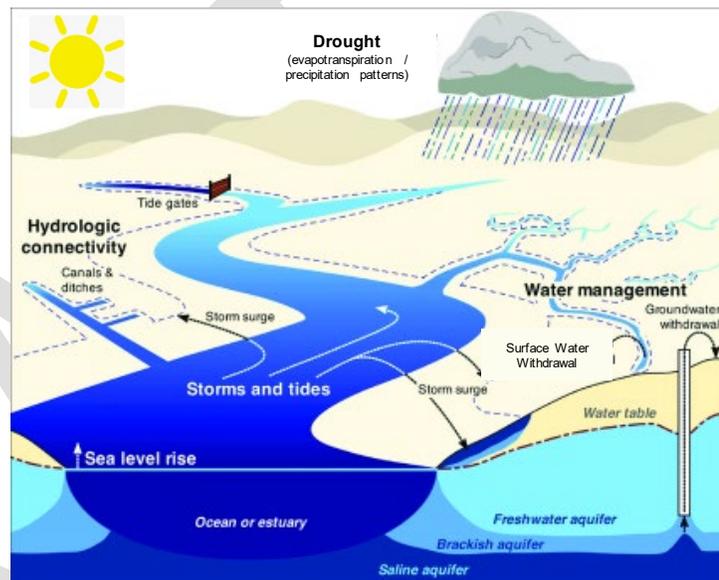


Figure 6-3. Diagram depicting elements of the coastal hydrologic cycle.

119 Moreover, the District actively promotes
 120 water conservation to incentivize efficient
 121 use of water, and recognition that
 122 conservation can extend available supplies
 123 while deferring the need for more expensive alternative water supply sources. The District has many
 124 programs, partnerships, and materials dedicated to promoting water conservation across all use classes and
 125 sources. These programs range from demand-reducing strategies like Florida Friendly Landscaping to the
 126 commercially focused Florida Water Star. These and other District conservation programs incentivize users
 127 to be intentional about water consumption by providing grants, rebates, and other funding sources, as well
 128 as guidance and conservation information. Reductions in per-capita consumption have been observed in
 129 several regions in South Florida because of water conservation efforts being advanced by the District,
 130 utilities, and local governments.

131 INVESTING IN WATER CONSERVATION AND ALTERNATIVE WATER 132 SUPPLY SOURCES

133 In addition to protecting existing water resources, the District also encourages the development of new
 134 or alternative water sources to reduce dependence on freshwater resources and meet growing demands for
 135 water. These solutions include the development and implementation of increased use of reclaimed water,
 136 use of brackish groundwater sources such as the Floridan Aquifer System (FAS), additional surface water
 137 storage options, and utilizing desalination of sea water or other high salinity sources. These solutions have
 138 been implemented across the District in various capacities and have been tried and proven as a sustainable

139 resilient strategy for many communities around the world. Since 1997, the District in cooperation with
 140 FDEP, has provided over \$243 million in state cost-share grant funding towards 530 Alternative Water
 141 Supply (AWS) projects that produced 523 million gallons of capacity per day. . Additionally, the District
 142 contributed approximately \$9 million toward 260 projects water conservation projects that have an
 143 estimated water savings of 5 billion gallons of water per year, or 13.6 million gallons of water per day,
 144 since 2003.

145 Florida is a national leader in water reuse, reusing nearly 900 mgd of reclaimed water to conserve
 146 freshwater supplies and recharge freshwater aquifers. There are over 100 reuse facilities in the District
 147 reusing about 300 mgd of reclaimed water for a beneficial purpose including irrigation of golf courses,
 148 residential lots and other green space, ground water recharge, environmental enhancement, and industrial
 149 purposes. However, there is approximately 590 mgd of potentially reusable water that is currently being
 150 disposed of through ocean discharge or deep injection wells in the District, primarily in the Lower East
 151 Coast. The biggest obstacle to further development is identification of feasible reuse options in highly
 152 urbanized areas, the cost of treatment to meet water quality requirements and related infrastructure, and
 153 funding.

154 There are over 40 reverse osmosis water treatment plants treating brackish groundwater from the FAS
 155 throughout South Florida with a combined capacity of approximately 300 mgd. Utilizing brackish
 156 groundwater from the FAS to meet future demands reduces the stress on existing surficial aquifer system
 157 resources, thereby reducing the potential for increased saltwater intrusion. The FAS is geologically isolated
 158 in South Florida from the overlying surficial aquifer system and due to its already brackish water quality
 159 and depth nearly 1,000 ft below the surface, it doesn't face the same acute climate risk from SLR as the
 160 freshwater surficial aquifer system. Though brackish water sources and related treatment systems are more
 161 expensive to operate, less efficient, and produce a brine concentrate needing disposal, use of brackish water
 162 is a sustainable water source as it has a smaller environmental impact with manageable waste streams, in
 163 addition to reducing demand on the surficial aquifer system. Utilities are planning to increase withdrawals
 164 from the FAS to meet projected growth beyond current freshwater allocations. In the past 20 years,
 165 desalination capacity in the SFWMD has increased by 480% through the addition of 28 reverse osmosis
 166 plants, mostly brackish groundwater treatment systems.

167 Finally, seawater desalination is a potential option explored by coastal communities throughout the
 168 world. Unfortunately, the relatively higher cost and energy associated with seawater desalination treatment
 169 processes reduce its utilization and increase its carbon footprint. Yet, seawater desalination remains as an
 170 option for water supply development under more critical future conditions. However, advances in
 171 desalination technology are decreasing energy demands and increasing recovery efficiencies. There are two
 172 seawater desalination facilities in the District both located in the Florida Keys, serving primarily as a back-
 173 up supply.

174 Below are a couple of examples of development of alternative water supplies in the District:

- 175 • Reuse Facilities: Oasis Water Reclamation Facility
 176 - The District's alternative water supply funding
 177 program has contributed more than \$100 million to
 178 reclaimed water projects including the City of
 179 Pompano Beach's Oasis Water Reclamation
 180 Facility – This facility has reused over 24 billion
 181 gallons of reclaimed water over the last 3 decades.
- 182 • Brackish Groundwater: Orlando Southeast Water
 183 Treatment Plant Lower Floridan Aquifer Wellfield
 184 Phase 1 – In 2021, the Orlando Utilities
 185 Commission received a District's brackish water
 186 alternative water supply development grant. The



Figure 6-4. Picture of reclaimed water "purple pipes".

187 total project cost is expected to be over \$95 million and is expected to provide the Orlando area
 188 with an additional 10 MGD of public water supply. Examples of municipalities using brackish
 189 sources along the coast include Jupiter and Lake Worth Beach.

- 190 • Seawater Desalination: Florida Keys Aqueduct Authority (FKAA) Kermit H. Lewin RO Facility –
 191 The existing seawater desalination facility at this site will be replaced with a new facility that will
 192 double the current desalinated seawater supply to 4 MGD. Approximately 75% of the plant was
 193 funded by a hurricane disaster recovery grant and its specifications are resiliency focused.

194 **SAVING FOR A NON-RAINY DAY**

195 Retaining wet-weather flows to use when its dry is one of the
 196 most tried and proven resiliency strategies for water supply and
 197 is another alternative water supply development strategy being
 198 supported by the District. From a regional perspective, the
 199 District captures surplus water primarily through the operation of
 200 the regional water management system. This system includes
 201 reservoirs and WCAs. Development of large-scale Aquifer
 202 Storage and Recovery (ASR), currently being designed and
 203 tested by the District north of Lake Okeechobee, will provide
 204 another option.

205 The District manages both natural systems and man-made
 206 reservoirs that serve as water supply primarily for the
 207 environment and to a much lesser extent water users such as
 208 water supply utilities and agricultural irrigation, among others.
 209 Natural systems used to retain surface water include Water
 210 Conservations Areas (WCA) / Water Management Areas
 211 (WMA), which are large swaths of land that retain water as well
 212 as facilitate groundwater recharge. Built-out reservoirs have been
 213 developed throughout the District and are often integrated into
 214 flood protection as a place for flood waters to be conveyed in
 215 addition to their water supply uses.

216 ASR wells store excess water primarily during the wet
 217 season into confined aquifer systems, saving it to be extracted
 218 during dry conditions. The District has a plan to construct up to
 219 55 ASR wells north of Lake Okeechobee as part of the
 220 Comprehensive Everglades Restoration Plan (CERP). There are existing ASR wells used by utilities for
 221 water supply, such as the wells in Boynton Beach, West Palm Beach, and Marco Island. In 2015 and 2018,
 222 the District published a comprehensive ASR study that confirmed further ASR development as a feasible
 223 solution to provide beneficial water storage and availability.

224 Below are examples of regionally focused water storage projects:

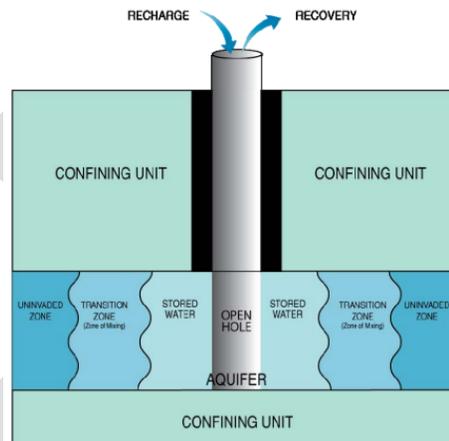


Figure 6-5. Graphic showing Aquifer Storage and Recovery (ASR) methodology.

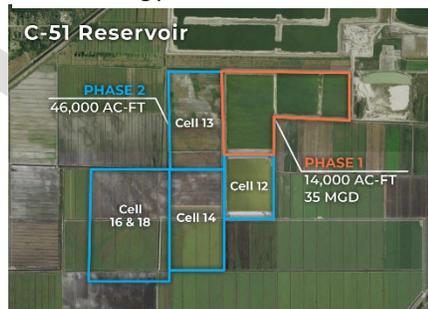


Figure 6-6. Plan view area of C-51 Reservoir project.

225 • ASR: Marco Island’s ASR wells – Marco Island utilizes four
 226 water supply options to meet drinking water and irrigation
 227 demands of the community: fresh surface water from Marco
 228 Lakes/Henderson Creek, brackish groundwater, reclaimed
 229 water, and surface water stored in ASR wells. Since 1997,
 230 Marco Island has developed seven ASR wells which store
 231 surface water from Marco Lakes/Henderson Creek during the
 232 rainy season for later use during the dry season. Marco Island
 233 estimates they have established a one-billion-gallon freshwater
 234 reserve in the brackish FAS through their ASR program. Marco
 235 Island recovers 2 to 5 mgd from the ASR wells during the dry
 236 season to meet consumer demand when surface water
 237 availability is limited.

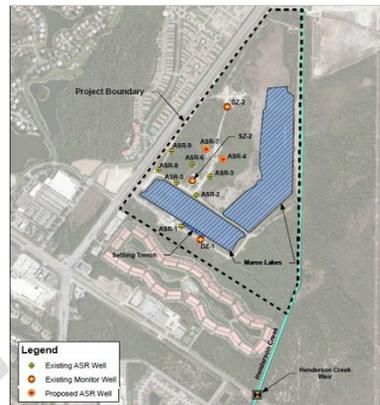


Figure 6-7. Map of Marco Island's ASR wellfield.

238 • Reservoirs: Everglades Agricultural Area (aka A-2)
 239 Reservoir – The project includes two major features: a
 240 treatment wetland that will improve water quality and a
 241 reservoir that will store excess water from Lake Okeechobee.
 242 The District is responsible for constructing the 6,500-acre
 243 wetland known as a Stormwater Treatment Area (STA). The
 244 District began construction ahead of schedule in April 2020
 245 and the project is expected to be completed in 2023.
 246 Additionally, the U.S. Army Corps of Engineers (USACE) is
 247 building the reservoir component, which will hold 240,000
 248 acre-feet of water. The USACE began construction in 2023
 249 and is estimated to be completed in 2030. The total project
 250 cost is expected to be just over \$2 Billion.



Figure 6-8. Water Conservation Areas (WCA) in the SFWMD.

251 • New WMA/WCA: SJRWMD C-10 WMA – In 2021, the St.
 252 Johns River Water Management District (SJRWMD)
 253 received a \$20 Million grant as part of FDEP Resilient
 254 Florida Program to develop the C-10 WMA. This project
 255 consists of a 1,300-acre WMA, pump station, outfall
 256 structure, 4-miles of new levee, and improvements to an
 257 existing federal levee. The project will collect water from a
 258 series of drainage canals to increase storage of water
 259 currently discharging to the Indian River Lagoon and direct
 260 flow to its historic drainage way towards the St. Johns River.
 261 The project is anticipated to provide 7.9 MGD of alternative
 262 water supply for the Upper St. Johns River. While not within
 263 SFWMD boundaries, this is a recent example of the
 264 development of a new WMA for resilient water supply in Florida.

265 • Phase 1 C-51 Reservoir Project: – This alternative water supply project, a public-private partnership
 266 between utilities and the mining industry, is designed to store excess water from the C-51 basin
 267 before being discharged to tide and conveying this water through canals during drier periods to
 268 areas adjacent to existing public supply wellfields. The project construction is estimated at \$161
 269 million, is expected to hold 14,000 acre-feet of static storage, and deliver 35 MGD in alternative
 270 water supply to offset impacts on regional canals from allocation increases. The reservoir is
 271 expected to be fully constructed in 2023.

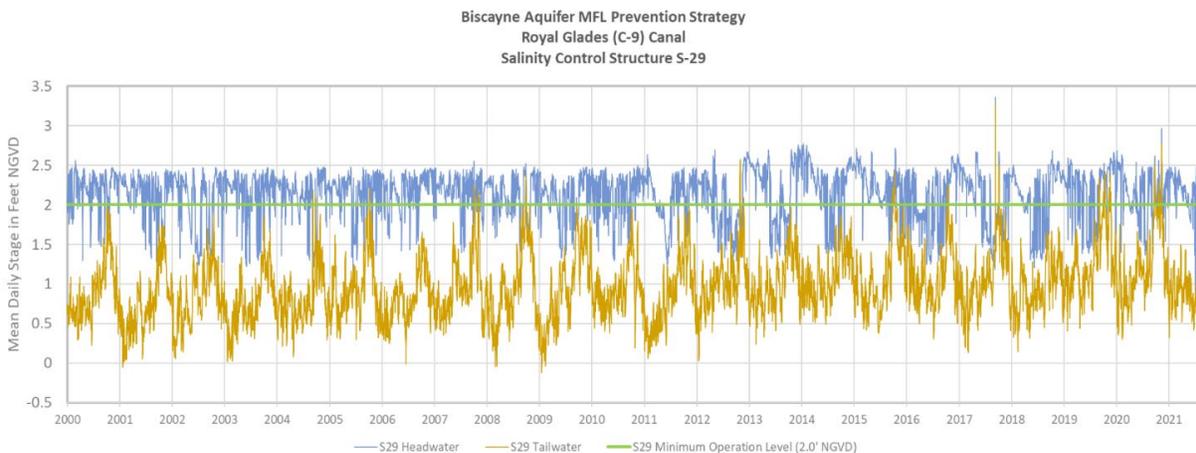
272

273 **ROLE OF COASTAL STRUCTURES IN PROTECTING WATER SUPPLY**
 274 **SOURCES**

275 As detailed earlier in this document, this resiliency plan seeks to build resiliency and mitigate the risks
 276 of flooding and sea level rise on water resources. The District’s canals and coastal structures are an integral
 277 part of water resources management. Among other purposes, the coastal structures act as barrier preventing
 278 saltwater intrusion from moving inland and impacting wellfield protection zones and other environmental
 279 protected areas. They do this by maintaining freshwater elevations upstream of the structure higher than
 280 ocean/saltwater levels, especially during the dry season, and provide recharge to the Surficial/Biscayne
 281 Aquifer.

282 The canals operate under normal and dry/wet season conditions which set the necessary water stages
 283 in the canal and therefore the subsequent operations of the canal’s structures. These operational conditions
 284 are relative to and therefore limited by the difference in elevation between the head and tail waters.
 285 Upstream (freshwater) operating levels are less than one foot higher than downstream tidal stages at certain
 286 coastal structure locations during high tide events. The Biscayne Aquifer MFL Prevention Strategy
 287 established that 2 feet of freshwater head needs to be maintained for more than 6 months a year, to prevent
 288 saltwater from encroaching into the Biscayne Aquifer. Figure 6-9 shows how often the S-29 structure’s
 289 tailwater level dips below the 2 feet minimum as well as how the tailwater and headwater are converging,
 290 which translates to less head difference in this gravity structure during extended periods of time. This
 291 reduced control is further exacerbated as the structures age, sea levels rise, and as climate and rainfall
 292 uncertainty increase, reducing the capability of the system to maintain freshwater minimum elevations and
 293 manage saltwater intrusion.

294



295

296 **Figure 6-9.** Headwater and Tailwater stages at S-29 structure.

297

298

299

300

301 The rehabilitation and replacement of lift gates
 302 and the installation of a new pump station will allow,
 303 beyond flood protection, for increased control of
 304 upstream fresh water by giving operators flexibility
 305 in discharge capacity, precise flow rate control, and
 306 optimization via integrated basin wide freshwater
 307 management, reducing unnecessary or earlier
 308 drawdowns as a result of the existing limitations in
 309 discharge capacity during higher tide events. The
 310 increased ability to maintain higher freshwater levels,
 311 especially during the dry season, significantly
 312 reduces the potential risk of saltwater intrusion
 313 effecting fresh water supplies. Additionally, the
 314 increased control will allow operators to adjust flows
 315 for. As an example, Figure 6-10 shows the benefit to
 316 subregional groundwater water levels as the result of
 317 maintaining higher canal levels near the end of the
 318 wet season in Collier County.

319 In two basins where resiliency projects are being
 320 prioritized currently, we can observe risks to existing
 321 wellfield protection zones by the advance of
 322 saltwater interface. In the C-9 basin example, the risk
 323 to water supplies is particularly acute as the majority
 324 of North Miami’s water is serviced by the Norwood-
 325 Oeffler Water Treatment Plant. This 15 MGD plant’s
 326 freshwater wells are within one mile of the saltwater
 327 intrusion line and coastal structure. In the C-7 basin, the saltwater intrusion line is 7 city blocks away from
 328 the freshwater wells for the Winson Water Treatment Plant. Since 2009, the saltwater interface has
 329 gradually been moving westward (see Figure 6-11). Since 2000, 25 water supply wells have been lost along
 330 South Florida’s coastline due to saltwater intrusion.

331

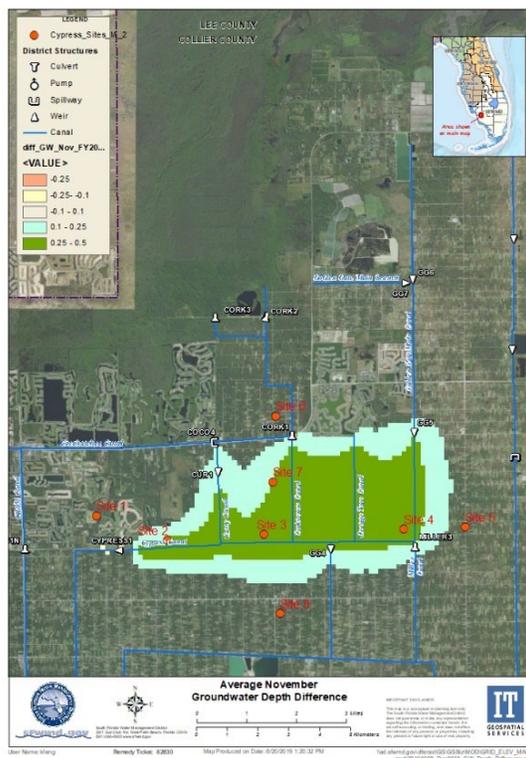


Figure 6-10. Average November positive groundwater depth difference due to optimized structure operations.

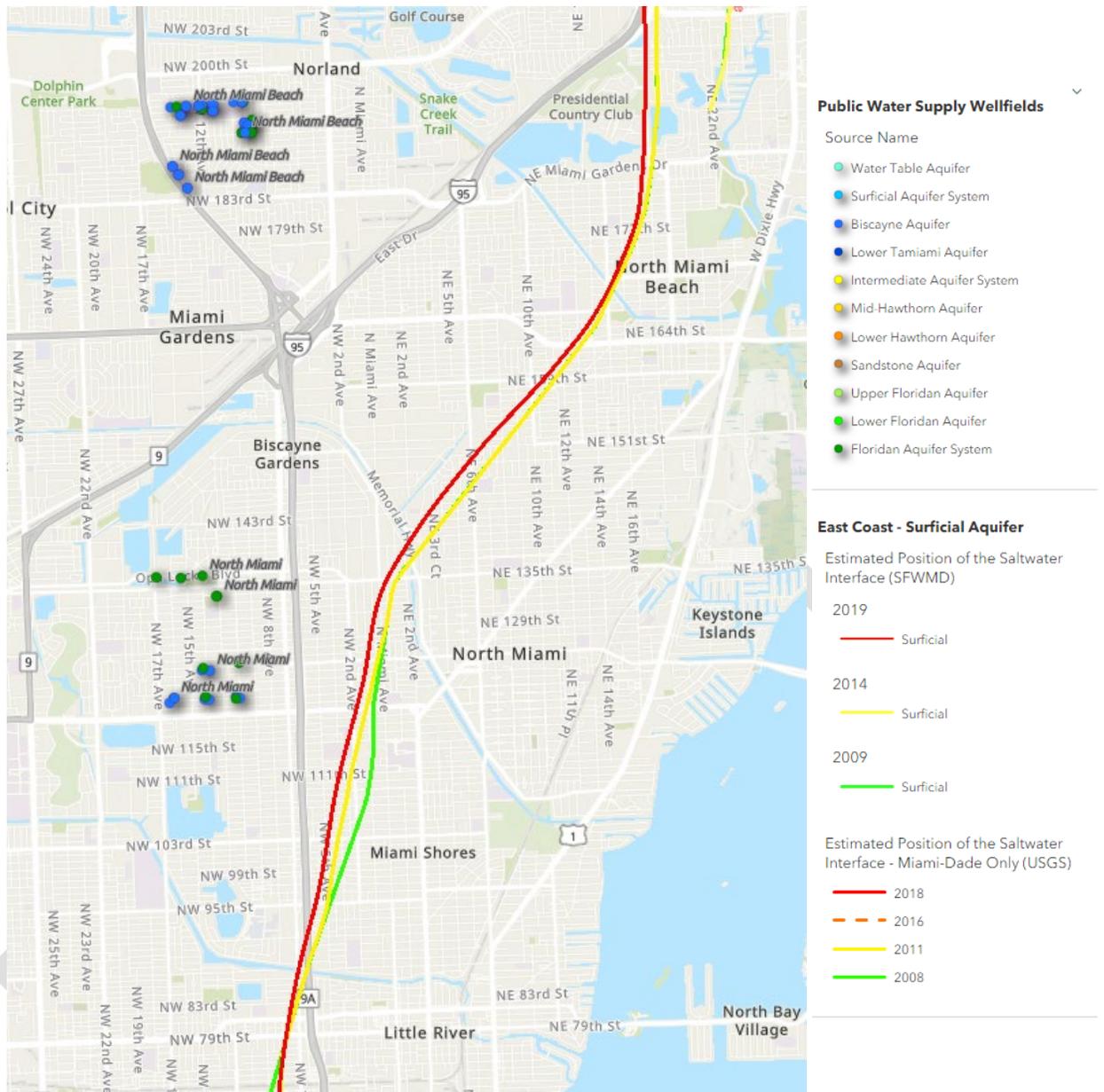


Figure 6-11. Saltwater interface line in S-27, S-28, and S-29 structures.

332

333

334

*Detailed information on Water Supply Management and saltwater intrusion is documented in the Lower East Coast Water Supply Plan and Saltwater Interface Monitoring and Mapping Program Technical Publication WS-58.

335

336 RESILIENCY PATH FORWARD

337 In addition to all the current projects being implemented or funded by the District and its partners, there
338 will be a process for assessing and responding to the resiliency needs of our water supplies. These needs
339 will be better understood through vulnerability assessments and robust data collection efforts already
340 underway as part of the District's Water Supply Vulnerability Assessment (WSVA) project. The WSVA
341 project will help the District determine what our water supply needs are and will provide guidance on the
342 execution of future resiliency projects like the ones featured throughout this plan. Additionally, this project
343 will inform the integration of appropriate measures and criteria for water allocation and serve as a
344 benchmark evaluating the overall sustainability of the District's water resources. These projects and all
345 additional data analysis and assessments related to the resiliency of our water supplies will be documented
346 as part of future iterations of the Resiliency Plan.

347

DRAFT

Chapter 7: Investing in Energy Efficiency and Renewable Energy

ENERGY EFFICIENCY

The South Florida Water Management District (District or SFWMD) is committed to improving the energy efficiency of operations and to offsetting new energy demands through renewable energy solutions. By following the latest building codes and using state of the art materials and designs, the District builds efficient and resilient projects (Flood Resistant Design and Construction, ASCE Standard 24).

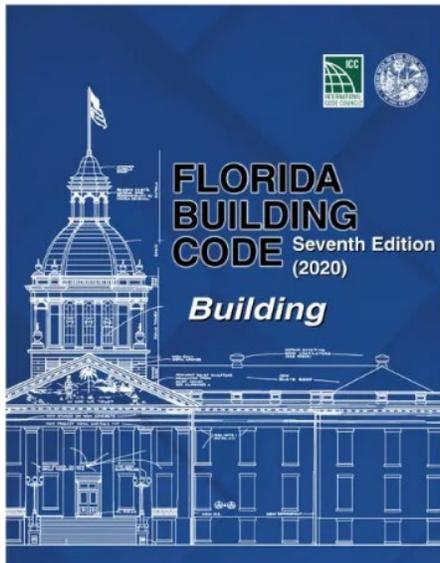


Energy efficiency is crucial because it helps to reduce the District’s overall energy consumption, which in turn might reduce the reliance on fossil fuels and other non-renewable sources of energy. By investing in energy-efficiency and renewable energy projects, the District can significantly reduce the amount of energy consumed and reduce the District’s carbon footprint. Overall, a combination of renewable energy and energy efficiency measures is essential for a sustainable future.

The District is looking into using two programs as guidance to help improve energy efficiency and promote sustainable energy in our facilities and projects. The LEED certification program and the Envision program are sustainable building design and certification programs that may be helpful in designing and implementing projects. With regards to renewable energy, solar energy systems are already integrated into some of District’s projects, as detailed below.

ACTIONS THAT THE DISTRICT TAKES TO HELP INCREASE ENERGY EFFICIENCY INCLUDE:		26
▪ AUTOMATION OF PUMP STATIONS – REDUCES RESOURCE USE, LESS FUEL AND EFFORT FOR MAINTENANCE		27
▪ DESIGN PROJECTS FOR LONGER LIFE – LESS MAINTENANCE OVER THE LIFE OF AN ASSET		28
▪ REDUCING USE OF OR SIZE OF CONTROL BUILDINGS - MOST CONTROL BUILDINGS ARE CONCRETE WITH LOW HEAT GAIN ALLOWING ALL OR MOST OF THE FACILITY TO FUNCTION APPROPRIATELY WITHOUT AIR CONDITIONING		29
▪ DIVERSIFYING THE DISTRICT’S MOTOR POOL TO INCLUDE ELECTRIC VEHICLES		30
▪ STAGGERING THE START OF MOTORS AND OTHER ELECTRICAL EQUIPMENT TO REDUCE THE MAXIMUM ELECTRICAL SERVICE NEEDED		31
▪ INCLUDE SMALLER “HOUSE LOADS” GENERATOR SO THAT GENERATORS ARE SIZED APPROPRIATELY FOR THE DIFFERENT LOADS THAT ARE NEEDED DURING PUMPING AND NON-PUMPING OPERATIONS		32
		33

34 FLORIDA BUILDING CODE REQUIREMENTS AND THIRD-PARTY 35 PROGRAMS



District project designs follow the Florida Building Code. The Code requires many of the energy efficiency related items that would be evaluated for projects seeking certification by third-party organizations such as the Leadership in Energy and Environmental Design (LEED) and Envision. Florida Building Code and recommendations from LEED and Envision are driving the District to develop and adopt energy efficient approaches to features such as heating, cooling, lighting and operations of motors and ancillary equipment. These state-of-the-art technologies will continue to be evaluated to improve the energy efficiency of District facilities.

LEED (Leadership in Energy and Environmental Design) is an ecology-oriented building certification program run by the U.S. Green Building Council (USGBC). LEED provides a framework for healthy, efficient, carbon and cost-saving green buildings. (“LEED Rating System” U.S. Green Building Council, <https://www.usgbc.org/leed>)

52 LEED certified buildings save money, improve efficiency, lower carbon emissions, and create a
53 healthier living environment. They are a critical part of addressing climate change and meeting
54 Environmental, Social, and Governance goals, enhancing resilience, and supporting more equitable
55 communities.

56 To achieve LEED certification, a project earns points by adhering to prerequisites and credits that
57 address carbon, energy, water, waste, transportation, materials, health, and indoor environmental quality.
58 Projects go through a verification and review process and are awarded points that correspond to a level of
59 LEED certification: Certified (40-49 points), Silver (50-59 points), Gold (60-79 points) and Platinum (80+
60 points).

61 The goal of LEED is to create buildings that:

- 62 • Reduce contribution to global climate change.
- 63 • Enhance individual human health.
- 64 • Protect and restore water resources.
- 65 • Protect and enhance biodiversity and ecosystem services.
- 66 • Promote sustainable and regenerative material cycles.
- 67 • Enhance community quality of life.

68 Envision is another holistic sustainability framework and rating system run by the Institute for
69 Sustainable Infrastructure that enables a thorough examination of the sustainability and resiliency of all
70 types of civil infrastructure. It can be used to assist the District in delivering civil infrastructure that tackles
71 climate change, addresses public health needs, cultivates environmental justice, creates jobs, and spurs
72 economic recovery. (“Envision: The Blueprint for a Sustainable Future” Institute for Sustainable
73 Infrastructure, <https://sustainableinfrastructure.org/envision/overview-of-envision/>)

74 Envision consists of:

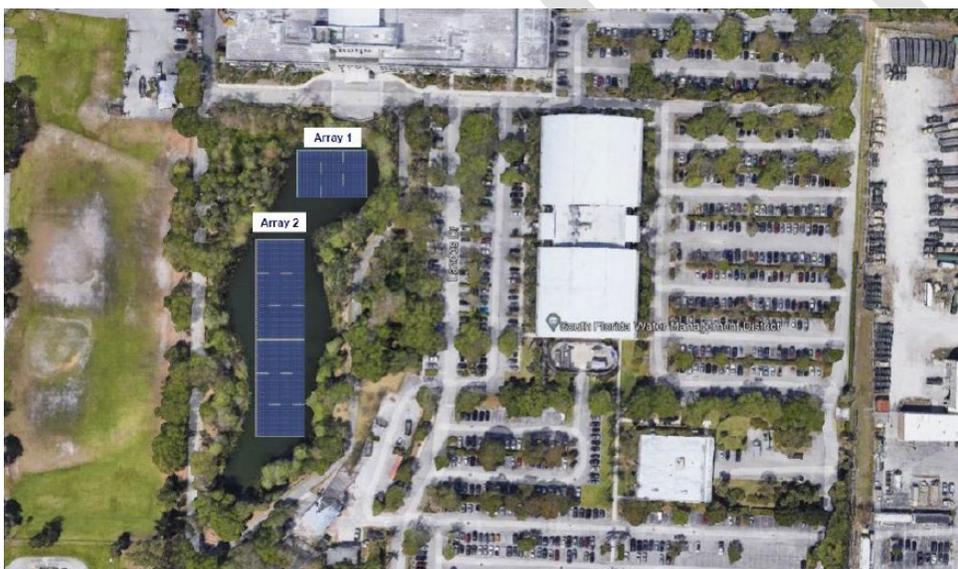
- 75 • A guidance manual that includes 64 sustainability and resiliency criteria
- 76 • Project assessment tools
- 77 • Third-party project verification
- 78 • Professional training and credentialing

79 RENEWABLE SOLAR ENERGY

80 Renewable energy sources are clean and emit little to no greenhouse gases, that are responsible for
81 climate change. This means that using renewable energy helps to reduce the District's carbon footprint and
82 mitigate the impacts of climate change. Florida receives abundant sunshine throughout the year, which
83 makes it an ideal location for solar power generation. Additionally, solar power can help to reduce energy
84 costs over the long-term, as a renewable source of energy.

85 The District is currently using renewable solar energy solutions to power much of its environmental
86 monitoring network and to assist in powering certain components of District facilities, such as lighting and
87 gate operation. Solar panels take up a considerable amount of space and large demand projects are complex
88 to implement in urban environments due to lack of larger open space. However, the District owns 1.5
89 million acres of land, some of which is available and suitable for solar arrays.

90 The District is considering one pilot project to explore the use of floating solar panels in applications
91 where wind damage to the solar infrastructure would not increase risk to the flood control system. This
92 proposed pilot project would be implemented on Lake Freddy at District headquarters in West Palm Beach.
93 In addition, a solar canopy for District fleet vehicles in the parking lot at headquarters is also being evaluated
94 to address a portion of existing energy demands.



95
96 **Figure 7-1:** Floating solar arrays pilot project proposed at Lake Freddy on SFWMD Headquarters.

97 In addressing larger energy needs, and with the goal of offsetting new energy demands, the District is
98 assessing the possibility of implementing solar power for projects in areas where there is an abundance of
99 open land for solar panels. Currently, the District is investigating opportunities with Florida Power and
100 Light (FPL) to install solar arrays on District lands near the C-43 and C-44 Reservoir projects, with the
101 goals of reducing energy costs at these facilities, as well as offsetting carbon emissions from existing and
102 new proposed structures that rely at least partially on fossil fuel generated power.

103 The District is also exploring the possibility of purchasing and installing solar arrays near specific
104 project locations. These potential projects would use smaller (approximately 2 megawatt) arrays that would
105 provide power directly to District facilities. These installations would be connected to the electrical grid
106 and use net-metering to track solar power generation and consumption as described below.

NET-METERING FOR SOLAR POWER SYSTEMS

- When a solar power system generates more electricity than the customer can use, the customer receives a credit for the excess kilowatt-hours (kWh) sent to the grid.
- If less electricity than needed is produced via solar, the customer must buy electricity from the utility to make up the difference.
- The customer pays for the “net” amount of electricity used (kWh purchased minus credit for kWh exported).

107

108 SOLAR INCENTIVES

109 A big incentive for solar over the years has been the Federal Investment Tax Credit (ITC). This was a
110 30% dollar-for-dollar tax credit that taxable entities received. Unfortunately, in the past, non-taxable entities
111 had no way of reaping this incentive. That changed with The Federal Inflation Reduction Act (IRA) of
112 2022 which now allows non-taxable entities to receive a 30% rebate on the total cost of solar installations.

113 In addition to the 30% ITC rebate, the IRA establishes three different types of ITC “Adders”, which
114 provide additional tax credits of up to 10% each, for projects that meet specified requirements (see below).
115 These incentives would allow the District to receive a rebate of up to 40% on solar projects.

116 **Low-income:** Projects located in a qualified “low-income community”, which is defined as a census
117 tract with a poverty rate of at least 20%, as well as a census tract where the median family income (MFI) is
118 80% or less of statewide MFI, or on “Indian land”, which is defined as land located within the boundaries
119 of an Indian reservation or lands held by a tribe.

120 **Domestic Content:** for projects that meet specified domestic content requirements which will be set
121 by Treasury, including 100% steel/iron for manufactured products with a 40% requirement through 2024.
122 Manufactured content will be deemed to have been produced in the United States if the adjusted percentage
123 of the total costs of all such manufactured products of the facility are attributable to manufactured products
124 which are mined, produced, or manufactured in the United States.

125 The District is currently further investigating these opportunities to determine how these initially
126 proposed projects might benefit from the 2022 IRA rebate programs.

Chapter 8: Characterizing and Ranking Our Resiliency Projects

INTRODUCTION

The South Florida Water Management District (District or SFWMD) is initially focusing its resiliency infrastructure investment priorities to address coastal water control structures vulnerability to sea level rise. This is a no-regret strategy, as recommended by the District's Flood Protection Level of Service (FPLOS) Phase I Flood Vulnerability Assessments, and validated by FPLOS Phase II Adaptation Planning Studies. The results of these FPLOS studies demonstrate current limitations on the operational capacity of and the need of adaptation to restore original design capacities at these structures.

During the initial stages of already observed SLR impacts, the District is continuing to operate structures through operational changes, by investing in extending the top of gates, and implementing targeted structure enhancement measures. As sea levels increase, additional measures will be required to maintain headwater stages at structures and to prevent saltwater intrusion and flooding impacts. Enhancing existing structures can substantially improve their functionality and performance by reducing the

vulnerability of systems and equipment to flooding and maintaining their ability to protect against saltwater intrusion.

Adaptation to SLR and storm surge involve large scale projects that integrate floodwalls, gates, and forward pumps to properly manage surface and groundwater within the area. In addition, long-term SLR may also involve seepage barriers to avoid saltwater intrusion and control the long-term rise in groundwater levels. Some of these efforts are beginning to be advanced in the region, to address storm surge and other coastal hazards.

Many of the District's coastal structures were constructed over 70 years ago and are no longer capable of conveying their design discharge due to changes within the watershed, SLR, and climate change. The District is proposing to restore the original design discharge at these structures by installing forward pump stations that can continue to discharge to tide when gravity discharge ceases (during storm surge or extreme high tide events) and to augment gravity discharge at critical times. Figure 8-1 below illustrates the relative percent of time that gate closures were needed during the King Tide season (September through November) in 2020 at four different locations. As observed in these charts, these gates were closed for



about 3-5 hours on average, per day during King Tide events, and with a significant increase of up to 15 hours per day during the peak of the 2020 King Tide season.

To determine pumping capacity needs at the coastal structures, pump sizes at the most immediate priority structures have been initially estimated using one half of the design discharge capacity of the structure. For instance, a structure with a design discharge capacity of 1,000 cubic feet per second (cfs) would need a 500 cfs pump station. Structures ranked as intermediate in terms of priority, are being augmented with one quarter of the design discharge capacity for initial pump sizing. Structures ranked in the long-term need category would not have pump cost estimates until they move from long-term to intermediate need. Initial pump sizing is based on a) existing C&SF forward pump implementation strategies; b) the assumption that other local flood mitigation strategies will be constructed in the basin in combination with the local forward pump solutions; c) the consideration of downstream capacity; and d) best professional judgement.

The C-8/C-9 Basin FPLOS Phase II Adaptation Planning Study has recently recommended more specific pump capacities for S-28 and S-29 Coastal Structures, as detailed in Chapter 9. As design is evolving for these and other coastal structures, final pump capacities will be determined. Figures 8-2 and 8-3 below illustrate a comparison between the amount of time needed to remove the cumulative flows (or the total runoff to bring the stages back to normal operating ranges) for the scenarios with forward pumps sized at 25% and 50% of the spillway design capacity, relative to the no pump scenario. The design of forward pump stations will be adaptable and will include the ability to add additional pumps in the future as environmental conditions change. The precise nature of improvements at each structure, including consideration of replacement needs, additional flooding barriers, and forward pump sizing, will be determined during the feasibility and design phases for each structure, and as part of the more detailed and comprehensive FPLOS adaptation planning, Phase II Studies, which includes the assessment of local and larger regional forward pump strategies. No harm to downstream conveyance capacity or increasing flooding risks will result from the proposed forward pumping projects. Appropriate operational criteria and mitigation measures will be planned and designed, as adequate, during final feasibility and implementation phases.

The effectiveness of using forward pumps to reduce flood risk and restore the original level of service can be demonstrated by the operational results of existing forward pumps at the S-25B and S-26 coastal structures. During Hurricane Isaias, between July 20 and August 2, 2020, the average daily upstream water levels (headwater) were lowered consistently at structures with gravity flow and a forward pump. At the S-25B and S-26 coastal structures, upstream water levels were reduced significantly with the combination of gravity flow and forward pumping. During the same storm event at S-27, S-28 and S-29, the average daily upstream water levels increased with gravity flow alone. These observations, as illustrated in Figure 8-4, demonstrate the existing limitations and associated challenges in maintaining or reducing upstream water levels by relying solely upon gravity flow.

Another flood mitigation alternative is the utilization of emergency storage options. One example is the C-4 Emergency Detention Basin (C-4 EDB) in Miami-Dade County. When the C-4 Canal can't handle the water volume necessary to prevent flooding, the C-4 EDB is employed to receive and store the excess water. The forward pump station at the mouth of the C-4 Canal is the first component of the C-4 EDB that is used, when needed, in addition to gravity flow. The S-26 Pump Station at the mouth of the Miami River Canal in the C-6 basin was built to ensure the higher tailwater resulting from pumping at the S-25B does not impact C-6 upstream of S-26. These stations pump to the Miami River and are used first for flood control. The EDB is used for larger rain events when stages continue to rise, and additional flood mitigation is needed. The C-4 EDB provides improved flood protection for the City of Sweetwater, Miami-Dade County, City of Miami, and City of West Miami.

Levee and canal bank enhancements are another example of project recommendations included in this plan to provide additional flood protection and prevent the impacts of SLR on water resources and the environment. Enhancement of L-31 and the Corbett Levee are being proposed to address vulnerability to

SLR, storm surge and increasing stormwater volumes, as a result of more extreme rainfall events. Future modeling efforts will determine additional resiliency needs at other levee structures.

All the proposed projects include resiliency strategies to reduce the vulnerability of communities and environmentally sensitive areas downstream and upstream of these structures.

The District is also committed to seeking “green” or nature-based solutions in addition to “gray” infrastructure improvements to increase resiliency, as described in Chapter 4. Gray infrastructure examples and green features will be necessary to meet the challenges of land development and climate change impacts, including SLR, along with basin-wide solutions to maximize the capacity of flood adaptation. The restoration of design discharge capacities will need to be combined with additional upstream and downstream solutions, to move forward as part of the FPLOS Phase II dynamic adaptive pathway approach. This approach and additional considerations were applied in the Pilot Phase II FPLOS Assessment for the C-7 Basin: Identification and Mitigation of Sea Level Rise Impacts (2015 FEMA PDM Study). The main objective of this study was to reduce the potential for loss of life and property by recommending alternative mitigation strategies to be updated in the Miami-Dade County Local Mitigation Strategy (LMS). The project had two elements: 1) a technical assessment of the FPLOS for the existing infrastructure under current and future SLR scenarios; and 2) a strategic assessment of alternative mitigation strategies intended for incorporation into the Miami-Dade LMS. The study evaluated a series of mitigation alternatives for the basin involving local hydraulic measures (M1), a regional forward pump (M2) and elevating buildings (M3) and associated benefits to be implemented by multiple agencies. The results show various pathways (sequences and combination of mitigation strategies) can be explored. If an individual flood mitigation alternative is not able to achieve the specified target of the performance criteria, additional or other mitigation strategies are needed. Adaptation pathways were assessed for the entire C-7 Basin, as summarized in Figure 8-5 below, showing how multiple strategies can be combined over time. A similar strategy was recently finalized as part of the C-8/C-9 Basins FPLOS Phase II Adaptation Planning Studies. Project Status and recommended strategies are being updated at: <http://www.buildcommunityresilience.com/SFWMD/FPLOS/c8c9/>.

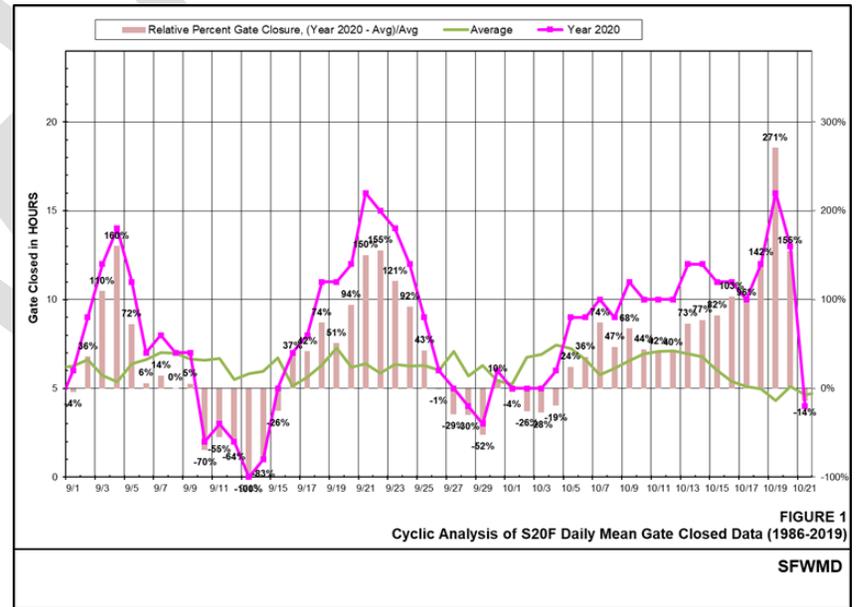
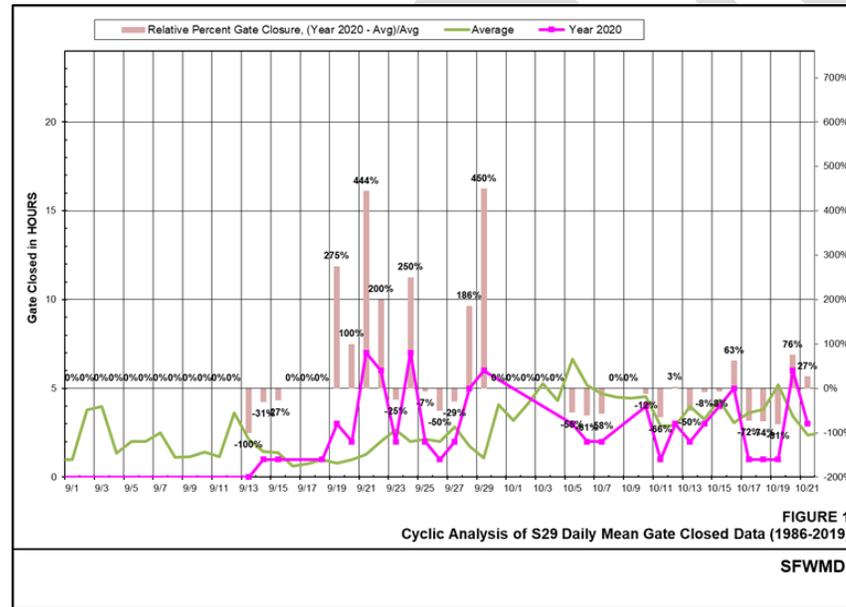
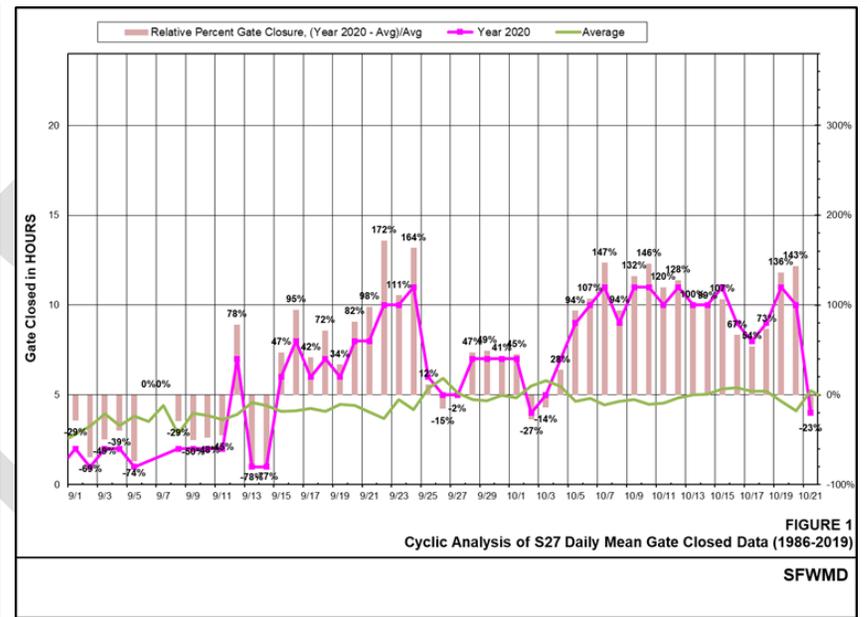
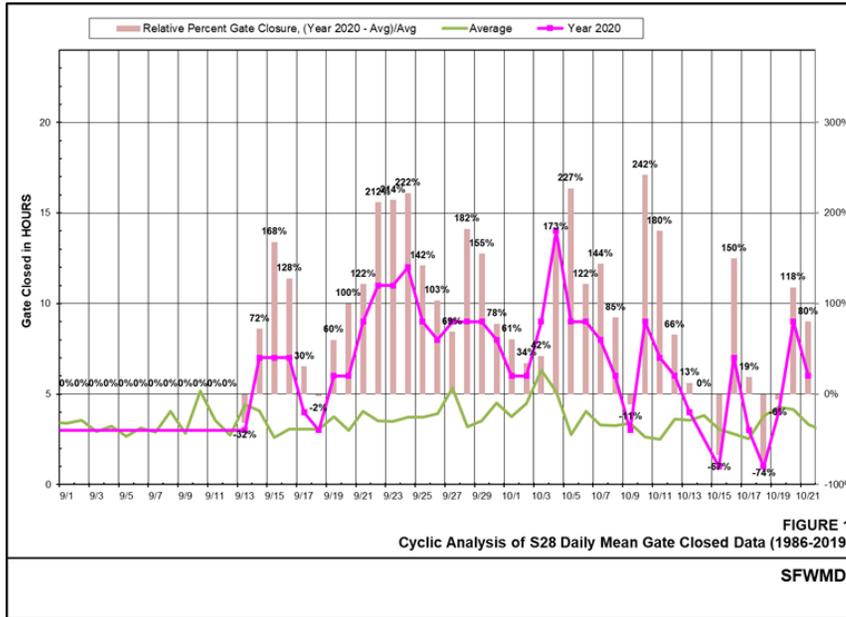
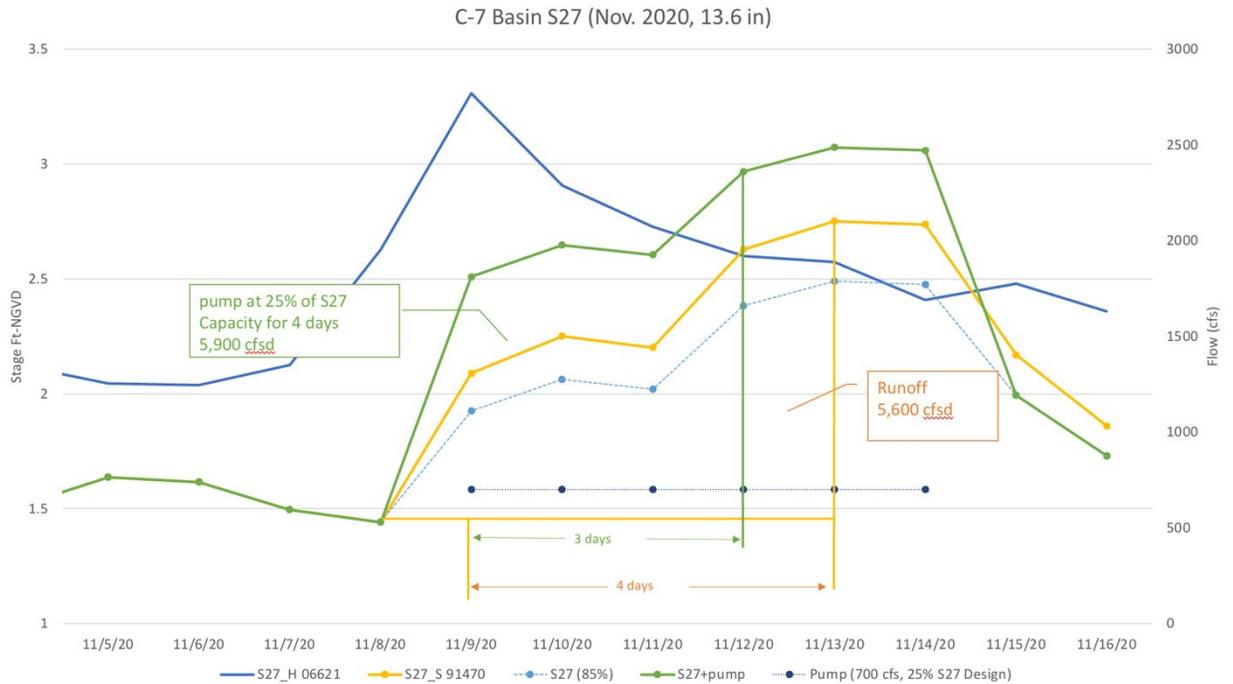
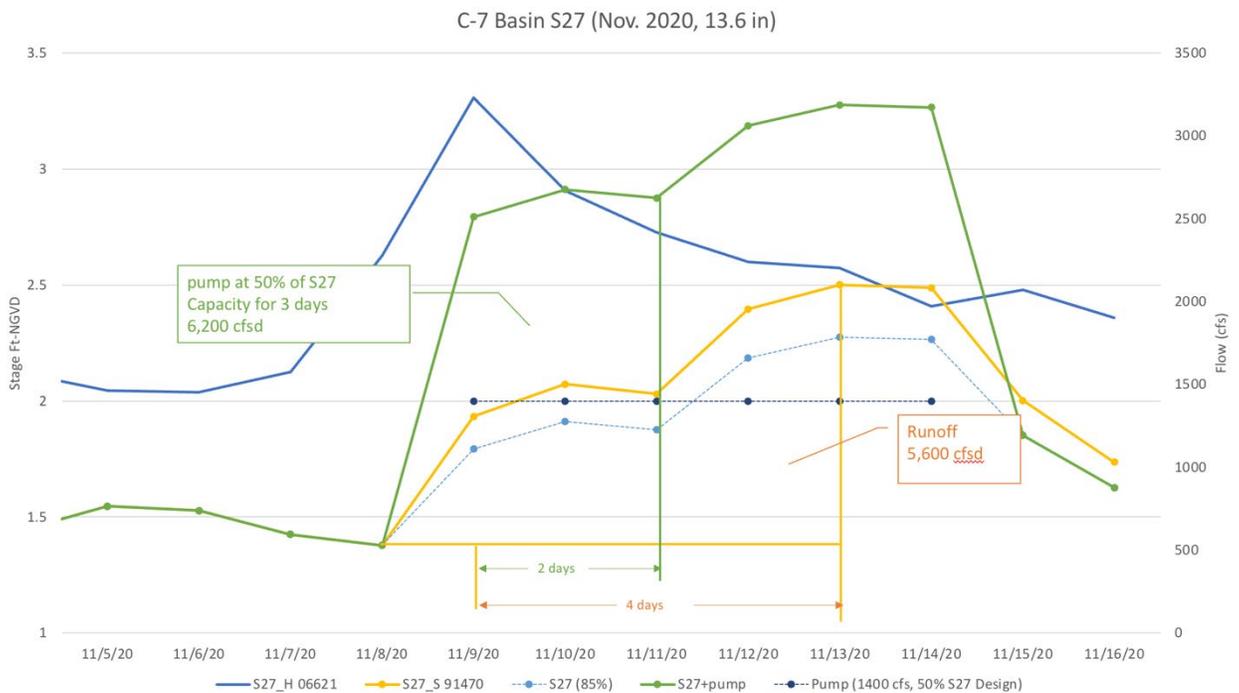


Figure 8-1. Relative Percent Gate Closure Times during the 2020 High Tide Season.

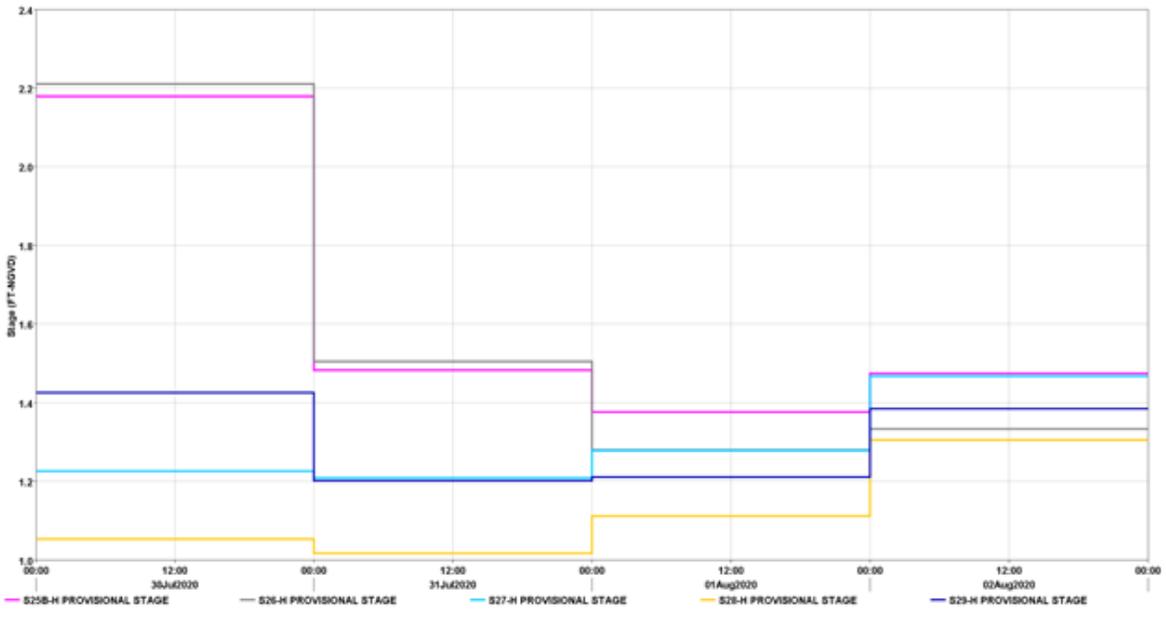


1
 2 **Figure 8-2.** Potential amount of time needed to remove the cumulative flows at S-27 (5600 cfsd total
 3 runoff to bring the stages back to normal operating ranges during Tropical Storm Eta in November 2020)
 4 for the scenario with forward pumps sized at 25% of the spillway design capacity (3 days) relative to
 5 the no pump scenario (4 days).



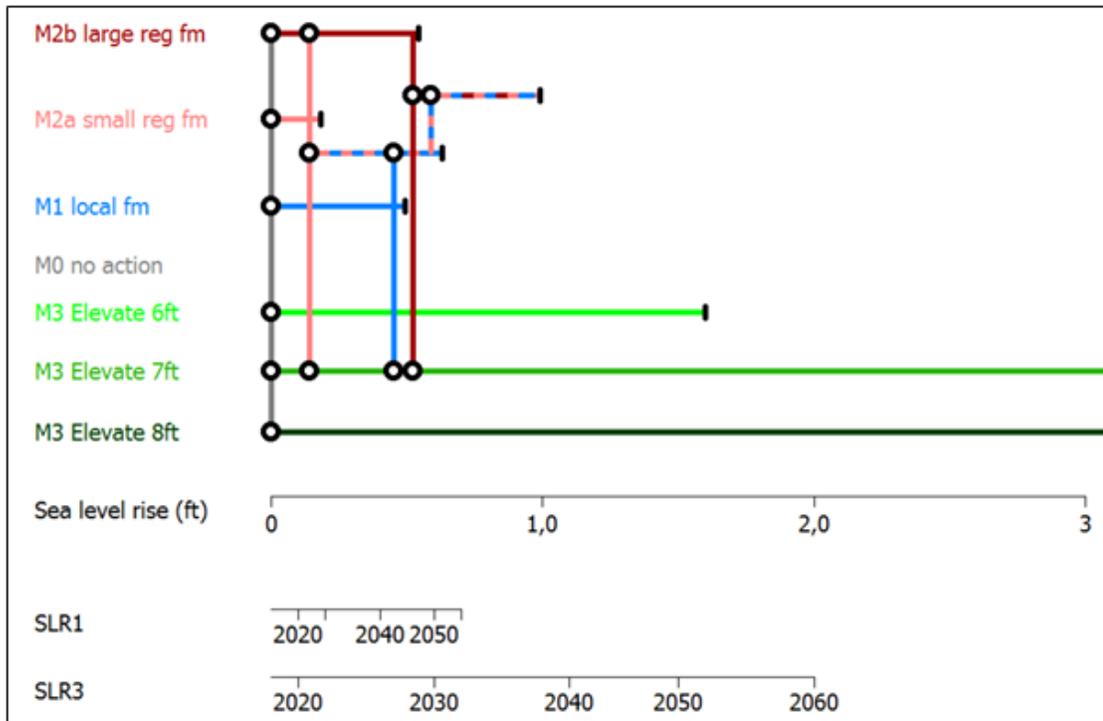
6
 7 **Figure 8-3.** Potential amount of time needed to remove the cumulative flows at S-27 (5600 cfsd total
 8 runoff to bring the stages back to normal operating ranges during Tropical Storm Eta in November

9 2020) for the scenario with forward pumps sized at 50% of the spillway design capacity (2 days)
 10 relative to the no pump scenario (4 days).



11

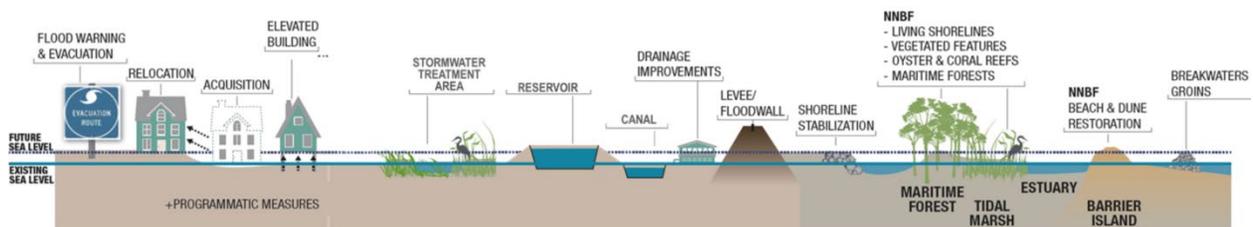
12 **Figure 8-4.** Observed Headwater Stages during Hurricane Isaias, in July/August 2020, at Coastal
 13 Structures with forward pump (S-25B and S-26) vs. Coastal Structures with gravity discharge only (S-
 14 27, S-28, S-29)



15

16 **Figure 8-5.** Adaptation Pathways map for the entire basin, based on the simulated expected annual
 17 damage for the current sea-level and the two possible future sea level rise scenarios.

18 Updated Federal Emergency Management Agency Coastal Zone A Maps, the U.S. Army Corps of
 19 Engineers (USACE) South Atlantic Coastal Study and Back Bay Feasibility Studies, including the Miami
 20 Dade, Collier County and the Florida Keys (Monroe County) Coastal Storm Risk Management Studies
 21 were recently released in response to coastal storm risks and flood protection needs. These studies were
 22 developed focusing on storm surge flood inundation risks. The District is working closely with these
 23 Federal Agencies to coordinate the implementation of coastal adaptation strategies such as beach and dune
 24 restoration, shoreline stabilization, flood walls and nature and natural base solutions, including living
 25 shorelines, oyster and coral reefs, marshes, etc., along with the ongoing Section 216 C&SF Flood Resiliency
 26 Study. Figure 8-6 below summarizes how these combinations of solutions can be developed, through
 27 cooperation among local, state, regional and Federal Agencies. The figure is meant to highlight many of
 28 the mitigation strategies that are available for use either by themselves or together when the site allows.



29 **Figure 8-6.** Potential Flood Mitigation Measures to improve resilience and sustainability (Source:
 30 USACE, modeled from https://ewn.el.ercd.dren.mil/nnbf/other/5-ERDC-NNBF_Brochure.pdf)

31 **SOCIALLY DISADVANTAGED COMMUNITIES**

32 The District serves diverse communities throughout its area of operations, each experiencing unique
33 and varied impacts resulting from climate change and other changing conditions, including population
34 increase and land development. The timing, extent, and kinds of these impacts vary depending on factors
35 like location, such as coastal or inland, and socioeconomic circumstances. The SFWMD considers the
36 disproportionate vulnerability of minority and financially disadvantaged communities who are more
37 adversely affected by the impacts of climate change as part of its resiliency planning efforts to ensure
38 equitable community-wide benefits. Ensuring equitable community-wide benefits means providing equal
39 protection from adverse impacts, equitable access to the benefits provided by resiliency projects, and equal
40 opportunity for participation in the planning and decision-making processes, for all members of our region's
41 communities.

42 To effectively plan resiliency projects to meet our mission, resiliency vision, and serve our
43 communities, we look to a set of guiding principles that steer social considerations. These guiding principles
44 ensure our resiliency projects provide an equal degree of protection against climate change driven
45 environmental impacts, promote an enhanced quality of life for all members of the communities residing
46 within the project basins, and offers equal access to the planning and decision-making processes through
47 stakeholder engagement and coordination with the local governments and impacted communities.

SFWMD's Resiliency Planning Guiding Principles for Social Considerations:

- **Do no harm** – SFWMD resiliency projects are designed to avoid further harm to vulnerable communities.
- **Prioritize and value prevention** – SFWMD focuses on preparing our communities for anticipated changing conditions, ensuring our systems can withstand natural hazards and recover quickly from disruptions.
- **Prioritize vulnerable communities** – SFWMD prioritizes investments in projects that benefit disadvantaged communities and enhances the quality of life for all community members.
- **Meaningful community engagement** – SFWMD actively seeks input and ideas from community members, ensuring projects are informed by their perspectives. Transparency is key in developing and executing resiliency work to foster ongoing engagement, communication, trust, and collaboration.
- **Proactive engagement and leadership** – SFWMD involves community experts and leaders from impacted community groups, seeking their insights and feedback to shape equitable projects.
- **Responsive and continued engagement** – SFWMD remains responsive and accountable to community concerns, prioritizing follow-up actions and ongoing discussion.

48
49 The SFWMD utilizes a range of resources to determine social vulnerability, identify disadvantaged
50 communities, and highlight locations that may be candidates for further review both at a regional scale and
51 within project impact areas. These data are included in project ranking criteria and grant applications. We
52 rely on reputable sources including the Center for Disease Control (CDC) Agency for Toxic Substances
53 and Disease Registry (ATSDR) Social Vulnerability Index (SVI), the Council on Environmental Quality
54 (CEQ) Climate and Economic Justice Screening Tool (CEJST), and the Environmental Protection Agency
55 (EPA) Environmental Justice screening and mapping tool (EJScreen). These resources are driven by diverse

56 federal datasets, as outlined below. Figures 8-7 through 8-9 show the areas where socially vulnerable and
 57 disadvantaged communities were identified within the SFWMD region.

58 Incorporating these socioeconomic indicators as part of our project ranking process ensure regional
 59 support to local communities, facilitating the identification and implementation of solutions that alleviate
 60 environmental impacts and increase the quality of life where it is most needed. The prioritized resiliency
 61 projects are expected to result in reduced flood risks, increased resilience of water supply systems,
 62 preservation and enhancement of natural areas, heightened civic engagement, and an improved quality of
 63 life for all residents of these communities.

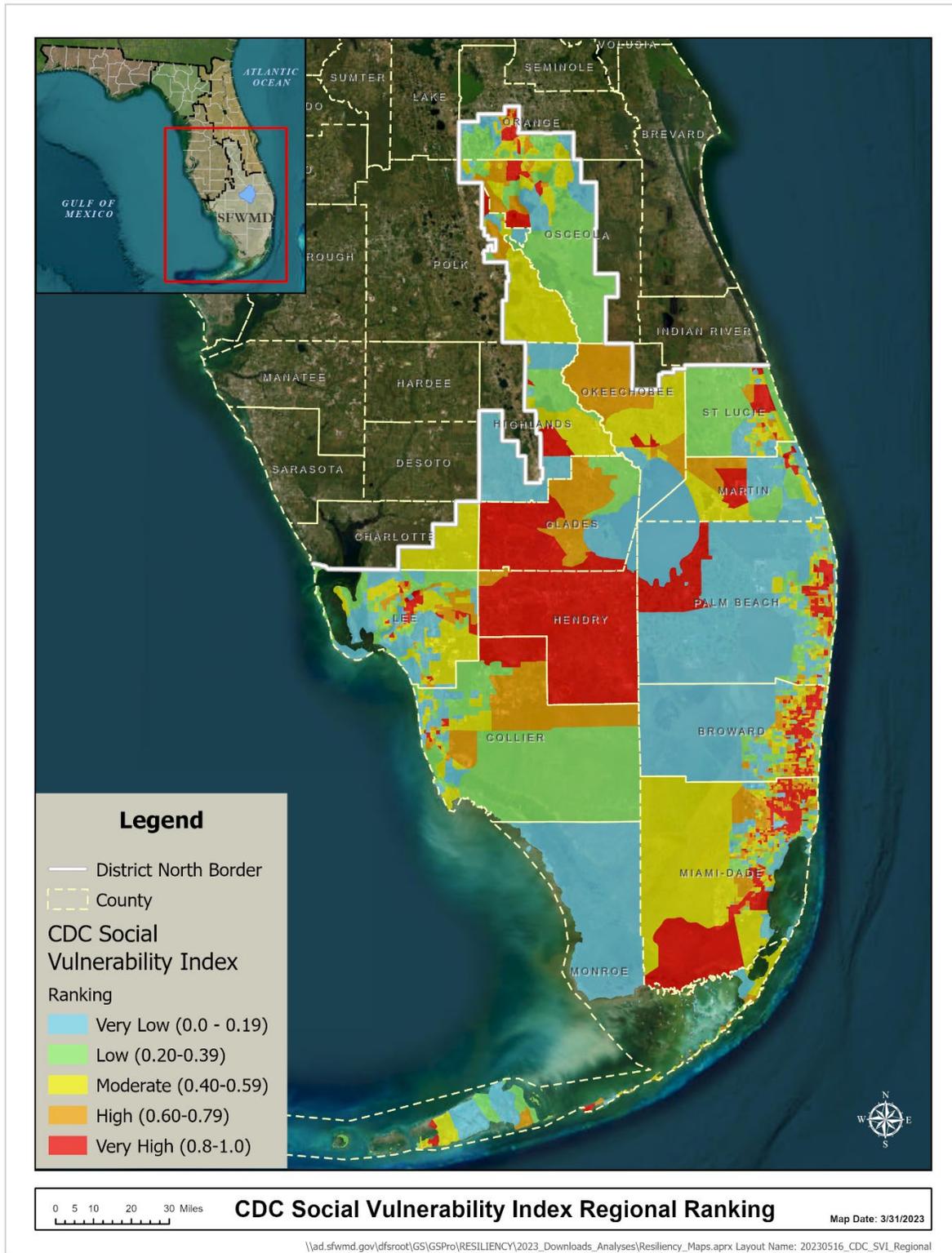
64 **CDC/ATSDR SVI**

65 The CDC’s Agency for Toxic Substances and Disease Registry (ATSDR) Social Vulnerability Index
 66 (SVI) utilizes U.S. Census data to assess the social vulnerability of communities in each census tract.
 67 Census tracts are geographical subdivisions within counties where statistical data is collected by the Census.
 68 The CDC/ATSDR SVI evaluates each tract based on 16 social factors, which are grouped into four themes
 69 (table 8-1). Each tract receives a separate ranking for each of the four themes and an overall ranking. The
 70 ranking scale ranges from Very Low (0.0-0.19) to Low (0.20-0.39), Moderate (0.40-0.59), High (0.60-
 71 0.79), and Very High (0.8-1.0).

72 SFWMD employs the overall SVI ranking equal or greater than the intermediate range to identify
 73 socially vulnerable and disadvantaged communities both at the regional level (as depicted in figure 8-7)
 74 and within project impact areas. Figure 8-7 highlights the locations where socially vulnerable communities
 75 have been identified within the SFWMD region.

76 **Table 8-1.** CDC/ATSDR SVI themes and corresponding social factors. Source: [CDC/ATSDR Social](#)
 77 [Vulnerability Index \(SVI\)](#).

Socioeconomic Status	Household Characteristics	Racial and Ethnic Minority Status	Housing Type & Transportation
<ul style="list-style-type: none"> • below 150% poverty • unemployed • housing cost burden • no high school diploma • no health insurance 	<ul style="list-style-type: none"> • aged 65 or older • aged 17 or younger • civilian with a disability • single-parent households • English language proficiency 	<ul style="list-style-type: none"> • Hispanic or Latino (of any race), Black and African American (not Hispanic or Latino), American Indian and Alaska Native (not Hispanic or Latino), Asian (not Hispanic or Latino), Native Hawaiian and Other Pacific Islander (not Hispanic or Latino), Two or More Races (not Hispanic or Latino), Other Races (not Hispanic or Latino) 	<ul style="list-style-type: none"> • multi-unit structures • mobile homes • crowding • no vehicle • group quarters



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Figure 8-7. Map showing communities identified as socially vulnerable based on the CDC/ATSDR SVI overall ranking data within the SFWMD region.

81 CEQ CEJST

82 The Council on Environmental Quality's (CEQ) Climate and Economic Justice Screening Tool
83 (CEJST) utilizes various data sources to identify disadvantaged communities, including:

- 84 • U.S. Census's American Community Survey, the Federal Emergency Management
85 Agency's (FEMA) National Risk Index,
- 86 • First Street Foundation's Climate Risk Data,
- 87 • Department of Energy (DOE)'s Low-Income Energy Affordability Data (LEAD) Tool,
- 88 • Environmental Protection Agency's (EPA) Office of Air and Radiation (OAR)
89 Environmental Justice Screening and Mapping Tool (EJScreen),
- 90 • Centers for Disease Control and Prevention's (CDC) PLACES and U.S. Small-area Life
91 Expectancy Estimates Project (USALEEP) data,
- 92 • National Community Reinvestment Coalition's (NCRC) dataset of formerly redlined
93 areas,
- 94 • Department of Housing and Urban Development's (HUD) Comprehensive Housing
95 Affordability Strategy (CHAD),
- 96 • Multi-Resolution Land Characteristics (MRLC) consortium by the Trust for Public Lands
97 and American Forests' Percent Developed Imperviousness (CONUS) data,
- 98 • Department of the Interior's (DOI) Abandoned Mine Land Inventory System (e-AMLIS),
- 99 • U.S. Army Corps of Engineers' Formerly Used Defense Sites data,
- 100 • EPA's Resource Conservation and Recovery Act (RCRA) database for Treatment,
101 Storage, and Disposal Facilities (TSDF) data compiled by EJScreen,
- 102 • EPA's Comprehensive Environmental Response, Compensation, and Liability
103 Information System (CERCLIS) database compiled by EJScreen,
- 104 • EPA's Risk Management Plan (RMP) facilities data compiled by EJScreen,
- 105 • EPA's National Air Toxics Assessment (NATA),
- 106 • Department of Transportation's (DOT) transportation access disadvantage data and
107 traffic data compiled by EJScreen,
- 108 • EPA's Underground Storage Tanks (USTs) data,
- 109 • EPA's Risk-Screening Environmental Indicators (RSEI) compiled by EJScreen, and
110 • Bureau of Indian Affairs' (BIA) Land Area Representation (LAR) dataset.

111 The CEJST uses these data as indicators of burdens and organizes them into eight categories. The eight
112 categories are climate change, energy, health, housing, legacy pollution, transportation, water and
113 wastewater, and workforce development (table 8-2). A community is identified as disadvantaged in the
114 CEJST if it meets two criteria: (1) the census tract is at or above the threshold for one or more
115 environmental, climate, or other burdens, and (2) the census tract is at or above the threshold for an
116 associated socioeconomic burden. Additionally, a census tract surrounded by disadvantaged communities
117 and with a low-income percentile at or above 50% is also considered disadvantaged.

118 SFWMD utilizes these eight categories to identify disadvantaged communities both at the regional level
119 and within project impact areas. Figures 8-8 through 8-9 illustrate communities identified as disadvantaged
120 in the eight categories within the SFWMD region.

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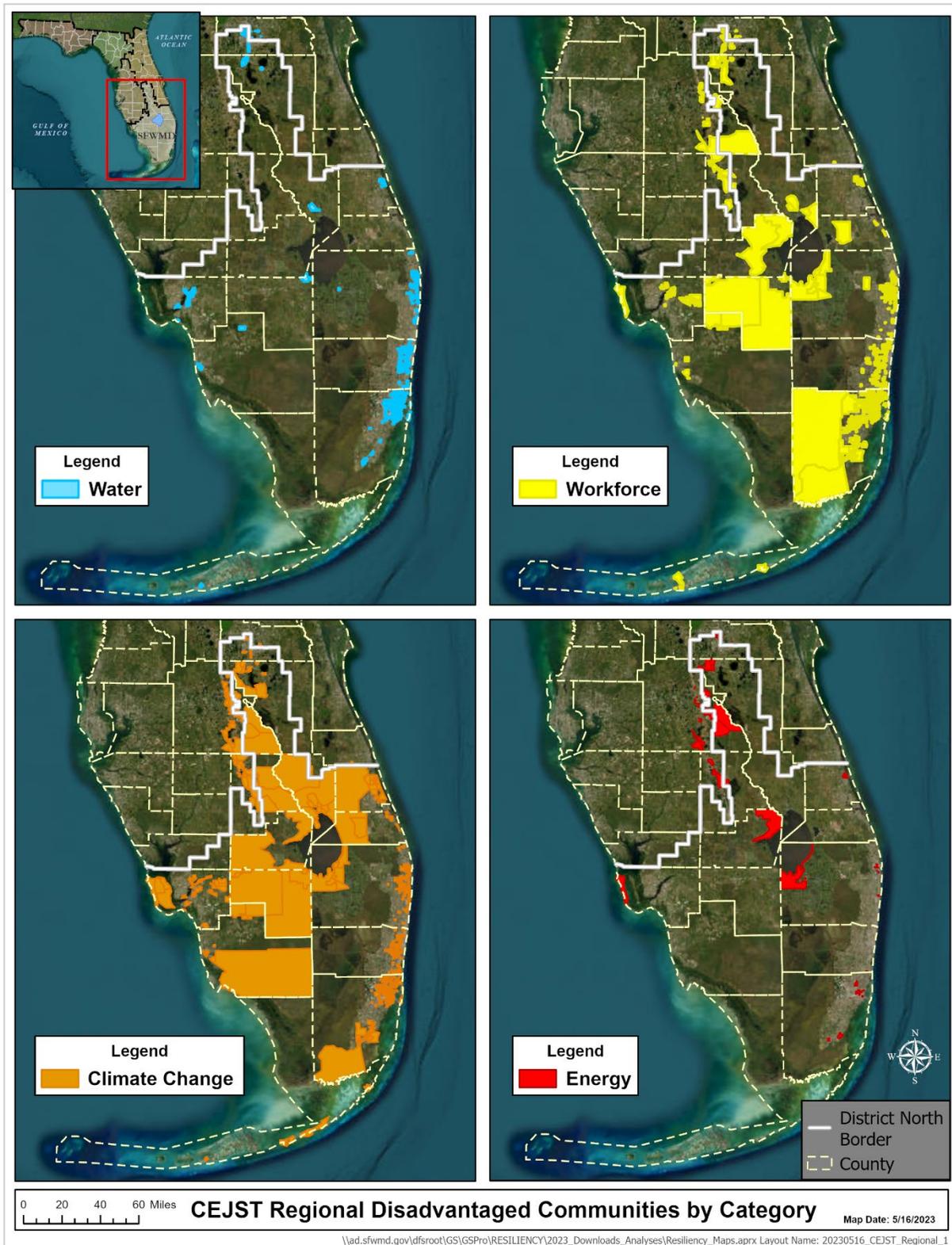
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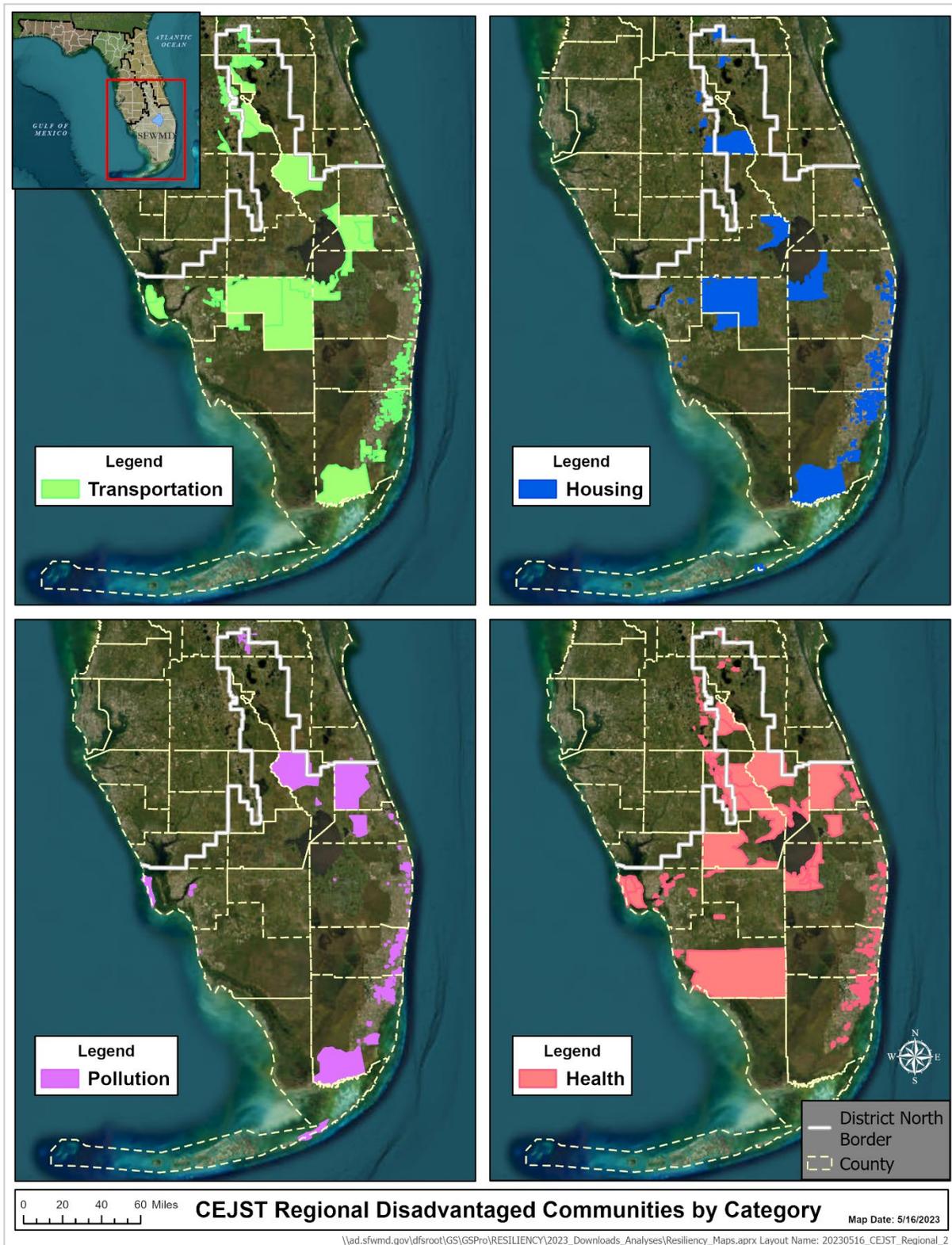
Table 8-2. The CEQ CEJST categories and corresponding factors. Source: [Methodology & data - Climate & Economic Justice Screening Tool \(geoplatform.gov\)](#).

Climate Change	Energy	Health	Housing
<p>ARE (1) at or above the 90th percentile for expected agriculture loss rate OR expected building loss rate OR expected population loss rate OR projected flood risk OR projected wildfire risk</p> <p>AND (2) are at or above the 65th percentile for low income</p>	<p>ARE (1) at or above the 90th percentile for energy cost OR PM2.5 in the air</p> <p>AND (2) are at or above the 65th percentile for low income</p>	<p>ARE (1) at or above the 90th percentile for asthma OR diabetes OR heart disease OR low life expectancy</p> <p>AND (2) are at or above the 65th percentile for low income</p>	<p>(1) Experienced historic underinvestment OR are at or above the 90th percentile for housing cost OR lack of green space OR lack of indoor plumbing OR lead paint</p> <p>AND (2) are at or above the 65th percentile for low income</p>
Legacy pollution	Transportation	Water and wastewater	Workforce Development
<p>(1) Have at least one abandoned mine land OR Formerly Used Defense Sites OR are at or above the 90th percentile for proximity to hazardous waste facilities OR proximity to Superfund sites (National Priorities List (NPL)) OR proximity to Risk Management Plan (RMP) facilities</p> <p>AND (2) are at or above the 65th percentile for low income</p>	<p>ARE (1) at or above the 90th percentile for diesel particulate matter exposure OR transportation barriers OR traffic proximity and volume</p> <p>AND (2) are at or above the 65th percentile for low income</p>	<p>ARE (1) at or above the 90th percentile for underground storage tanks and releases OR wastewater discharge</p> <p>AND (2) are at or above the 65th percentile for low income</p>	<p>ARE (1) at or above the 90th percentile for linguistic isolation OR low median income OR poverty OR unemployment</p> <p>AND (2) fewer than 10% of people ages 25 or older have a high school education (i.e. graduated with a high school diploma)</p>



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Figure 8-8. Map showing communities identified as disadvantaged based on the CEQ CEJST for the water and wastewater, climate change, workforce, and energy burden categories within the SFWMD region.



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Figure 8-9. Map showing communities identified as disadvantaged based on the CEQ CEJST for the transportation, housing, pollution, and health burden categories within the SFWMD region.

134

135 **EPA EJScreen**

136 The environmental Protection Agency (EPA) Environmental Justice screening and mapping tool
137 (EJScreen) conducts a preliminary assessment of communities most affected by environmental harms and
138 risks in a selected location. EJScreen incorporates data from various sources, including:

- 139 • EPA, Office of Air and Radiation (OAR) Fusion of Model and Monitor Data
- 140 • EPA, Office of Air Quality Planning and Standards, Air and Toxics Data Update
- 141 • U.S. Department of Transportation traffic data
- 142 • U.S. Census's American Community Survey
- 143 • Comprehensive Environmental Response, Compensation, and Liability Information
144 System (CERCLIS) database, National Priorities List and Superfund Alternative Approach
145 sites
- 146 • EPA, Risk Management Plan (RMP) database, facility data
- 147 • EPA, Resource Conservation and Recovery Act (RCRA) database (RCRAInf)
- 148 • EPA, Risk-Screening Environmental Indicators (RSEI) Model, Toxics Release Inventory
149 (TRI) data

150 These data serve as environmental indicators and socioeconomic factors for calculating the
151 environmental justice (EJ) and supplemental indexes. EJScreen comprises twelve EJ indexes and twelve
152 supplemental indexes in EJScreen, each representing twelve environmental indicators and either the
153 demographic index (which includes the average of two socioeconomic factors) or the supplemental
154 demographic index (which includes the average of five socioeconomic factors) (table 8-3). Each
155 environmental indicator and demographic index has its own separate EJ or supplemental index; there is no
156 cumulative score or single EJ index.

157 The supplemental indexes provide a more comprehensive analysis. To calculate a specific EJ index,
158 EJScreen applies a formula that combines an environmental indicator with the demographic index (EJ Index
159 = the Environmental Indicator Percentile for a Block Group X the Demographic Index for Block Group).
160 Similarly, a formula is applied that combines a single environmental factor with the supplemental
161 demographic indicator to calculate a single supplemental index (Supplemental Index = the Environmental
162 Indicator Percentile for Block Group X Supplemental Demographic Index for Block Group). The smallest
163 geographic unit for which census data is published is called a block, while a block group is a cluster of
164 blocks that form a subdivision of a census tract.

165 EJScreen does not classify communities in an area as socially vulnerable or disadvantaged. Instead, it
166 calculates environmental justice indexes to identify areas that may require further review, analysis, or
167 outreach as the EPA develops programs, policies, and other activities. SFWMD leverages local knowledge
168 of resiliency concerns and additional information to enhance the results of the Supplemental Indexes greater
169 than or equal to the state and national 40th percentile to incorporate socioeconomic and demographic
170 consideration into resiliency planning.

171

172 **Table 8-3.** EPA EJScreen and supplemental indexes and corresponding indicators. Sources:
 173 [Understanding EJScreen Results | US EPA](#) and [EJ and Supplemental Indexes in EJScreen | US EPA](#).

Environmental Justice (EJ) Index	Demographic Index	Supplemental Demographic Index
<ul style="list-style-type: none"> • Particulate Matter 2.5 • Ozone • Diesel Particulate Matter Air Toxics Cancer Risk • Air Toxics Respiratory Hazard Index • Traffic Proximity • Lead Paint • RMP Facility Proximity • Hazardous Waste Proximity • Superfund Proximity • Underground Storage Tanks • Wastewater Discharge 	<ul style="list-style-type: none"> • % low income • % people of color 	<ul style="list-style-type: none"> • % low income • % unemployed • % limited English speaking • % less than high school education • low life expectancy

174

175 **PROPOSED RANKING CRITERIA**

176 A multicriteria approach was developed to support the characterization and ranking of resiliency
 177 projects, including metrics that help to identify the most critical infrastructure associated with the most
 178 vulnerable areas. The selection of criteria were based on the Resilient Florida Program, as detailed below.
 179 This program is administered by the Florida Department of Environmental Protection (FDEP), and it allows
 180 water management districts to submit a list of proposed projects that mitigate the risks of flooding or SLR
 181 on water supplies or water resources of the state by September 1, annually. Each project submitted to the
 182 program must contain a description of the project, project location, completion schedule, cost estimate, and
 183 the cost share percentage available with a minimum of 50%. The legislation requires FDEP to implement
 184 a scoring system for assessing each project. The scoring system will include the following tiers and criteria:

- 185 1) Tier 1 must account for 40 percent of the total score and consist of all of the following criteria:

- 186 a) The degree to which the project addresses the risks posed by flooding and SLR identified in the
 187 local government vulnerability assessments or the comprehensive statewide flood vulnerability and
 188 SLR assessment, as applicable. (10%)
 189 b) The degree to which the project addresses risks to regionally significant assets. (10%)
 190 c) The degree to which the project reduces risks to areas with an overall higher percentage of
 191 vulnerable critical assets. (10%)
 192 d) The degree to which the project contributes to existing flooding mitigation projects that reduce
 193 upland damage costs by incorporating new or enhanced structures or restoration and revegetation
 194 projects. (10%)
- 195
- 196 2) Tier 2 must account for 30 percent of the total score and consist of all of the following criteria:
 197 a) The degree to which flooding, and erosion currently affect the condition of the project area (7.5%)
 198 b) The overall readiness of the project to proceed in a timely manner, considering the project's
 199 readiness for the construction phase of development, the status of required permits, the status of
 200 any needed easement acquisition, and the availability of local funding sources. (7.5%)
 201 c) The environmental habitat enhancement or inclusion of nature-based options for resilience, with
 202 priority given to state or federal critical habitat areas for threatened or endangered species. (7.5%)
 203 d) The cost-effectiveness of the project. (7.5%)
- 204
- 205 3) Tier 3 must account for 20 percent of the total score and consist of all of the following criteria:
 206 a) The availability of local, state, and federal matching funds, considering the status of the funding
 207 award, and federal authorization, if applicable. (6.5%)
 208 b) Previous state commitment and involvement in the project, considering previously funded phases,
 209 the total amount of previous state funding, and previous partial appropriations for the proposed
 210 project. (6.5%)
 211 c) The exceedance of the flood-resistant construction requirements of the Florida Building Code and
 212 applicable floodplain management regulations. (7%)
- 213
- 214 4) Tier 4 must account for 10 percent of the total score and consist of all the following criteria:
 215 a) The proposed innovative technologies designed to reduce project costs and provide regional
 216 collaboration. (5%)
 217 b) The extent to which the project assists financially disadvantaged communities. (5%)

218

219 Following the overall Resiliency Florida scoring system, and incorporating additional criteria that are
 220 relevant to characterize and to prioritize the most critical project needs in this Plan, the following criteria
 221 set has been implemented:

222 **Criteria Set 1: Likelihood of System Deficiencies**

223 ***FPLOS Phase I Assessment Results (Current and /or Future Conditions)***

224 Basin wide flood vulnerabilities, as part of FPLOS Phase I Assessment Results (or equivalent
 225 assessment): vulnerability of the drainage system within the project impact area to manage flood risks to
 226 adjacent developed or partially developed land under current and future conditions represented by the
 227 FPLOS overall flood protection level of service (i.e., 5-YR, 10-YR, 25-YR), as summarized in Phase I
 228 FPLOS Reports – Flood Vulnerability Assessments.

229 Note: When FPLOS Phase I Assessment Results are not yet available within the area of influence of a
230 project, but significant flooding events have been recently reported (as detailed below), all points will be
231 awarded to the proposed project.

232 ***Known chronic and nuisance flooding report***

233 Observed flooding events, with documentation by agencies/universities/media/citizens providing
234 evidence of significant flooding events in the project impact area in the past 5 years.

235 ***No Alternatives / Backup to Mitigate Worst Case Scenario***

236 The respective structure does not have an alternative operational routing or no system backup to
237 mitigate potential limitation in operation or the worst case scenario of structure failure, under extreme event
238 conditions.

239 ***Return Period of Overbank Flooding***

240 Infrastructure Performance Under Sea Level Scenarios or Extreme Rainfall Events (higher water levels
241 exceeding infrastructure design capacity): Frequency that canal overbank flooding and/or other
242 infrastructure bypass is observed onto the adjacent developed or partially developed floodplain (riverine
243 flooding) as a result of peak stage profile at any point along the canal system being higher than canal bank
244 / levee elevation (vulnerability of the drainage / flood protection system within the project impact area of
245 the proposed project). Excludes overbank flooding of non-saline water that results primarily in inundation
246 of wetlands or other natural areas.

247 ***Sea Level Resulting in Overbank Flooding***

248 Infrastructure Performance Under Sea Level Scenarios or Extreme Rainfall Events (higher water levels
249 exceeding infrastructure design capacity): Increase of sea levels that result in canal overbank flooding
250 and/or other infrastructure bypass resulting in increase in flood risks to developed or partially developed
251 adjacent land and water supplies (vulnerability of the drainage / flood protection / salinity barrier system
252 within the project impact area of the proposed project; proposed project will reduce in inundated areas).

253 ***Exceedance of Canal Normal Operating Range***

254 Infrastructure Performance Under Sea Level Scenarios or Extreme Rainfall Events (higher water levels
255 exceeding infrastructure design capacity): Maximum peak stage profile levels along the primary canal
256 system exceeding normal operational range stages (canal performance), which reduces discharges from
257 secondary systems, increasing flood risks further inland. Project will lower canal stages (reduce inundated
258 areas).

259 ***FFE < BFE***

260 Infrastructure Finish Floor Elevation Exposure: Comparison between Infrastructure Finish Floor
261 Elevation (FFE) and FEMA Base Flood Elevation (BFE), when applicable

262 ***FEMA Flood Zone (benefits set or likelihood set of criteria)***

263 Project impact area is within FEMA Flood Zone A, AH, AE, V and will lower flood risks (reduction
264 of inundated areas).

265 ***Storm Surge Inundation Exposure***

266 Project Impact Area (or Finished Floor Elevation, for infrastructure enhancement projects) is within
267 specific Hurricane Categories - Storm Surge event inundated area, when applicable, and project will lower
268 flood risks (reduce inundated areas).

269 Criteria Set 2: Consequence of System Deficiencies**270 Critical Assets/Lifelines Density**

271 Total number of Critical Assets (Lifelines: Water, Resource Facilities, Regional Medical Centers,
272 Emergency, Operations Centers, Regional Utilities, Major Transportation Hubs and Corridors, Airports and
273 Seaports) located within the project impact area of the proposed project.

274 Total number of Regional Significant Assets (Lifelines: Water, Resource Facilities, Regional Medical
275 Centers, Emergency, Operations Centers, Regional Utilities, Major Transportation Hubs and Corridors,
276 Airports and Seaports) located within the project impact area of the proposed project.

277 Impact Area Across Administrative Boundaries

278 Number of administrative and County boundaries across the area of influence, which characterizes
279 different levels of regional significance for the respective projects.

280 Social Vulnerability

281 CDC SVI: Percent of the communities within the proposed project's impact area are identified as
282 socially disadvantaged based on datasets available from the Center for Disease Control (CDC) Agency for
283 Toxic Substances and Disease Registry (ATSDR) Social Vulnerability Index (SVI) that consider economic
284 status, household characteristics, ethnicity and race, and access to transportation to determine
285 socioeconomic burden and vulnerability in a changing climate.

286 CEQ CEJST: Communities within the proposed project's impact area that are identified as socially
287 disadvantaged and vulnerable based on one of the eight datasets available from the Council on
288 Environmental Quality's (CEQ) Climate and Economic Justice Screening Tool (CEJST) that consider
289 economic status, household characteristics, ethnicity and race, illness, air, land, and water pollution,
290 transportation and traffic, greenspaces, and workforce development to determine socioeconomic burden
291 and vulnerability in a changing climate.

292 Environmental Protected Areas

293 Vulnerable environmental protected areas - state or federal critical habitat for threatened or endangered
294 species- within the project impact area of the proposed project, and that can be impacted by flooding events.

295 Total Population

296 Total number of people residing within the project impact area of the proposed project

297 Public Water Supply Wellfields

298 Vulnerable public water supply wellfields within 20,000ft of the 2018/2019 Saltwater Interface and
299 within the project impact area of the proposed project (when applicable – if proposed project influence
300 saltwater interface – dual purposes, e.g., coastal structures).

301 Adaptation Action Areas

302 Project impact area is within an established "Adaptation Action Area" or "Adaptation Area". Section
303 163.3164(1), Florida Statutes defines AAA as "a designation in the coastal management element of a local
304 government's comprehensive plan which identifies one or more areas that experience coastal flooding due
305 to extreme high tides and storm surge, and that are vulnerable to the related impacts of rising sea levels for
306 the purpose of prioritizing funding for infrastructure needs and adaptation planning." Equivalent priority
307 planning areas, as recommended by Counties, were also identified within project impact areas.

308 **Criteria Set 3: Benefits from System Enhancements**

309 ***Nature-based Solutions***

310 Project includes NBS or “green” infrastructure in addition to “gray” infrastructure improvements to
311 increase resiliency (Natural or semi-natural systems that provide water quality / ecosystem benefits,
312 environmental habitat enhancement).

313 ***Ecosystem Restoration***

314 Project included natural enhancements of the environment by restoring the lands and waters that benefit
315 wildlife.

316 ***Cost Benefit Analysis***

317 Cost-effectiveness of the project estimated as larger than one, estimated based on avoided economic
318 loss.

319 ***Previous State Commitment / Involvement***

320 Project received previous state funding into its previous phases, including pre-construction activities,
321 design, permitting or Phase I Construction.

322 ***Available Match***

323 Project includes documentation that 50% cost share is available, or funds will be available but have not
324 been appropriated or released.

325 ***Florida Building Code Design Criteria***

326 Exceedance of the flood-resistant requirements in the Florida Building Codes Act, as adopted by the
327 State of Florida pursuant to Part IV, Chapter 553, F.S. or local floodplain management ordinances.

328 ***Innovative Technologies***

329 Project proposal includes innovative technologies to optimize project benefits, protect communities and
330 the environment, reduce project costs and provide regional collaboration.

331 **Criteria Set 4: Project Status (SIP/CIP Programs)**

332 ***SIP Overall Rating-***

333 Performance level used to define the ability of the structure to perform intended function under current
334 conditions, as reported as part of SFWMD Structure Inspection Program Report (Final Category).

335 ***Capital Improvement Program (CIP) Status***

336 Project Status as part of the District fiscally constrained expenditure plan that lays out anticipated
337 infrastructure investments over the next five years. Project indication about Design or Pre-Design is stated
338 in the CIP.

339 **PROCESS FOR APPLYING CRITERIA**

340 To apply the criteria sets detailed above, project impact areas were established for each project, as
341 illustrated in the examples shown in Figure 8-14 below. Figures 8-15 through 8-18 summarize the ranking
342 point assignment distribution, overall assumptions and adopted weighting for each of the four categories of
343 criteria. The project impact areas were determined based on potential benefits to the communities and the

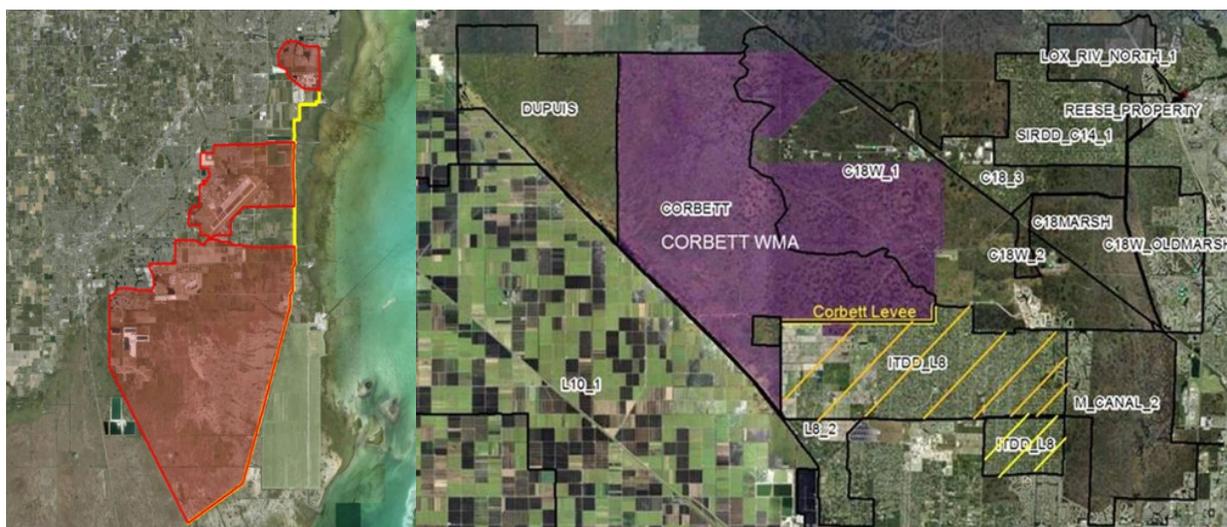
344 environment that the proposed infrastructure is expected to provide upstream and downstream of each
 345 project location. A wide range of information was considered to delineate the project impact areas,
 346 including, but not limited to H&H modeling, design technical manuals, storm surge inundation scenarios,
 347 SLR and saltwater intrusion studies, environmental restoration and impact assessments, existing conditions
 348 reports, local engineering expertise and discussions with District’s staff. Assumptions include the project’s
 349 ability to protect water supply and water resources of the state, increase the resilience levels of agricultural,
 350 natural and urban areas to flood conditions as well as improvement of wildlife corridors, habitat
 351 connectivity, salinity reduction, and water quality.

352 According to the Resilient Florida final rule language for Florida Rules Chapter 62S-8 Statewide
 353 Flooding and Sea Level Rise Resilience Plan, effective 8/22/2022, “Project impact area” means the discrete
 354 area the project encompasses as well as the delineated area that will be directly benefitted by a mitigation
 355 project (such as a watershed or hydrologic basin for flood mitigation projects, a service or sub-service area
 356 for a utility, a neighborhood, a natural area, or a shoreline).

357 All infrastructure projects receive a certain number of points for each of the evaluated criteria according
 358 to the evaluation of each respective project impact area and established weights. Projects with the highest
 359 combination of points, become the highest priority projects. Table 8-9 below lists the infrastructure projects
 360 and presents the total points obtained for each criteria subset, and overall points. Figures 8-19 through 8-23
 361 illustrate some of these adopted criteria, and how values vary spatially at each project impact area.

362 This ranking process will be updated continuously as part of future Resiliency Plan updates and as
 363 vulnerability assessment results and additional information becomes available. The new criteria established
 364 in this current plan differs from the criteria established in the 2021 Sea Level Rise and Flood Resiliency
 365 Plan, mainly because of the adoption of overall criteria and weights determined in the Resilient Florida
 366 final rule language for Chapter 62S-8 Statewide Flooding and Sea Level Rise Resilience Plan. Shifts in
 367 project priorities, relative to last planning cycle were observed and will be evaluated, individually, as part
 368 of the next planning cycle. A higher weight, in comparison to Chapter 62S-8, was assigned to the Likelihood
 369 of System Deficiency subset, and notably the criteria relative to FPLOS Flood Vulnerability Assessment
 370 results, which characterizes the degree of flooding risks at each assessed basin, utilizing the latest and
 371 greatest input data and most advanced modeling tools, coupling rainfall, storm surge and groundwater
 372 compound flooding risks.

373



374 **Figure 8-10.** Examples of Project Impact Areas from the Proposed L31 Levee Project (left) and the
 375 Corbett Levee (right).

376

Criteria	ID	Category	Weighting	Low Probability				High Probability
				1	2	3	4	5
Likelihood of System Deficiency	1.1	FPLOS Phase I Assessment Results (Current and /or Future Conditions)	15%	Future Conditions Less than 25-Year	Future Conditions 10-YR or less	Future Conditions 5-Yr or less	Current Conditions 10-YR or less	Current Conditions 5-YR or less
	1.2	Known Chronic and Nuisance Flooding Report (OR)	13%					Yes, flooded more than three times within the last five years or is experiencing ongoing erosion.
	1.3	No Alternatives/Backup to Mitigate Worst Case Scenario	3%			Partial		Yes
	1.4	Return Period of Overbank Flooding	6%	More than 100-yr	100-yr or less	50-yr or less	25-yr or less	5-yr or less
	1.5	Sea Level Resulting in Overbank Flooding		>3 ft	2 ft to 3 ft	1 ft to 2 ft	0.5 to 1 ft	0.5 ft or less
	1.6	Exceedance of Canal Normal Operating Range (OR)			Less than or Equal to 1 ft	More than 1 ft	> 2.5 ft	> 3.5 ft
	1.7	Finished Floor Elevation < Base Flood Elevation	3%			FFE < BFE + 1'	FFE < BFE + 2' (or 1' inland)	FFE < BFE + 3' (or 2' inland)
	1.8	FEMA Flood Zone Exposure						Yes
	1.9	Storm Surge Inundation Exposure				Yes, under Cat 3	Yes, under Cat 4	Yes, under Cat 5

377

378
379

Figure 8-11. Summary and Scoring System utilized for characterizing Criteria Set 1 “Likelihood of System Deficiency”.

Criteria	ID	Category	Weighting	Low Probability				High Probability
				1	2	3	4	5
Consequence of System Deficiency	2.1	Critical Assets / Lifelines	6%			0-25% of Critical Assets are within areas lower than 6FT or within inundated areas from FPLOS	25-50% of Critical Assets are within areas lower than 6FT or within inundated areas from FPLOS	More than 50% of Critical Assets are within areas lower than 6FT or within inundated areas from FPLOS
			6%			1 or more R5 Critical Assets	3 or more R5 Critical Assets	5 or more R5 Critical Assets
	2.2	Impact Area Across Administrative Boundaries	2.5%	1 County		1 County & 2 Administrative Boundaries		> 2 Counties & > 2 Administrative Boundaries
	2.3	Social Vulnerability (CDC SVI)	5.0%				0.4 - 0.6	> 0.6
		Social Vulnerability (CEQ CEJST)						Yes
	2.4	Environmental Protected Areas	3.5%	Lower Density		Average		Higher Density
	2.5	Total Population	1%	Up to 50,000 people	Up to 100,000 people	Up to 200,000 people	Up to 500,000 people	More than 500,000 people
	2.6	Public Water Supply Wellfields	5%	Lower Density		Average		Higher Density
2.7	Adaptation Action Areas	1%	Does not Intersect Adaptation Action Area				Intersect Adaptation Action Area	

380

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382

Figure 8-12. Summary and Scoring System utilized for characterizing Criteria Set 2 “Consequence of System Deficiency”.

383

Criteria	ID	Category	Weighting	Low Probability				High Probability
				1	2	3	4	5
Benefits from System Enhancement	3.1	Nature-based Solutions	5%					Yes
	3.2	Ecosystem Restoration						Yes
	3.3	Cost Benefit Analysis	2.5%					BCA Larger than 1
	3.4	Previous State Funding	2.5%		Previous State Funding utilized in Preconstruction activities	Previous State Funding utilized in Design	Previous State Funding utilized in Permitting	Previous State Funding utilized in Construction
	3.5	Available Match	2.5%			Specifically identified local, state, or federal cost share, but the funds have not been appropriated or released at the time the applicant submits its proposal to the FDEP		Approved and adopted capital improvement plan
	3.6	Florida Building Code Design Criteria	2.5%					Yes
	3.7	Innovative Technologies	5%					Yes

384

385 **Figure 8-13.** Summary and Scoring System utilized for characterizing Criteria Set 3 “Benefits from System Enhancement”.

387

Criteria	ID	Category	Weighting	Low Probability				High Probability
				1	2	3	4	5
Project Status (SIP / CIP Programs)	4.1	SIP Overall Rating	5%			Overall C-3 or N/A	Overall C-4	Overall C-5
	4.2	Capital Improvement Program (CIP) Status	5%	Issue ID & Risk Ranking	PDR Approved / Project Kick-off Meeting and/or Suvey & Geotech Commenced	Partial Design	Design Complete / Permit Application Submitted	Initiated Construction

388

389 **Figure 8-14.** Summary and Scoring System utilized for characterizing Criteria Set 4 “Project Status (SIP/CIP Programs)”.

391

392

393 **Table 8-4.** Ranking of Coastal Structure Projects (top) and Priority Projects (bottom) according to the
 394 pre-established criteria sets, and total summarized points.

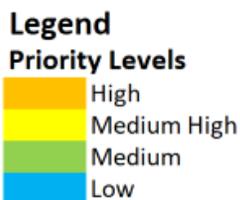
Coastal Structure Resiliency Projects	Likelihood of System Deficiency	Consequence of System Deficiency	Benefits from System Enhancement	Project Status	Total Points
S-26	38.25	24.16	18.75	5.00	86.16
S-29 & C-9 Basin Resiliency	35.30	24.16	17.50	4.00	80.96
S-27 & C-7 Basin Resiliency	39.50	21.26	16.25	3.00	80.01
S-21	39.50	19.26	16.25	4.00	79.01
G-57	37.05	21.56	16.25	4.00	78.86
S-28 & C-8 Basin Resiliency	36.50	21.06	16.25	3.00	76.81
S-37A	33.50	22.96	16.25	3.00	75.71
S-25B	35.25	15.06	18.75	5.00	74.06
G-58	39.50	14.01	16.25	4.00	73.76
G-93	33.50	18.01	16.25	6.00	73.76
S-22	36.50	16.96	16.25	3.00	72.71
S-25	37.00	15.26	16.25	3.00	71.51
S-197	37.05	13.35	16.25	3.00	69.65
G-54	27.50	22.76	16.25	3.00	69.51
S-20F	26.50	20.76	16.25	5.00	68.51
G-56	26.30	22.96	16.25	3.00	68.51
S-13	31.65	16.96	16.25	3.00	67.86
S-36	29.30	17.76	16.25	3.00	66.31
S-20G	26.50	17.01	16.25	4.00	63.76
S-123	26.50	16.76	16.25	3.00	62.51
S-33	19.30	22.56	16.25	3.00	61.11
S-20	26.50	13.35	16.25	3.00	59.10
S-21A	23.50	13.01	16.25	5.00	57.76

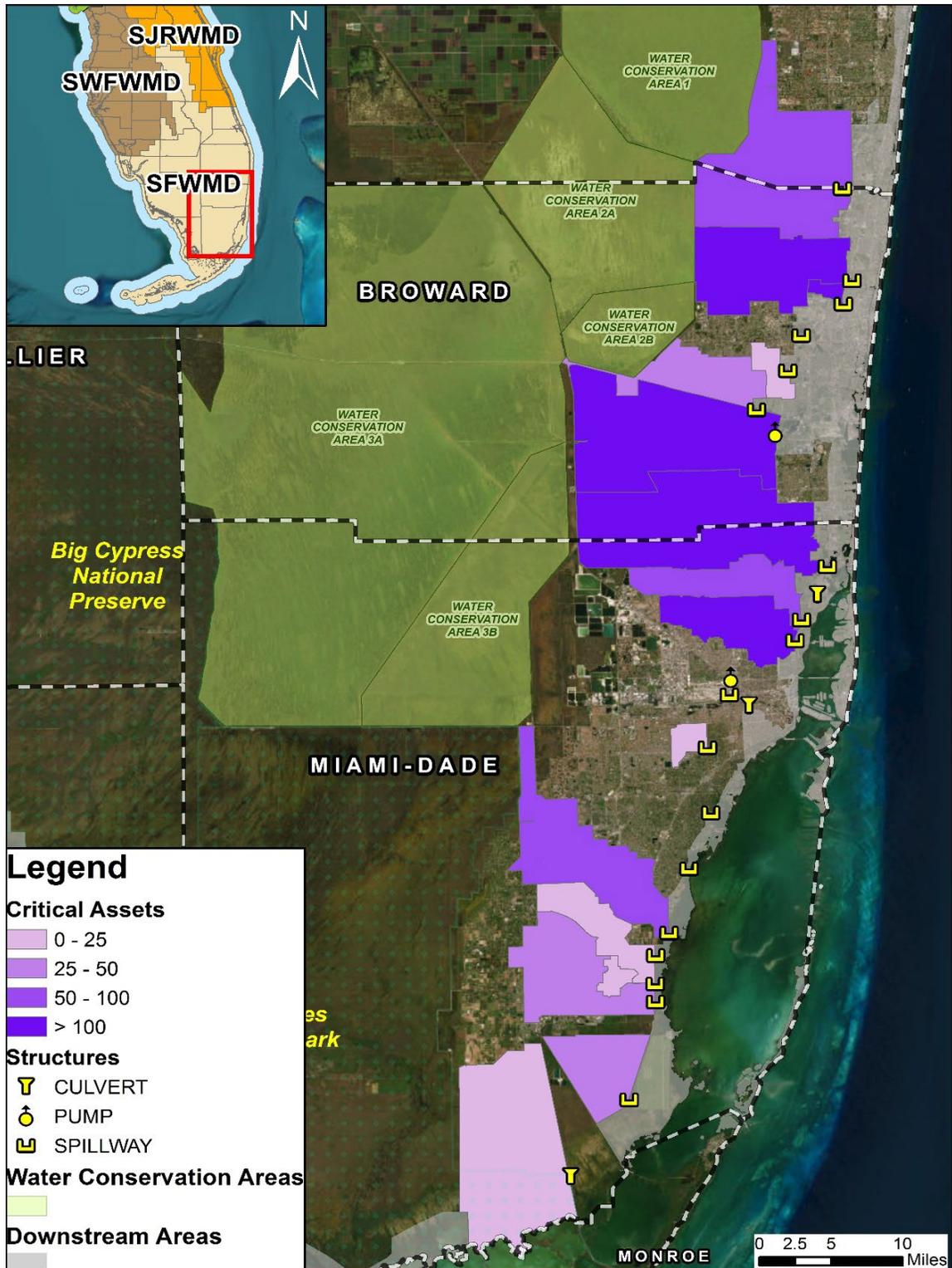
Other Priority Projects	Likelihood of System Deficiency	Consequence of System Deficiency	Benefits from System Enhancement	Project Status	Total Points
Big Cypress Basin Microwave Tower	39.50	22.96	17.50	4.00	83.96
S-61 Spillway Enhancement and Erosion Control	36.50	23.16	16.25	7.00	82.91
C-29, C-29A, C-29B and C-29C Canal Conveyance Improvements	36.50	23.16	16.25	6.00	81.91
S-59 Enhancement and C-31 Canal Conveyance Improvements	36.50	23.16	16.25	6.00	81.91
S-58 Structure Enhancement and Temporary Pump	36.50	23.16	16.25	6.00	81.91
L-31E Levee Improvements	35.85	20.16	16.25	4.00	76.26
EMMA	37.00	13.35	18.13	7.00	75.48
Corbett Levee Water Control Structures	36.25	15.01	17.50	6.00	74.76
South Miami-Dade Curtain Wall	31.00	21.96	18.75	3.00	74.71

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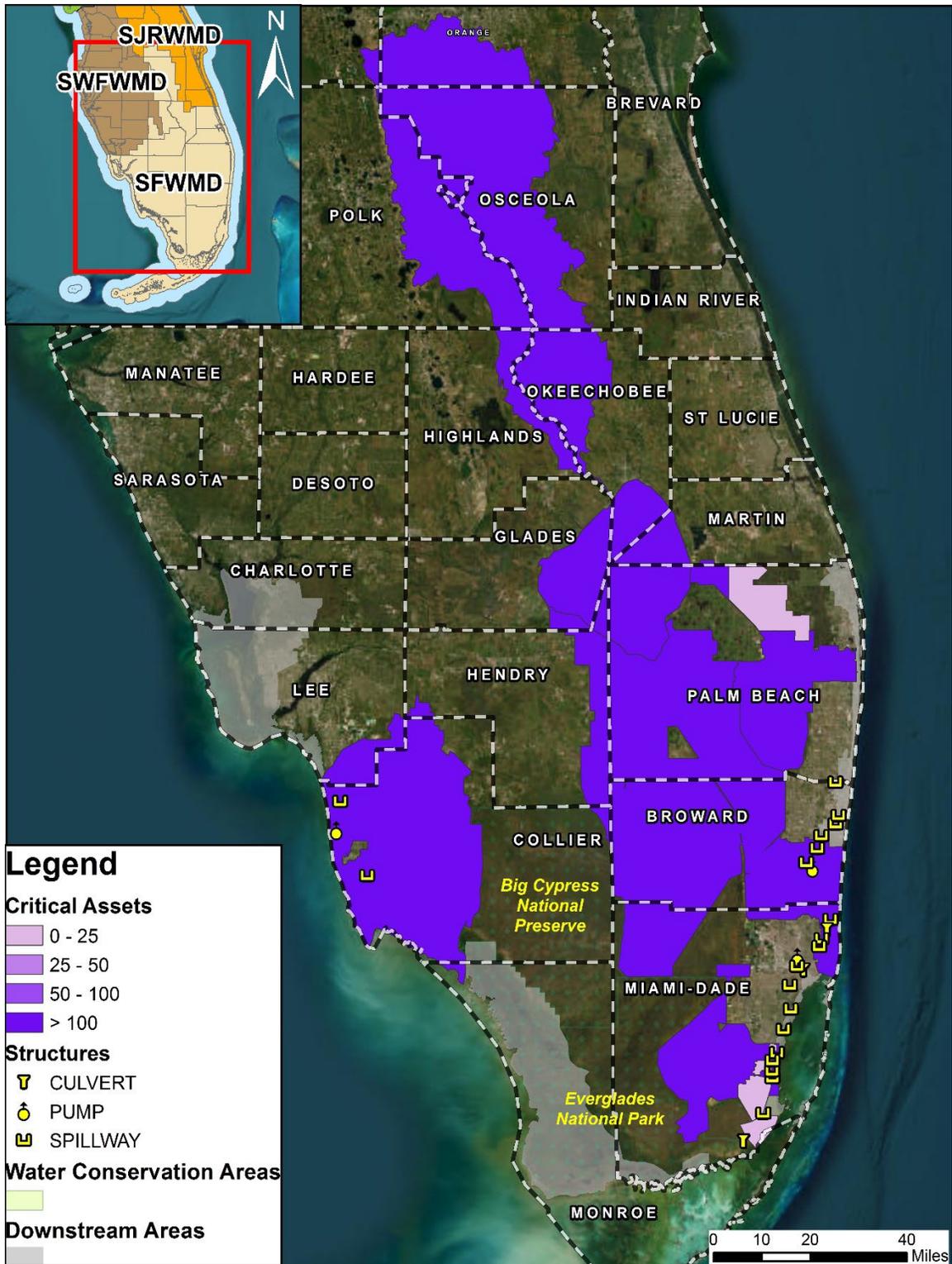




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399 **Figure 8-15.** Critical Assets (Lifelines) per Coastal Structures Resiliency Project Impact Areas, utilized
 400 as part of the Resiliency Projects Ranking Criteria Set 2.

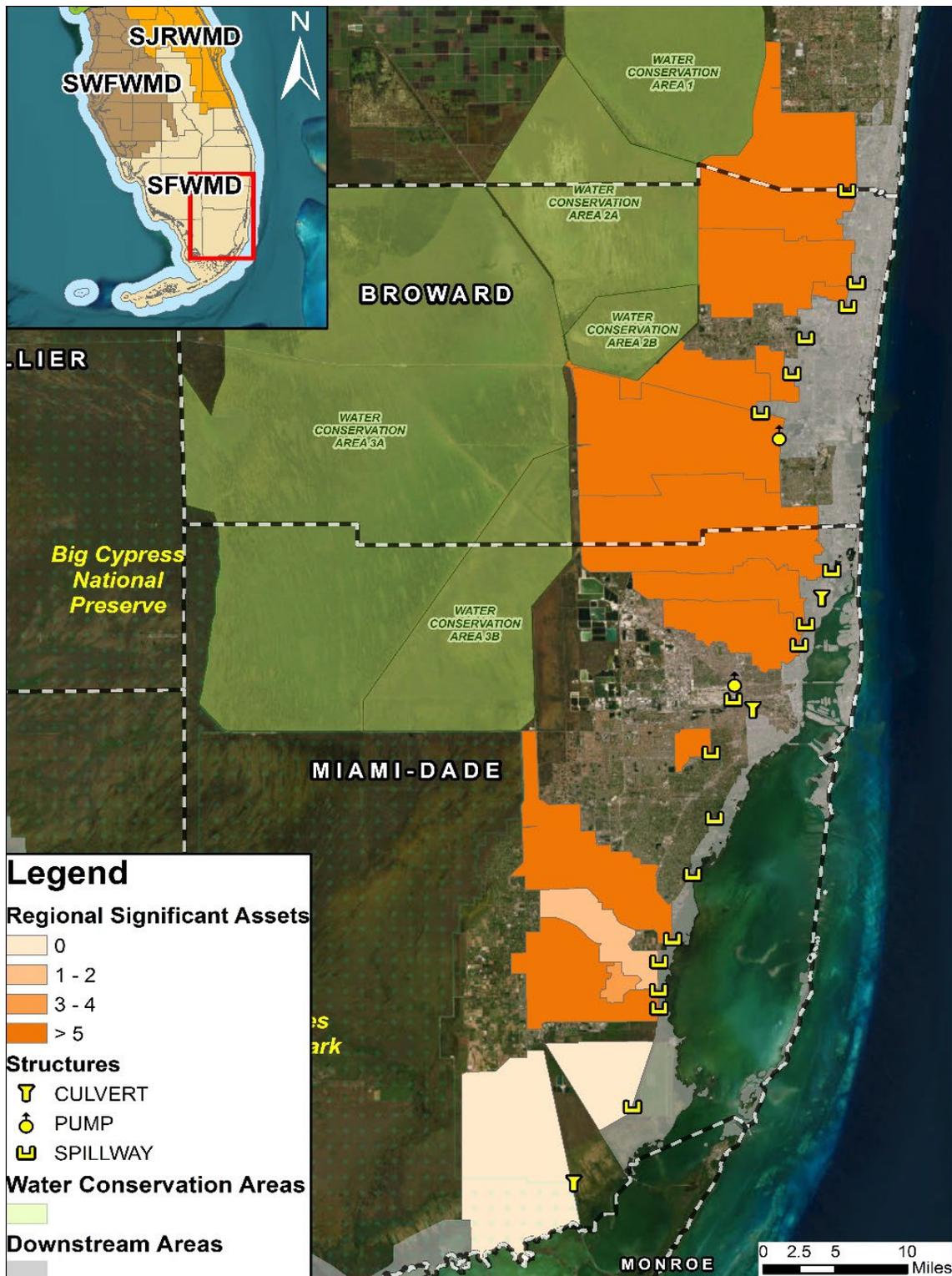
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402

403 **Figure 8-16.** Critical Assets (Lifelines) per Other Priority Project Impact Areas, utilized as part of the
 404 Resiliency Projects Ranking Criteria Set 2.

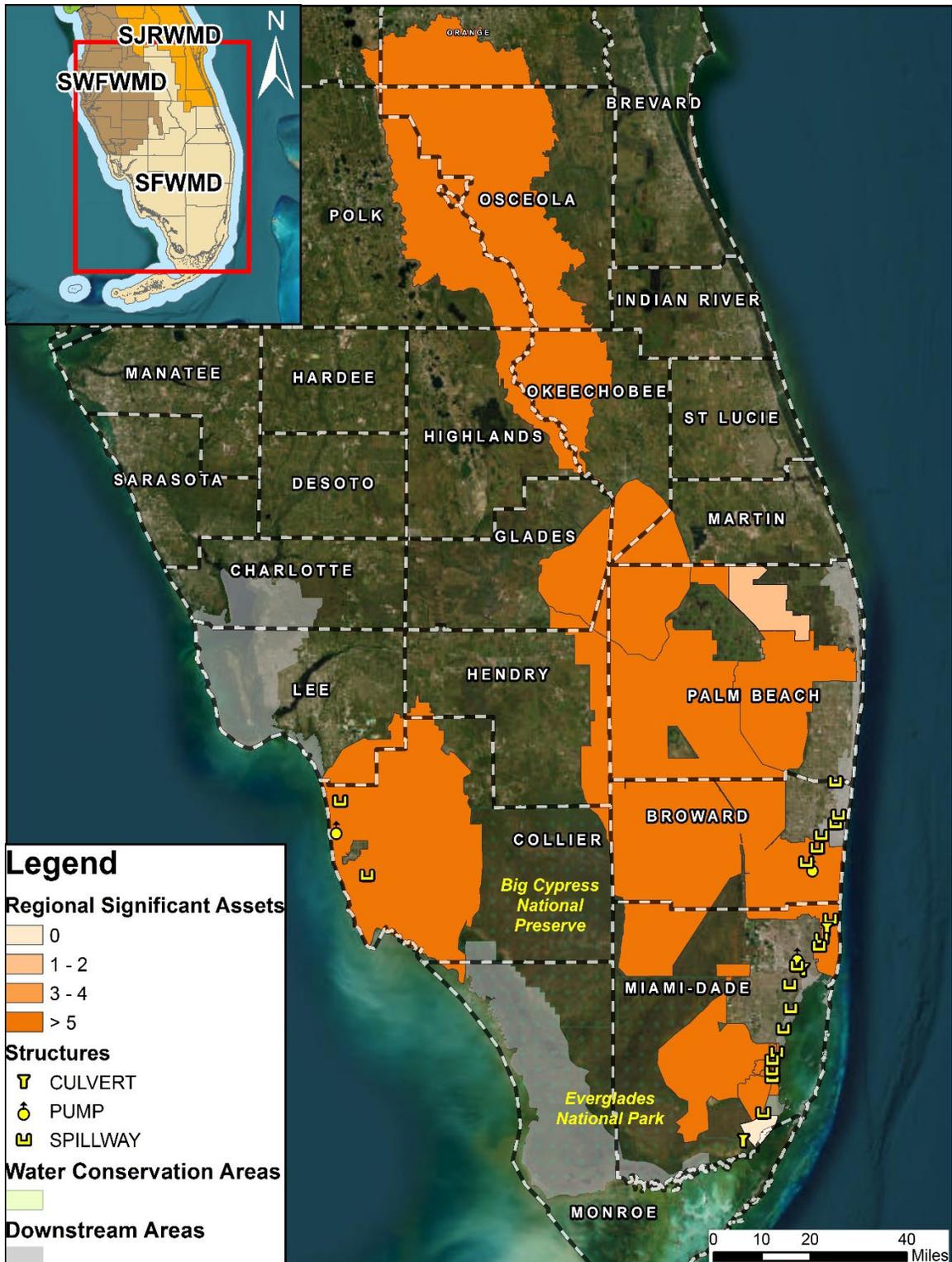
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Figure 8-17. Regional Significant Assets per Coastal Structures Resiliency Project Impact Areas, utilized as part of the Resiliency Projects Ranking Criteria Set 2.

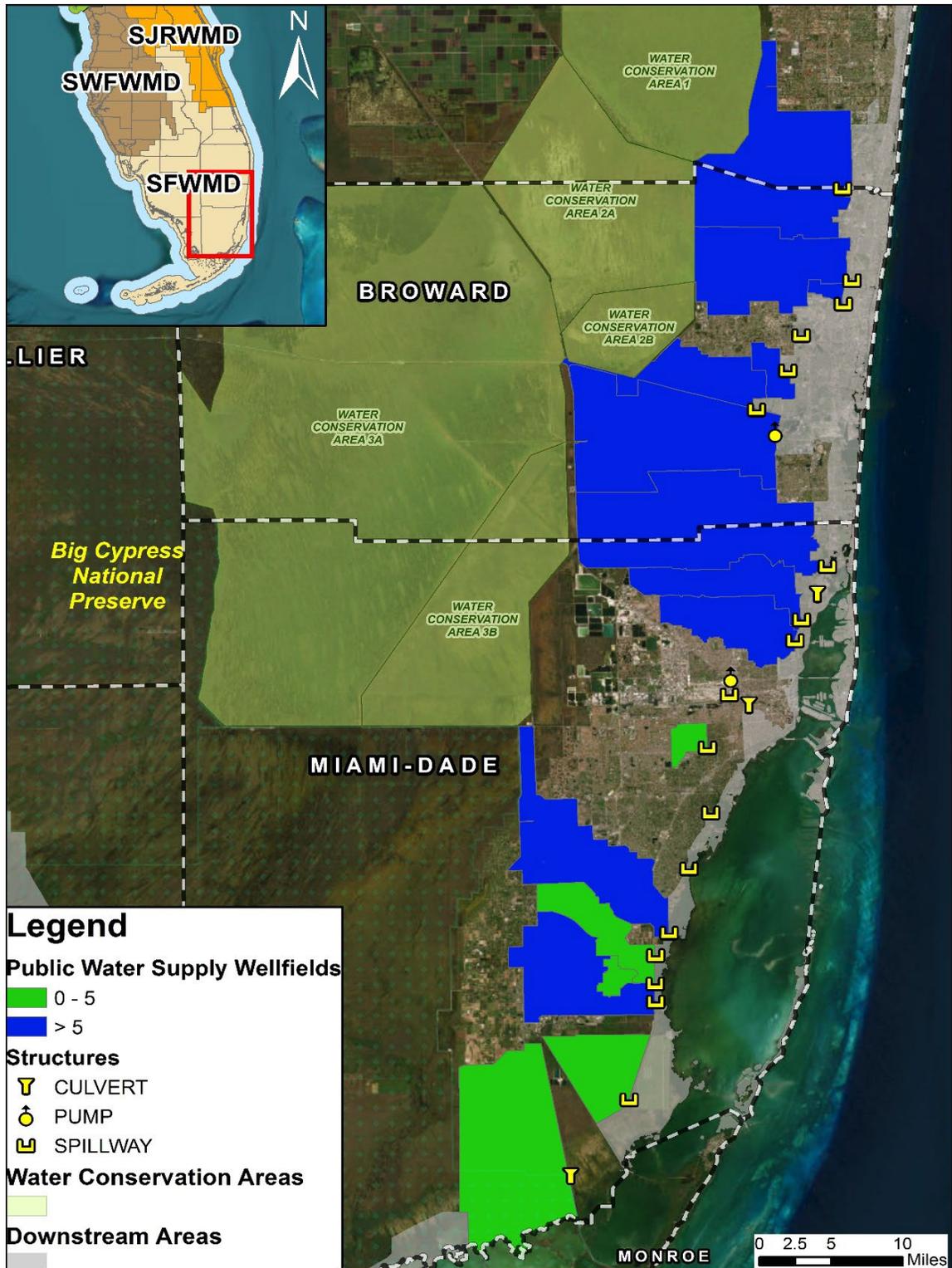
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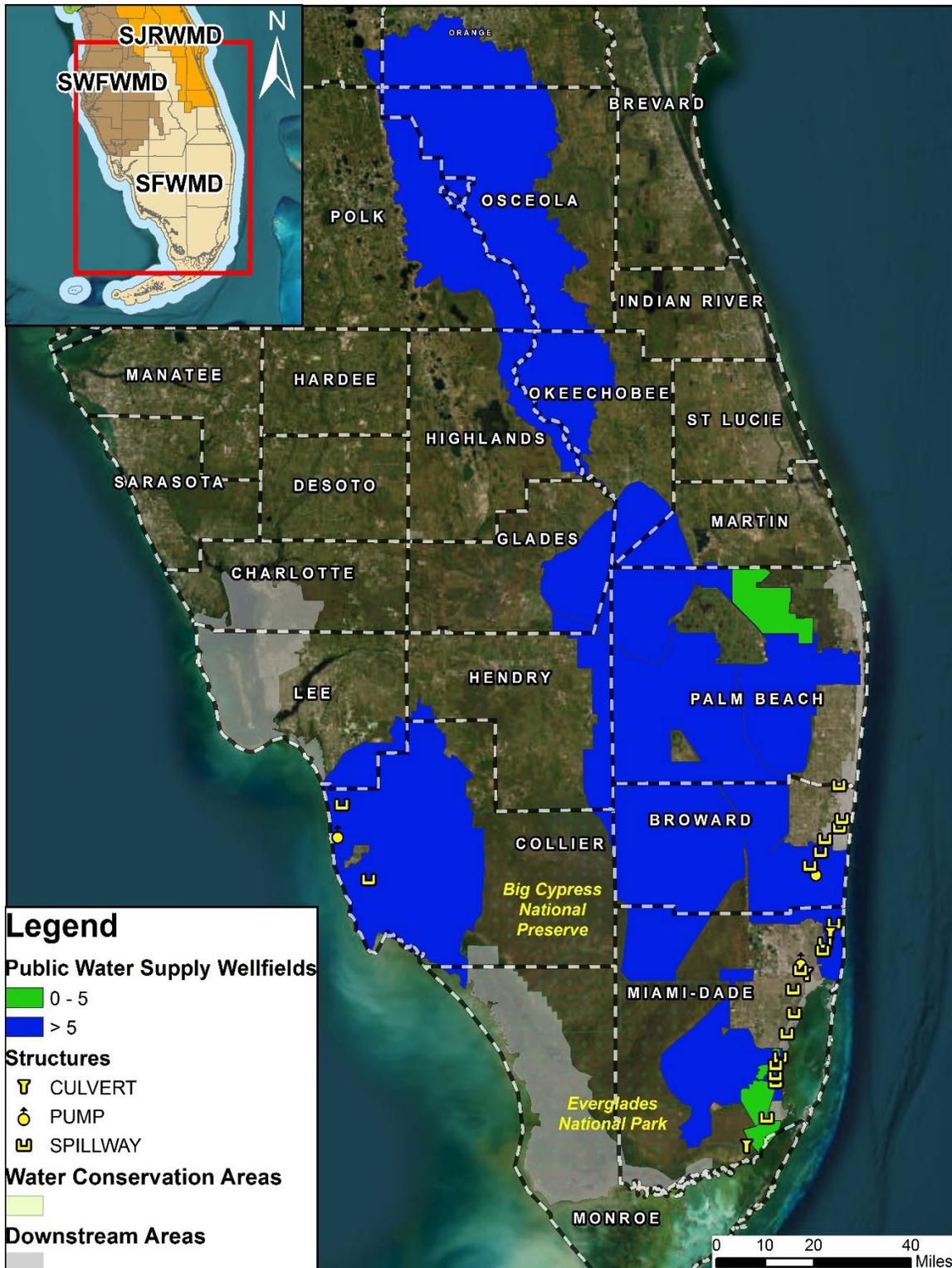
Figure 8-18. Regional Significant Assets per Other Project Impact Areas, utilized as part of the Resiliency Projects Ranking Criteria Set 2.



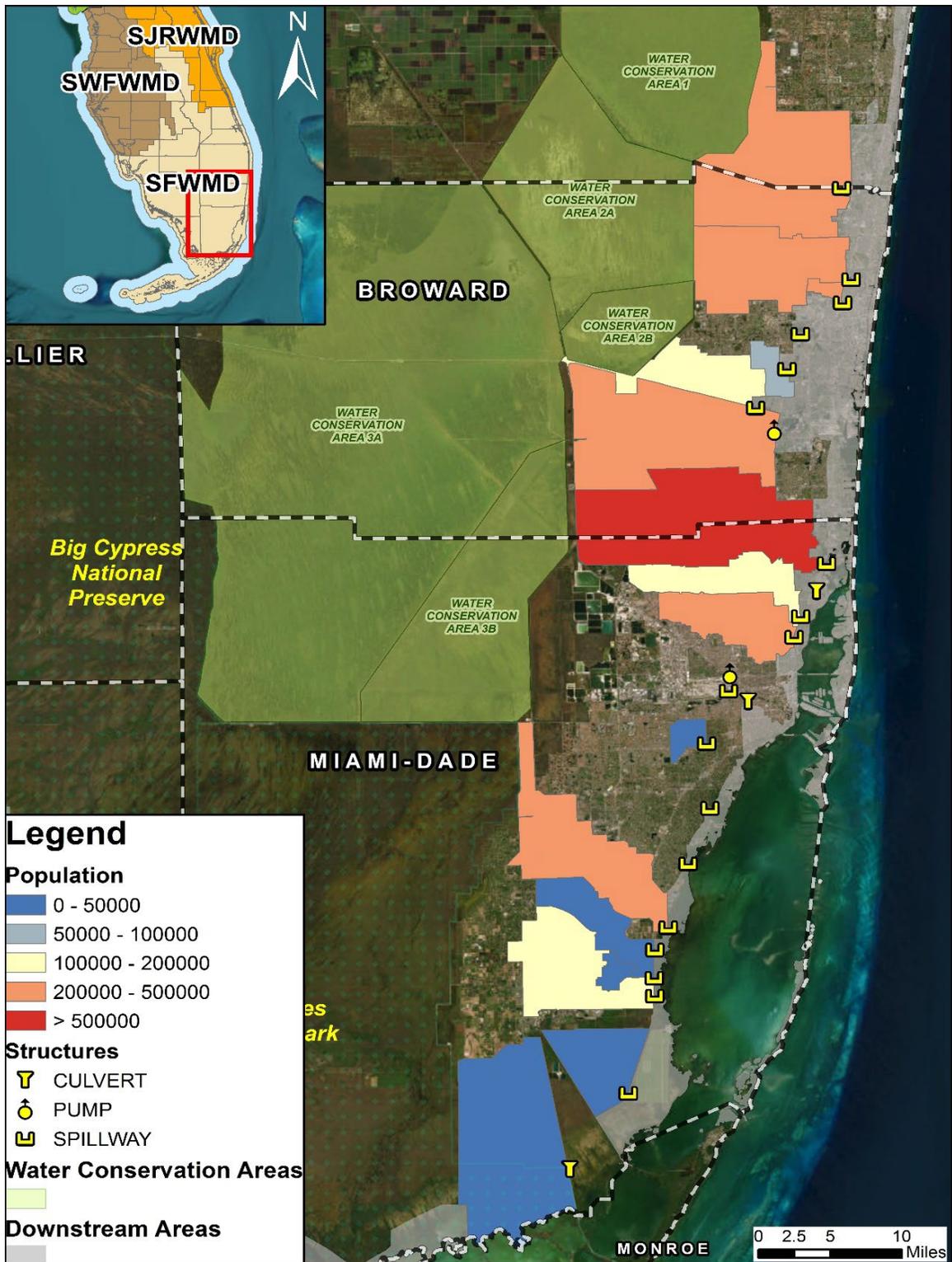
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414 **Figure 8-19.** Public Water Supply Wellfields per Coastal Structures Resiliency Project Impact Areas,
 415 utilized as part of the Resiliency Projects Ranking Criteria Set 2.

416

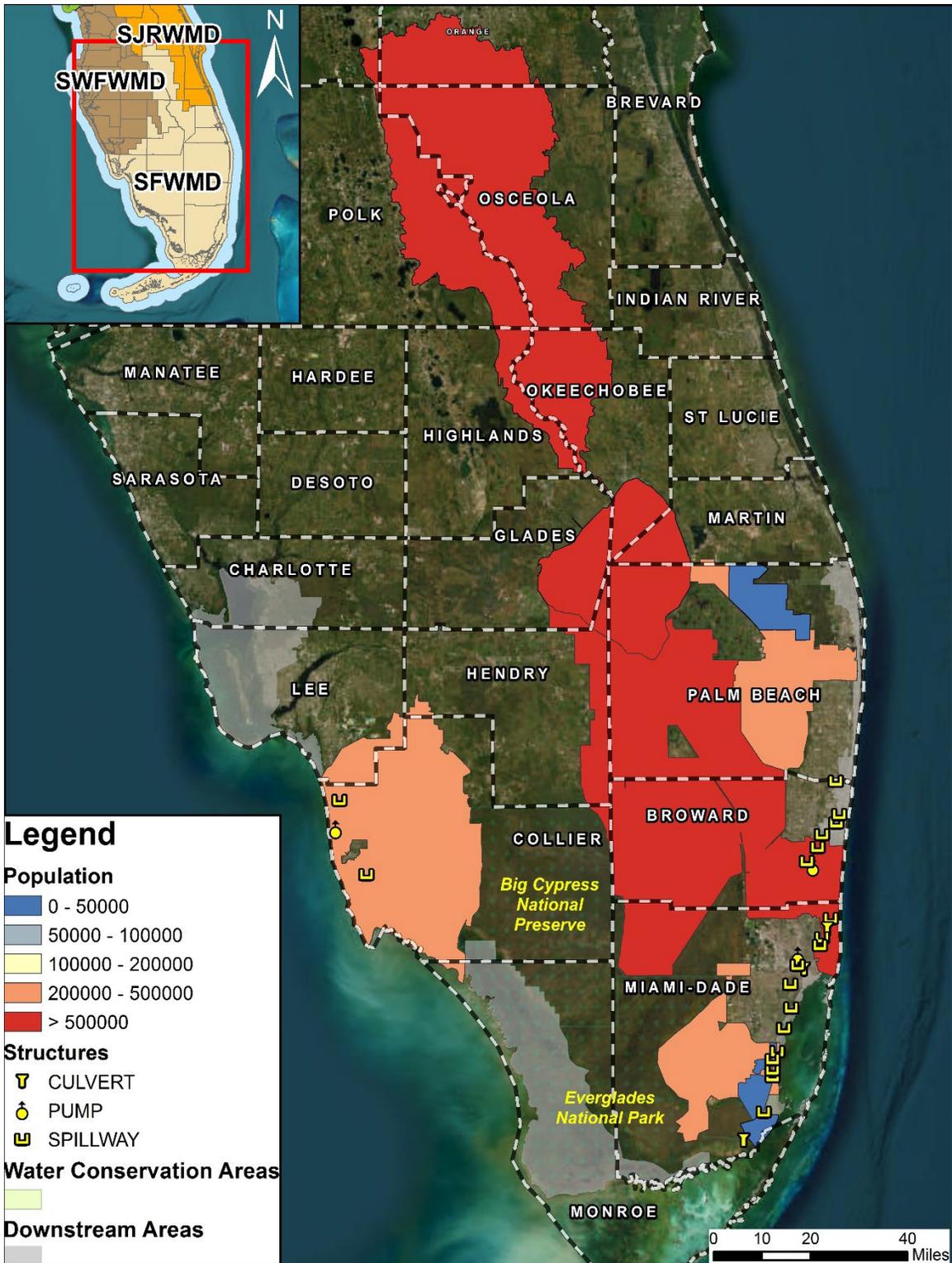


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 418 **Figure 8-20.** Public Water Supply Wellfields per Other Project Impact Areas utilized as part of the
 419 Resiliency Projects Ranking Criteria Set 2.



420

421 **Figure 8-21.** Total Population per Coastal Structures Resiliency Project Impact Areas, utilized as part of
 422 the Resiliency Projects Ranking Criteria Set 2.



423

424 **Figure 8-22.** Total Population per Other Project Impact Areas utilized as part of the Resiliency Projects
 425 Ranking Criteria Set 2.

426

Chapter 9: Enhancing our Water Management Systems: Priority Implementation Projects

OUR MISSION AND RESILIENCY

The South Florida Water Management District's (District or SFWMD) mission is to safeguard and restore South Florida's water resources and ecosystems, protect our communities from flooding, and meet the region's water needs while connecting with the public and stakeholders. Resiliency, for current and future conditions, is embedded in each mission element:

Flood Control: Flood Control is part of the District's mission since its creation, as the Central and Southern Florida Flood Control District in 1949. Operations and Maintenance staff operate and oversee approximately 2,175 miles of canals and 2,130 miles of levees/berms, 89 pump stations, 915 water control structures and weirs and 621 project culverts. As part of this responsibility, the District has been implementing its Capital Improvement Program (CIP) to ensure investment in the maintenance of the flood control assets, a Structure Inspection Program (SIP) to routinely inspect and assess the structural integrity and operation of the flood control assets and, more recently, the Flood Protection Level of Service (FPLOS) program to comprehensively assess the system's ability to meet and continue to meet the flood protection needs of the region into the future. These programs are critical to keeping South Florida habitable and its primary flood control system functioning as designed, today and into the future.

Water Supply Planning: Water supply planning is essential to meet the growing demands of 9 million residents, millions of visitors, businesses, and the environment. Section 373.790 F.S. requires the District to develop and update regional water supply plans, approximately every five years with a planning horizon of 20 years, to ensure that the available water resources in the region are sufficient to meet future water needs. These plans also identify measures to achieve demands where deficiencies are found, including promoting water conservation and the use of alternative water supplies. The District has taken steps to include sea level rise (SLR) and climate change impacts in water supply planning efforts, and maintains a Saltwater Interface Monitoring and Mapping Program, to determine the approximate location of the saltwater interface since 2009, with updated maps every five years. Future conditions saltwater intrusion scenario projections are being simulated as part of the upcoming Lower East Coast Water Supply Plan and follow up water supply vulnerability assessment.

Ecosystem restoration: Numerous ecosystem restoration projects are being planned, built, and operated to protect and preserve South Florida's unique ecosystems, including the Everglades, the Kissimmee River, Lake Okeechobee, and a diverse array of coastal watersheds. The most prominent of these efforts is the Comprehensive Everglades Restoration Plan (CERP), a cost-share partnership between the State of Florida and the Federal government to restore, protect and preserve the greater Everglades. Ecosystem Restoration supports the District's efforts to address the effects of climate change and SLR by building systemwide resiliency. Completed CERP projects will increase the District's ability to better manage anticipated extreme weather events. The restoration of beneficial freshwater flows throughout the system slows down saltwater intrusion promoting more sustainable aquifer recharge rates, healthier estuaries and bays, more stable coastlines, and reduced occurrence of marsh dry outs.

41 This Resiliency Plan document, and particularly the list of priority implementation projects included in this
 42 chapter, reflects the status of resiliency incorporation into each of the District’s mission elements, summarized
 43 above. As demonstrated throughout the document and in the list and figure below (Figure 9-1), resiliency
 44 strategies in support of our water supply mission are still in a relatively nascent (emerging) stage, when typical
 45 efforts are characterized by vulnerability assessments and exploratory studies, with more short-term and
 46 localized adaptation strategies being prioritized. The flood protection mission is in a more advanced and
 47 transforming stage, with resiliency strategies that include adaptation, supported by robust technical assessments
 48 in place for over a decade, through the FPLOS Program. Therefore, the flood resiliency projects included in
 49 this chapter are supported by detailed technical analysis with consideration for how these projects are sized
 50 to address current and future evolving conditions. Similarly, work in support of ecosystem restoration,
 51 including model development, analyses, implementation of projects and assessment of project performance
 52 is substantive and has been building resiliency in South Florida for over two decades time. More recently,
 53 restoration studies are integrating SLR as part of future conditions assessments, such as the Biscayne Bay
 54 Southeastern Everglades Ecosystem (BBSEER) study. The goal over the next decade is to move each of
 55 the mission areas to mature stages, as adaptation strategies become clearer and more comprehensive for
 56 building resiliency in South Florida.

Conceptual Resiliency Maturity by Mission Area

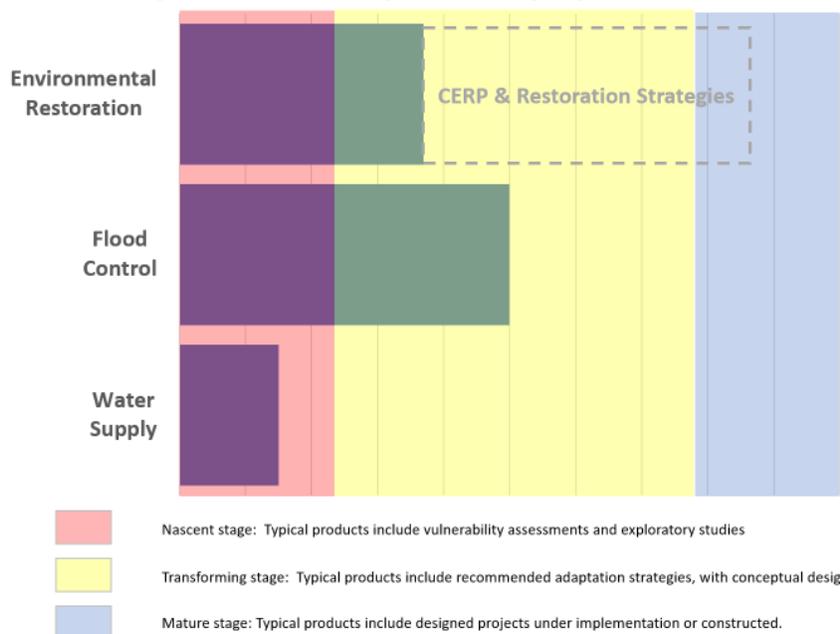


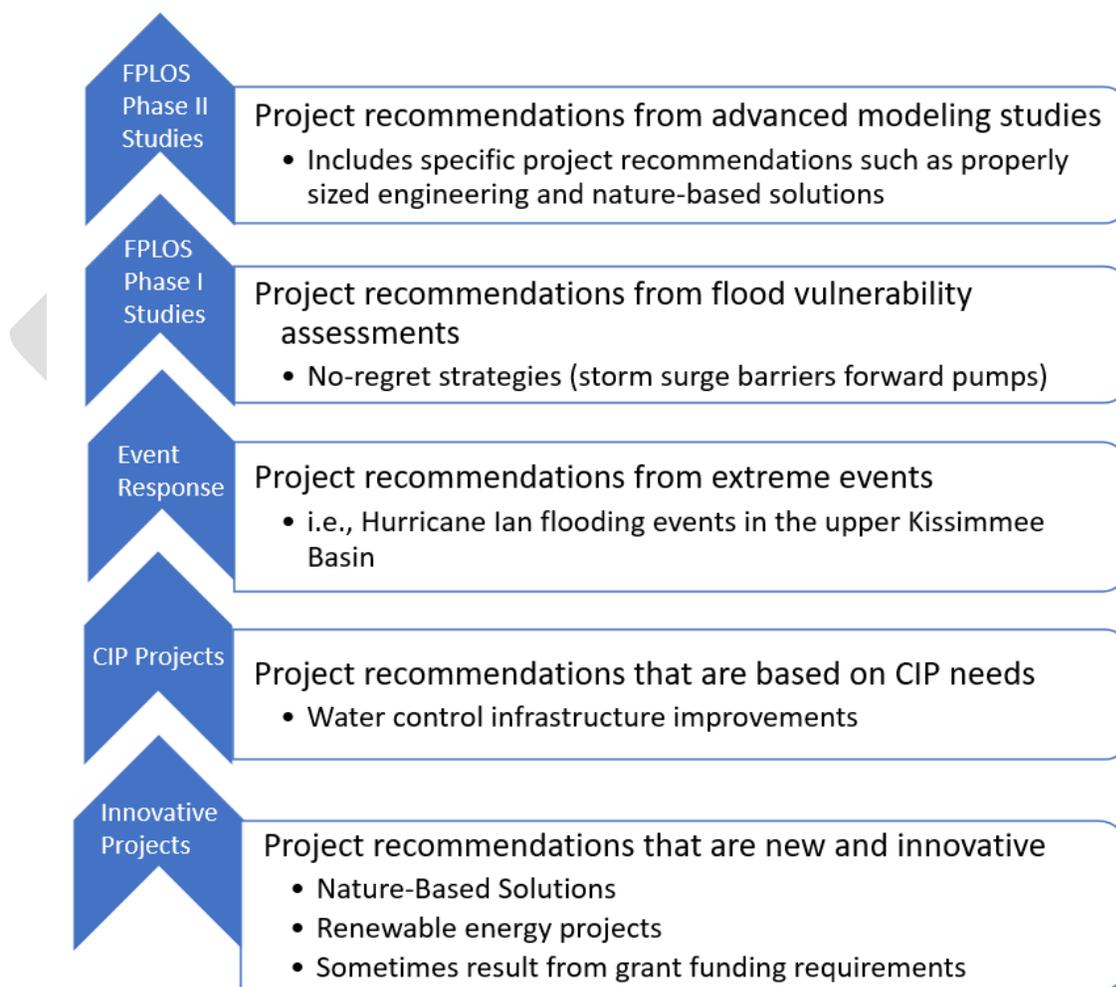
Figure 9-1: Conceptual Resiliency Maturity by Mission Area

57 It is important to recognize that this plan is constantly evolving. The objective is to incorporate
 58 resiliency strategies that include robust adaptation solutions supported by integrated technical assessments,
 59 detailed analyses and projects designed to address current and future conditions. The primary sources of
 60 projects formulated for this plan are detailed in figure 9-2 and include FPLOS Phase II Studies, FPLOS
 61 Phase I Studies, Post Storm/Event Response, CIP and Innovative Projects. Recommendations with the
 62 strongest technical support are listed first. These are the projects that have been validated with the most
 63 advanced modeling and future scenario assessments.
 64
 65

66 FPLOS Phase II project recommendations are the result of robust, comprehensive feasibility studies
 67 that evaluate a set of alternative adaptation strategies throughout the system (including primary, secondary,
 68 and tertiary systems). These studies assess the potential effects of implementing the project and the
 69 quantified benefits for flood risk reduction basin wide, which will inform basis for design as the following

70 step. FPLSO Phase II recommendations also include project sequencing so that planning is adaptable to
 71 evolving conditions and projects are implemented as needed, and based on the determination of thresholds
 72 established to maintain appropriate flood protection level of service.

73 FPLSO Phase I project recommendations are projects identified based upon the results of flood
 74 vulnerability assessments, not yet validated through adaptation planning modeling. They include no-regret
 75 strategies such as enhancing coastal structures, building forward pump stations, storage options and flood
 76 barriers at coastal structures. Post Storm or Event response recommendations are developed based upon the
 77 characterized impacts and pre-identified response actions to extreme events such as hurricanes and extreme
 78 rainfall events. During and after extreme events, the District water managers operate the system in the most
 79 efficient manner and might make adjustments to how the system is operated to help relieve flooding, as
 80 needed. Event response project recommendations aim to build upon what is learned from pre-, during- and
 81 post-storm operations, along with observed limitations to the water management system, and develop best
 82 response strategies for system enhancement. Capital Improvement Plan project recommendations are
 83 projects that are based on CIP and Operations and Maintenance regular needs. These projects are driven by
 84 the need to replace, repair and/or enhance aging or damaged flood control infrastructure and are aligned
 85 with resiliency goals. Innovative Project Recommendations are new and innovative ideas that may need to
 86 be further assessed before they are fully developed. They can include project features such as nature-based
 87 solutions (NBS) and/or renewable energy project features. Project features that are the result of grant
 88 funding requirements often fall under this category as well.



89 **Figure 9-2:** Diagram describing how projects are formulated and entered in this plan.

90 **RESILIENCY PRIORITY IMPLEMENTATION PROJECTS – COST**
91 **ESTIMATES**

92 The list of priority resiliency implementation projects includes investments needed to increase the
93 resiliency of the District’s coastal structures, such as structure enhancement recommendations and
94 additional SLR adaptation needs that include NBS along with traditional gray infrastructure enhancements.
95 These projects represent urgent actions to address the vulnerability of the existing flood protection
96 infrastructure. Additional project recommendations comprise basin-wide flood adaptation strategies that
97 are based upon FPLOS recommendations that protect water supply and water resources of the State.
98 Examples of these projects include adding “self-preservation mode” functionality to water control
99 structures, construction of the South Miami-Dade Curtain Wall, L31E Levee improvements, the J.W.
100 Corbett Wildlife Management Area Hydrologic Restoration and Levee Resiliency project and the
101 Everglades Mangrove Migration Assessment project (EMMA). The EMMA project is being proposed to
102 capture the adaptive foundational resilience of coastal wetlands within the District, and to demonstrate the
103 ability of coastal wetlands to adapt to rising sea levels via enhanced soil elevation change. Each of these
104 projects help to increase the functionality and capacity of the District’s flood control system and protection
105 of the environment..

106 Many of the projects described in this plan include adding forward pump stations to coastal water
107 control structures to restore the original flood protection level of service. These projects can have
108 downstream water quality impacts. To neutralize these impacts, projects with forward pump stations also
109 include nature-based features to improve water quality within the basin to offset downstream impacts. The
110 cost estimates for structure improvements were prepared using the District’s current understanding of
111 construction cost in the marketplace and historical costs from projects of similar scope. Additionally, the
112 District followed cost estimating procedures such as those employed by the U.S. Army Corps of Engineers.
113 The initial sizing of each proposed pump station is based upon the recent FPLOS study results. Pump station
114 discharge capacity was calculated using one quarter of the design discharge capacity of the structure. For
115 instance, a structure with a discharge capacity of 1000 cfs would need a 250 cfs pump station.

116 The pump station cost estimates were calculated by a Professional Engineer certified in the State of
117 Florida. Estimates were based upon the District’s record of pump station costs from 2006 to present and
118 adjusted for coastal conditions in Miami-Dade County. The cost estimates for each forward pump station
119 were calculated based upon the range of pumping capacity of the pump station (Table 9-1). For example, a
120 250 cfs pump station would cost \$13,750,000 as the cost per unit of discharge for the “up to 250 cfs range”
121 is \$55,000. All estimated costs include backup generators, as appropriate, and the schedules for
122 implementation of the Coastal Structure Refurbishment and Forward Pump Projects is estimated at an
123 average of 1.5 years for design and 2.5 years for construction. Schedules will be adjusted based upon
124 confirmation of project implementation. Real Estate costs were determined for the S-27 and S-29 Coastal
125 Structures and range from \$8M - \$16M depending on the project footprint and the land use within the areas
126 surrounding the project. An initial placeholder of \$7M for real estate costs, as well as \$2M for tying the
127 structure back to higher elevation were included in all the structure cost estimates and will be refined during
128 the pre-design stage. Cost estimates for forward pumps and respective backup generators (at 10% of pump
129 total costs) are also included, but forward pumps may not be recommended for all the structures. Feasibility
130 studies, conducted as part of FPLOS Phase II efforts, will confirm the need for forward pumps. All cost
131 estimates have been updated for 2023 according to SFWMD Engineering and Construction
132 recommendations, based on the building structure cost index adjustment from January 2022 to June 2023
133 of 2% lower than the 2022 estimates.

134 All new developed structures and components will exceed existing and expected future flood related
135 codes. The State of Florida Building code established the minimum floor elevation by determining the
136 Baseline Flood Elevation (100-year flood line) per ASCE 24-14, plus 1 (one) foot. The Miami-Dade County
137 Code (Chapter 11C) is at regulatory flood elevation (100-year flood).

138 **Table 9-1.** Summary of Cost Assumptions.

Pump Capacity % (from Design Discharge)	
Medium and High Impact Structures	50%
Medium, Medium Low and Low Impact	25%

139

Forward Pump Cost Estimates		
Cubic Feet per Second	Threshold	Cost per Unit Discharge
Up to 250	250	\$68,750
250-500	500	\$66,250
500-750	750	\$63,750
750-1000	1000	\$62,500
>1000	Other	\$60,000

140

Real Estate Costs – Placeholder Average Costs	\$8,750,000
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141

Forward Pump Backup Generator	10% of forward pump costs
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142

Tie-back (flood barriers around coastal structure)	\$2,500,000
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143

144

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146 **CAPITAL IMPROVEMENT PLAN – PRIORITY PROJECTS**

147 Priority Resiliency implementation projects were evaluated to confirm that we are using an integrated
 148 strategy for implementation. An analysis was completed to identify how each individual CIP project is
 149 related to this plan’s recommended resiliency projects. The analysis identified projects that have common
 150 objectives or overlapping impact areas and that can optimize benefits and continue to ensure that the water
 151 management system is operating at peak efficiency.

152 The District CIP infrastructure investments have been making system improvements beyond the needs
 153 identified in Operations and Maintenance inspection reports. These investments are enhancing District’s
 154 water management systems with additional components and operational capacity, making it possible for
 155 the 70-plus year old system to function and ensuring the District’s flood control mission is accomplished.
 156 These ongoing resiliency investments, along with new proposed enhancements that account for future
 157 conditions, are being implemented through a bundling strategy. Table 9-2 presents a list of CIP projects
 158 that will continue to enhance the C&SF System and Big Cypress Basin. More information about these
 159 projects can be found in the District’s CIP.

160
 161 **Table 9-2.** List of CIP priority projects.

Category	Project Names
Canal and Levee Conveyance	C-100A Tree Removal & Bank Stabilization C25 Canal Bank Repairs (Hurricane Irma) Canals C16, G16, C14, C41, C1W, C1N, C15 C40, C23, C24, C25 Dredge/Bank Stabilization Hillsboro Package 3 L8 Tieback - Boil Repair/Dupuis Canal Backfill
Communication/Control and Telemetry Upgrades and Replacement	Manatee Gate Control Panel Replacements Picayune Command & Control Center SCADA Stilling Well/Platform(C&SF) SCADA Stilling Well/Platform (STA) Tower Repair Program
Field Facilities Construction Upgrades and Replacement	Fort Lauderdale Field Station Modifications Homestead Field Station Replacement Miami Field Station Modifications and Replacements Gate Overhauls: Sandblast, Air Compressor Facilities Underground Storage Tank Replacements West Palm Beach Field Station Modifications O&M Facility Construction/Improvements Staff Support
Project Culvert Replacement	Large Project Culvert Replacements – Multiple Sites PC Culvert Project Replacements & Removals - MS PC Replacements ~ STCL FS PC to Bridge conversion PC Replacements ~ WPB FS Area, 6 Sites on L15
Pump Station Upgrades and Replacement	Arc Flash Program Automation Upgrades: G310, G335, S319, S362

Category	Project Names
	G-251 Dewatering Provision G310 Trash Rake Refurb/Replace G-310/G-335 Pump Overhaul G335 Trash Rake Refurb/Replace G370/372 Trash Rake, Fuel Farm & Structural L8 FEB / G539 PS - Resiliency Upgrades L8 FEB Flap Gate Purchase / Retrofit Pump/Engine Overhauls (C&SF) Pump/Engine Overhauls (C&SF) Grant Pump/Engine Overhauls (STA) S2, S3, S4 Pump Refurbishments S2, S3, S4, S7, S8 Engine Control Panel Hardening S-331 Command & Control Center Comm (Multiple Sites) S6 Package 1 S6 Pump Refurbishment S7 Pump Refurbishment S-9/S-9A Trash Rakes & Refurbishment Pump Station Modification/Repair Staff Support
Structure Upgrades and Replacement	Fall Protection G57 Wingwall Replacement & G16 G6A/S6 Access Bridge G93 IT Shelter and Structure Refurbishment Gate/Hydro Cylinder Overhauls (C&SF) Gate/Hydro Cylinder Overhauls (STA) Generator Replacement Program Hoist Conversion Project S179 & future conversions S167 Wingwall Replacement S169W Trash Rake S26 Major Refurbishment S65 Spillway Replacement S65A Spillway Replacement S65D Spillway Replacement S70 Replacement S71 Replacement S49 Replacement STA1W Structure Refurbishments & Replacements STA1E Outflow Structure Generator Addition STA1WE1 Outflow Structures Generator Additions Structure/Bridge Modification/Repair Staff Support

163 **DISTRICT RESILIENCY PRIORITY PROJECTS**

164 The list of priority resiliency implementation projects (Table 9-3), is presented below, showing the
 165 status of funding and how the project is linked to the District’s mission.

166
 167 **Table 9-3:** List of Resiliency Priority Projects showing how the project is linked to the District’s mission
 168 as well as implementation and funding status.

Project Name	Mission	Source	Status of Implementation	Status of Funding
S-28 Coastal Structure and C-8 Basin Resiliency	Flood Control, Water Supply, Ecosystem Restoration	FPLOS Phase II	Not Started (Conceptual Design Completed)	Partially funded \$50M FEMA BRIC + SFWMD & MDC Match
S-29 Coastal Structure and C-9 Basin Resiliency	Flood Control, Water Supply, Ecosystem Restoration	FPLOS Phase II	Ongoing Design	Design Funds Only (SFWMD)
S-27 Coastal Structure and C-7 Basin Resiliency	Flood Control, Water Supply, Ecosystem Restoration	FPLOS Phase II (Pilot)	Ongoing Design	Design Funds Only (SFWMD)
S-26 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
G-57 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-22 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-37A Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
G-58 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-123 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-20F Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-21 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
G-93 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded

Project Name	Mission	Source	Status of Implementation	Status of Funding
S-25B Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
G-56 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
G-54 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-25 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-33 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-20G Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-13 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-36 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-197 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
S-20 Coastal Structure Resiliency	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
Remaining Coastal Structures Resiliency	Flood Control, Water Supply	FPLOS Phase I (not yet completed)	Not Started	Not yet funded
L-31 Levee Improvements	Flood Control, Water Supply	FPLOS Phase I	Not Started	Not yet funded
Self-Preservation	Flood Control, Water Supply	CIP/Post Storm	Ongoing Design	Fully Funded \$6.3M FDEP Resilient Florida + SFWMD Match
Hardening Of S-2, S-3, S-4, S-7, S-8 Engine Control Panels	Flood Control, Water Supply	CIP	Ongoing Design & Construction Initiation	Fully Funded \$8.5M FDEP Resilient Florida + SFWMD Match
L8 FEB / G-539 Pump Resiliency Upgrades	Flood Control, Water Supply	CIP	Ongoing Design	Fully Funded \$4M FDEP Resilient Florida + SFWMD Match

Project Name	Mission	Source	Status of Implementation	Status of Funding
Corbett WMA Hydrologic Restoration and Levee Resiliency	Flood Control, Water Supply, Environmental Restoration	Post Storm / Event Response	Ongoing Design	Fully Funded \$7.7M Palm Beach County FDEP RF + SFWMD, ITID, PBC, FWC Match
C-29, C-29A, C-29B and C29C Canal Conveyance Improvements	Flood Control	Post Storm / Event Response	Not Started	Not yet funded
S-59 Structure Enhancement and C-31 Canal Conveyance Improvements	Flood Control	Post Storm / Event Response	Not Started	Not yet funded
S-58 Structure Enhancement and Temporary Pump	Flood Control	Post Storm / Event Response	Not Started	Not yet funded
S-61 Spillway Enhancement and Erosion Control	Flood Control	Post Storm / Event Response	Not Started	Not yet funded
Corbett Levee Water Control Structures	Flood Control	Post Storm / Event Response	Not Started	Not yet funded
Big Cypress Basin Microwave Tower	Flood Control, Water Supply	Post Storm / Event Response	Not Started	Not yet funded
Everglades Mangrove Migration Assessment (EMMA)	Flood Control, Water Supply, Environmental Restoration	Innovative Projects	Not Started (Conceptual Design Completed)	Not yet funded
Mangrove Experimental Manipulation Exercise (MEME)	Flood Control, Water Supply, Environmental Restoration	Innovative Projects	Not Started (Conceptual Design Completed)	Partially funded (SFWMD)
South Miami-Dade Curtain Wall	Flood Control, Water Supply	Innovative Projects	Not Started	Not yet funded
Renewable Energy Projects	Flood Control, Water Supply, Environmental Restoration	Innovative Projects	Not Started	Not yet funded

170 **S-28 COASTAL STRUCTURE AND C-8 BASIN RESILIENCY**

171 This resiliency project is mainly tied to the District’s mission to provide flood control, water supply
 172 protection, and ecosystem restoration. An example of a project that is proposing to use a combination of
 173 NBS and gray infrastructure is the District’s C-8 Basin project in Miami-Dade County. The District has
 174 been awarded FEMA grant funding to advance flood risk reduction measures in the C-8 Basin, a region of
 175 about 270,000 people that covers 28 square miles, in the northeastern portion of Miami Dade County. It is
 176 estimate that an additional 70,000 workers, travelers, and visitors are using the area for employment,
 177 transportation, and recreation. In addition, 96 critical assets would be protected under the proposed project.
 178 These include Airports (1), Faith Based Facilities (38), Fire Stations (6), Hazardous Waste Transport
 179 Facilities (3), Heliports (1), Hospitals/Medical Facilities (6), Law Enforcement Centers (6), and Public
 180 Schools (33). Overall flood protection levels of service will improve and water supply protection from
 181 saltwater intrusion will increase. This means that 13% of the most populous county in Florida will benefit
 182 from an increased level of flood protection. The area drained by the C-8 Canal is fully developed with
 183 primarily residential and commercial uses. The C-8 Canal is the central flood control feature that receives
 184 and conveys basin floodwaters by gravity through the S-28 Coastal Structure to sea.

185 S-28 is a reinforced concrete, gated spillway,
 186 with discharge controlled by two cable operated,
 187 vertical lift gates that are 17.5 feet high by 27.8
 188 feet wide. The structure has a discharge capacity
 189 of 3,220 cfs. S-28 is in the City of Miami near
 190 the mouth of C-8 about a mile from the shore of
 191 Biscayne Bay. S-28 is a gravity structure, and
 192 the designed discharge capacity is achieved
 193 when the gradient between head and tail water
 194 are sufficient to pass the flow. Operation of the
 195 gates is automatically controlled so that the gate
 196 hydraulic operating system opens or closes the
 197 gates in accordance with the operational criteria.
 198 The S-28 Structure was designed to 1) maintain
 199 optimum water control stages upstream in C-8,
 200 2) release the design flood (100 percent of the
 201 Standard Project Flood) without exceeding
 202 upstream flood design stage, 3) restrict
 203 downstream flood stages and discharge
 204 velocities to non-damaging levels, and 4)
 205 prevent saltwater intrusion during periods of
 206 extreme high flood tides. The impacts of SLR at
 207 S-28 Coastal Structures are illustrated in Figure 9-3,
 208 demonstrating the risks of saltwater overtopping the
 gates and minimum freeboard requirements as early as 2040.

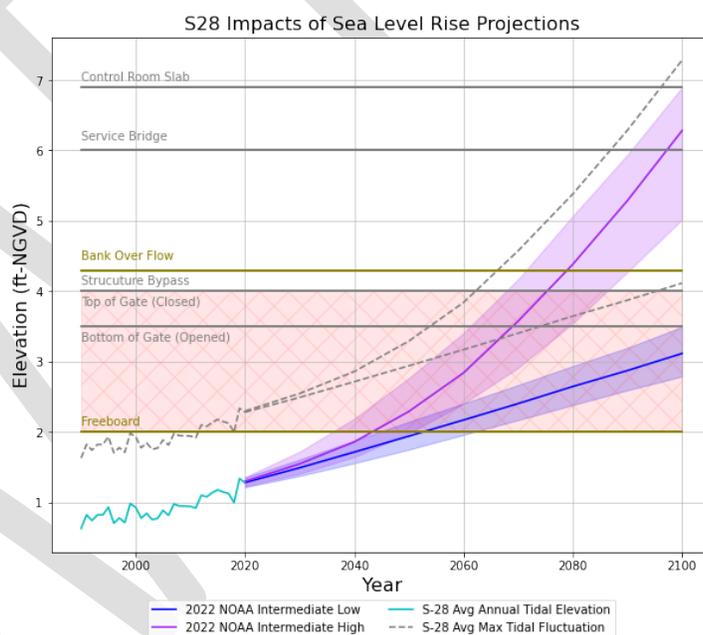


Figure 9-3. S-28 Impacts of Sea Level Rise Projections.

209 **Percent of Population Impacted**

210 One hundred percent of the population currently living in the C-8 basin, estimated at 270,000 people,
 211 will either directly or indirectly benefit from this project. We estimate an additional 70,000 workers,
 212 travelers, and visitors using the area for employment, transportation, and recreation. This means that 13%
 213 of the most populous county in Florida will benefit from an increased level of protection.

214 **Community-Wide Benefits**

215 Miami Dade County has been shifting to incorporate a wider range of co-benefits (social,
 216 environmental, operational) into their projects to consider equity community-wide. In the context of the

217 proposed project, “community-wide” refers to the historic, cultural, and recreational values that South
218 Florida residents share. This project is aligned with the County’s goals of promoting resilience in a way
219 that goes beyond environmental sustainability ([https://www.miamidade.gov/global/management/strategic-
220 plan/home.page](https://www.miamidade.gov/global/management/strategic-plan/home.page)). The County encourages jurisdictions to take a holistic approach for resilience efforts
221 across four broad dimensions: Leadership and Strategy, Economy and Society, Health and Wellbeing, and
222 Infrastructure and Environment. Their vision is “Delivering excellent service today and tomorrow”. The
223 SFWMD works closely with the County and local jurisdictions to instill these values, particularly in respect
224 to preparing for disasters and extreme events.

225 **Impacts to Lifelines**

226 This project will reduce direct and cascading flood impacts to Community Lifelines, residents,
227 businesses, public services, infrastructure, and natural systems through three key lifelines: Food, Water,
228 Shelter, Transportation, and Energy. Food, Water, Shelter - The proposed project significantly reduces the
229 threat to property. Under the lifeline subcategory of shelter, the project increases the level of protection for
230 over 200,000 primary homes across the area (and nearly 16,000 commercial, industrial, government,
231 education, and religion buildings). Without the project, it would take months for residents whose homes
232 may be significantly damaged to stabilize their living situation. Given the level of damage expected,
233 residents would be displaced while repairs to homes occurred. All the Village of Miami Shore's single-
234 family homes are on septic tank systems. The septic tank systems east of NE 12th Avenue are particularly
235 vulnerable to SLR. In recent years, several properties in the Village have had to retrofit their septic system
236 due to system failure. Alleviation of flooding would minimize future failures.

237 **Transportation**

238 The golf course is bordered by Biscayne Blvd (US. 1) to the east. This road is a key evacuation route
239 and connector for the region. The project would alleviate flooding and allow this main artery to flow during
240 extreme events.

241 **Safety and Security**

242 In addition, 96 critical assets would be protected under the proposed project. These include Airports
243 (1), Faith Based Facilities (38), Fire Stations (6), Hazardous Waste Transport Facilities (3), Heliports (1),
244 Hospitals/Medical Facilities (6), Law Enforcement Centers (6), and Public Schools (33). Overall flood
245 protection levels of service will improve and water supply protection from saltwater intrusion will increase.
246 The proposed project removes a portion of utility infrastructure from the floodplain.

247 **Impacts to Disadvantaged Communities**

248 According to ACS Census, approximately 19% of the population living in the C-8 basin is considered
249 financially disadvantaged. The CDC Social Vulnerability Index shows the census tracts to the north of the
250 project area are in the highest vulnerability ranking. The proposed project has positive direct and indirect
251 (ancillary) impacts related to risk reduction which will benefit these vulnerable communities. The project
252 will improve existing open space amenities, provide regional flood resilience, and leverage public
253 investment in ongoing resiliency efforts through coordination with local partners. Ancillary impacts of the
254 proposed green infrastructure will improve water quality, air quality, habitat creation, economic
255 opportunity, reduced social vulnerability, cultural resources, public health, and mental health. These
256 benefits are mainly related to the flood risk reduction measures, environmental benefits, and the
257 opportunities created for recreation and development.

258

259

260

261 **Project Scope**

262 This project will reduce flood risk under sea-level rise and provide ancillary water quality benefits, by
263 restoring the basin's flood protection level of service and enhancing quality of life in the region. The project
264 includes:

265 FPLoS Phase II Recommendations:

- 266 • S-28 Costal Structure Replacement: replacing major components of the S-28 Structure with a new
267 elevated, gated, water control structure. Converting the gate opening system to a more robust
268 mechanism, replacing the existing gates with corrosion resistant stainless-steel gates and increased
269 height, replacing the control building with a hardened and elevated control building, and adding a
270 corrosion control system to the structure
- 271 • Forward Pump: building a new 2550 cfs forward pump station that will convey flood waters to tide
272 when downstream water elevations are too high to allow gravity flow. The design of the proposed
273 forward pump station will be adaptable and will include the ability to add additional pumps in the
274 future as conditions continue to change.
- 275 • Tie Back Levee: Constructing a tie-back levee to provide flood and storm surge protection and
276 supporting the required function of the spillway gates and pump during a 100-year event with three-
277 foot SLR.
- 278 • Canal Improvements: including improving geometry, widening, and elevating and enhancing canal
279 banks throughout the basin, including the S-28 Coastal Structure immediate of C-8 Canal, as well
280 as the most vulnerable locations along the secondary system (Marco Canal, NW 17 AVE Canal,
281 Red Road/NW 57 AVE Canal, Spur #4 Canal, Spur Canal, Upper Rio Vista Canal), in partnership
282 with Miami Dade county.
- 283 • Storage: Adding approximately 250-acre feet of distributed storage in the C-8 Basin.

284 Additional stormwater green infrastructure project components:

- 285 • Building vegetated berms and constructing a temporary impoundment to reduce runoff, therefore
286 reducing peak flood elevations by storing water on the Miami Shores Golf Course during extreme
287 events until canal elevations subside allowing the impoundment to drain slowly and including a
288 gated culvert to connect the detention area to the C-8 Canal. Beneficial reuse of excavated
289 sediments from ditches/ponds to build levees, berms.
- 290 • Installing living shoreline features to assist in reducing bank erosion, improve aesthetics and storm
291 resiliency. Ancillary benefits include creation of aquatic habitat and water quality benefits which
292 will increase recreational value in the project area (kayaking, canoeing, wildlife observation and
293 fishing)

294 **Adaptation and Mitigation Study for the C-8 Basin**

295 The proposed C-8 Basin Resiliency Project was advanced following completion of flood vulnerability
296 assessments and findings of a need for major refurbishment of S-28 Structure, through the Structure
297 Inspection Program. The project, a no-regret strategy at the time of its inception, is currently in design. The
298 recently completed comprehensive study of the C-8 basin, (FPLoS Phase II Studies in the C-8 and C-9
299 Basins, 2023), confirmed the C-8 Basin project elements, evaluated the potential downstream impacts and
300 water quality impacts to Biscayne Bay, and identified additional adaptations necessary to achieve flood risk
301 reduction and resiliency within the C-8 Basin. The study, completed in collaboration with water managers

302 of the secondary and tertiary flood control system, identified and recommended a sequencing for the
 303 projects implementation. M2B implementation strategy is being recommended for near-term
 304 implementation, and M2C for longer-term implementation, addressing flood risks results from more than 2
 305 feet of SLR. Table 9-4 illustrates which project components were recommended as part of each
 306 implementation strategy. The M2C features, once implemented, will achieve a level of service equal or
 307 greater than the existing conditions under the 25-year SLR0 event for the 25-year SLR3 scenario. In
 308 addition to these regional project features, there are local projects that will be developed in partnership with
 309 local partners – at secondary and tertiary systems.

310 **Table 9-4.** FPLOS Phase II project component recommendations for the C-8 Basin.

311

FPLOS Recommendation	M2A	M2B	M2C
➤ Forward pump station at S-28 Structure location	1550 cfs	2550 cfs	3550 cfs
➤ Tidal structure improvements and tieback levees/floodwalls	x	x	x
➤ Canal improvements (raised bank elevations)		x	x
➤ Canal improvements (Improved canal geometry)		x	x
➤ Canal improvements (Canal widening)			x
➤ 250 acre-feet of distributed storage		x	x

312

313 **Reducing Risk and to What Level**

314 The proposed project consists of local and regional flood mitigation strategies that reduce flood risk
 315 and enhance resiliency. These mitigation strategies will increase the effective resilience of the entire C-8
 316 Basin. A range of critical assets including fire stations, emergency shelters, and medical facilities support
 317 several Community Lifelines and a variety of cultural, historic, and environmental resources in the basin.
 318 Additionally, the County has a high Building Code Effectiveness Grading Schedule (BCEGS) score of 2,
 319 which shows a commitment to reducing risk through strong building code adoption and enforcement
 320 activities. Extensive land development and population increases within the basin have already exceeded the
 321 original design assumptions of the C-8 Canal and S-28 Structure. Significant changes in climate conditions
 322 and SLR have also impacted the project and are limiting flood protection operations. These risks and their
 323 potential impacts are multifaceted and involve flood hazards driven by storm surge, high tides, and extreme
 324 rainfall.

325 **Increase Resilience**

326 A significant aspect of this project includes using a portion of the Miami Shores Golf Course as a
 327 temporary flood water storage area during extreme rain and storm surge events. Vegetated berms and living
 328 shoreline features are also incorporated into the conceptual plan to enhance water quality and aquatic

329 habitat. The strategy to reduce runoff in this densely urbanized basin includes implementation of a series
330 of distributed storage solutions. This project features can serve as a pilot example regionally, as nearby
331 jurisdictions are looking to implement similar measures.

332 ***Ancillary Benefits***

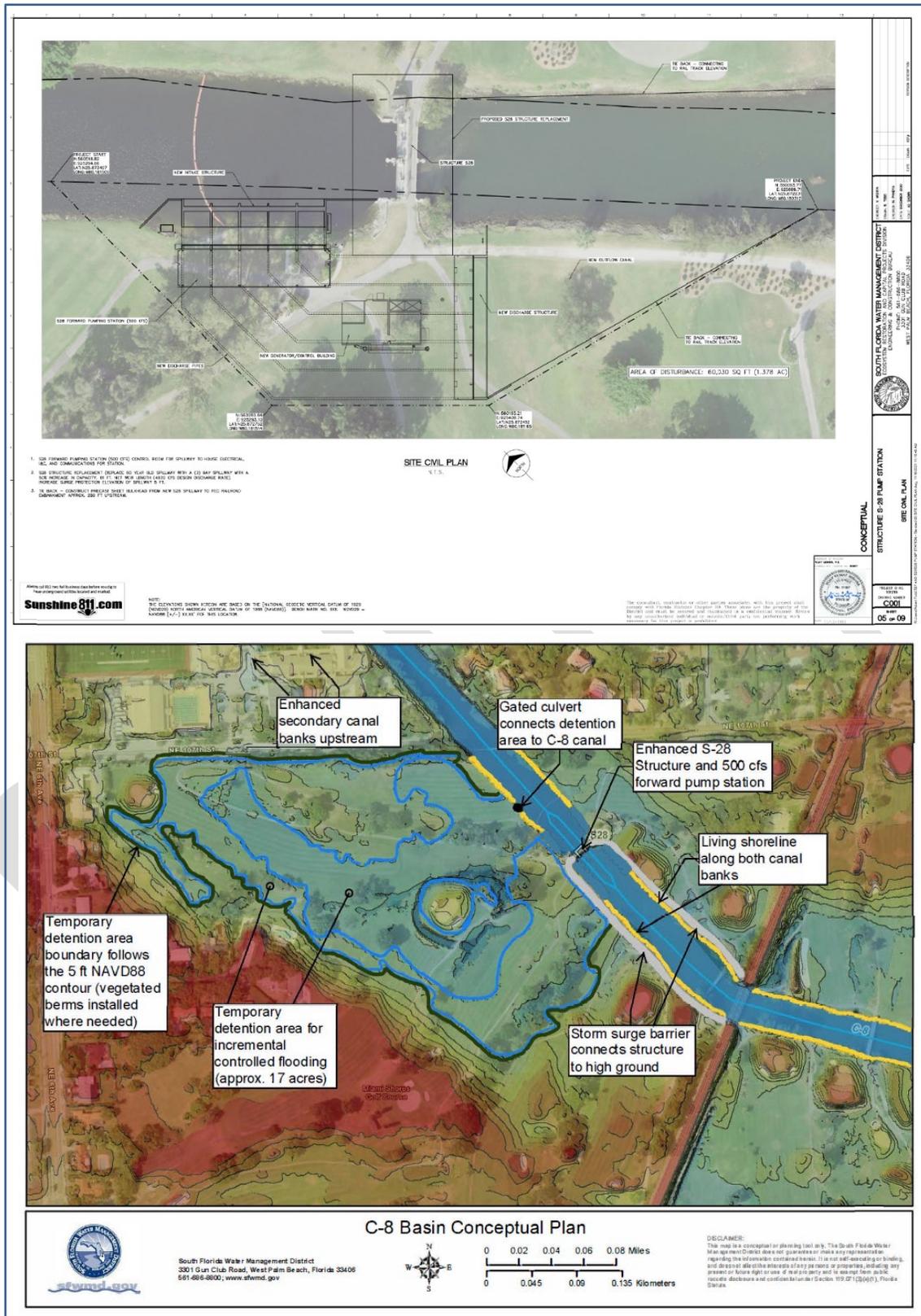
333 Ancillary benefits include improved fish and wildlife habitat from implementation of the living shoreline
334 features, improved land value due to reduced flood risk and enhanced aesthetics, prevention of canal bank
335 erosion, water quality benefits from implementation of vegetated berms and temporary flood water storage
336 on the golf course and increased opportunities for recreation. SFWMD aims to improve the C-8 Basin's
337 water quality and ecological functions, beyond enhancing the flood protection level of service, while
338 maximizing the risk reduction benefits and co-benefits of natural and NBS, such as short- and long-term
339 environmental, economic, and social advantages that improve a community's quality of life and make it
340 more attractive to new residents and businesses.

341 ***Leveraging Innovation***

342 This project will introduce green infrastructure features that have not been used previously in this area.
343 While Miami-Dade County is eager to pilot linear parks, living shorelines and expand Greenways and
344 Blueways, this project will be the first opportunity in this basin. The County conducted stakeholder
345 engagement to share the approaches and gather feedback. The community most enthusiastically supported
346 the green infrastructure approaches.

347 ***Outreach Activities***

348 A comprehensive public outreach process is embedded as part of the SFWMD Flood Protection Level
349 of Service Program to engage the public in the drainage basins that are at increased risk of flooding impacts
350 due to SLR and climate change. The initial round of workshops and meetings are designed to obtain local
351 project data and information about community needs, promoting coordination and collaboration with
352 partners agencies and local communities. The closing workshops and outreach efforts are designed to
353 provide stakeholders helpful planning tools and cost-effective courses of action for prioritizing and
354 designing projects in the secondary and tertiary systems and inform the community about the impacts of
355 flooding and the benefits of the adaptation and mitigation projects identified. This process is currently
356 underway at the C-8 Basin, the project site
357 <http://www.buildcommunityresilience.com/SFWMD/FPLOS/c&c9/> is used as a tool to collect information
358 and feedback from community partners and make outreach materials available.



359

360

Figure 9-4. Site plan for S-28 Structure features and conceptual plan for the C-8 Basin.

361

362 A significant aspect of this project includes using a portion of the Miami Shores Golf Course as a
 363 temporary flood water storage area during extreme rainfall and storm surge events (Figure 9-4 above).
 364 Vegetated berms and living shoreline features are also incorporated into the plan to enhance water quality
 365 and aquatic habitat. The strategy to reduce runoff in this densely urbanized basin includes implementation
 366 of a series of distributed storage solutions. These project features can serve as pilot project examples for
 367 the region. Ancillary benefits include improved fish and wildlife habitat from implementation of the living
 368 shoreline features, improved land value due to reduced flood risk and enhanced aesthetics, prevention of
 369 canal bank erosion, water quality benefits from implementation of vegetated berms and temporary flood
 370 water storage and increased opportunities for recreation.

371 A total cost estimate to harden the S-28 Coastal Structure, to address flooding, SLR and other related
 372 risks to vulnerable communities in the C-8 Basin is presented below and it includes modifications to the
 373 existing structure and control building, addition of a forward pump and construction of flood barriers. The
 374 additional pumping capacity will extend the conveyance performance for additional years as sea level rises,
 375 delay out of bank flooding, and reduce canal peak stages. Additional potential funds to purchase real estate
 376 for the project are included and negotiations with landowner will initiate upon funding confirmation.

377 C-8 Basin Cost Estimate

Structure Enhancement and Pump Station (M2B)	
S-28 Structure Replacement	\$ 19,057,000
Forward Pump (2550 cfs)	\$ 107,002,000
Forward Pump Backup Generator Facility	\$ 11,440,000
Structure Tie Back (Flood Barrier)	\$ 2,987,000
Design & Construction Management	\$ 21,073,000
Real Estate	\$ 7,000,000
Total Pump Station Cost	\$ 168,559,000
Storage (M2B)	
Distributed Storage (~250 Ac-Ft)	\$ 38,860,000
Design & Construction Management	\$ 5,829,000
Total Storage Cost	\$ 44,689,000
Canal Improvements (M2C)	
Raise Canal Banks (to 7.5 ft NGVD29)	\$ 12,412,000
Widen Canal (approx. 20,000 linear ft by 100 ft)	\$ 31,619,000
Design & Construction Management	\$ 6,605,000
Total Canal Improvements Cost	\$ 50,636,000
Stormwater Green Infrastructure / NBS (BRIC Application)	
Temporary Impoundment, Vegetative Berms and Living Shoreline	\$ 1,500,000
Total Cost Estimate for C-8 Basin	\$ 265,384,000

378

379 **S-29 COASTAL STRUCTURE AND C-9 BASIN RESILIENCY**

380 This resiliency project is
 381 mainly tied to the District’s
 382 mission to provide flood
 383 control, water supply
 384 protection, and ecosystem
 385 restoration. This project
 386 proposes flood risk reduction
 387 measures for the C-9 Basin, a
 388 region of about 549,964
 389 people (Census Tracts, 2022),
 390 encompassing 100 square
 391 miles, located in the southern
 392 portion of Broward County
 393 and northeastern portion of
 394 Miami-Dade County (Figure
 395 9-5). The basin area is fully
 396 developed with primarily
 397 residential and commercial
 398 uses. The C-9 Canal and the
 399 S-29 Coastal Structure are the

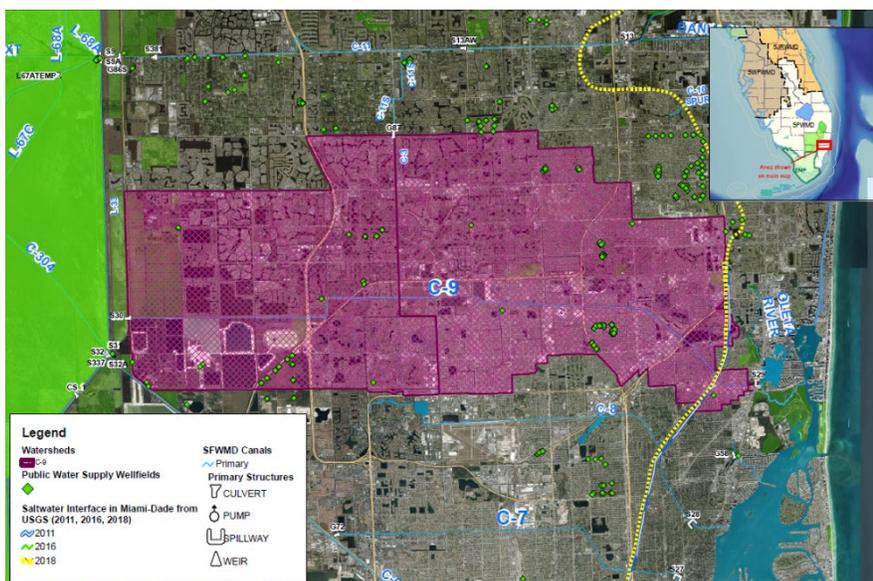


Figure 9-5. Map of C-9 Basin.

400 primary flood control features of this basin. The C-9 Canal receives and conveys flood waters by gravity
 401 through the S-29 Coastal Structure to the Oleta River (tide). The S-29 Coastal structure is a reinforced
 402 concrete, gated spillway, with discharge controlled by four cable operated, vertical lift gates with a
 403 discharge capacity of 4,780 cfs. The S-29 Structure is located near the mouth of the C-9 Canal, in an
 404 urbanized area of North Miami Beach east of Biscayne Boulevard and just north of Northeast 165th Terrace.
 405 The structure controls fresh waterflows out of the C-9 Canal into the Oleta River and drains the C-9 East and
 406 C-9 West watersheds. The C-9 Canal extends approximately 19.5 miles east from the L-33 Canal adjacent to
 407 Water Conservation Area 3B and the lake belt region, before traversing the densely populated area between
 408 Miramar to the north and Miami
 409 Gardens to the south. The canal
 410 drainage area is developed with a
 411 mixture of commercial structures
 412 along Biscayne Boulevard, high
 413 rise residences immediately to the
 414 east and a public park to the north.
 415 The S-29 Structure was originally
 416 designed by the U.S. Army Corps
 417 of Engineers (USACE) as part of
 418 the Central and Southern Florida
 419 (C&SF) Project with the objective
 420 of providing flood control and
 421 preventing saltwater intrusion.
 422 The C&SF Project was authorized
 423 in 1948 and was constructed by
 424 the USACE between 1950 and
 425 1970. S-29 is a gravity structure,
 426 and the designed discharge
 427 capacity is achieved when the
 428 gradient between head and tail water are sufficient to pass the flow. Operation of the gates is automatically

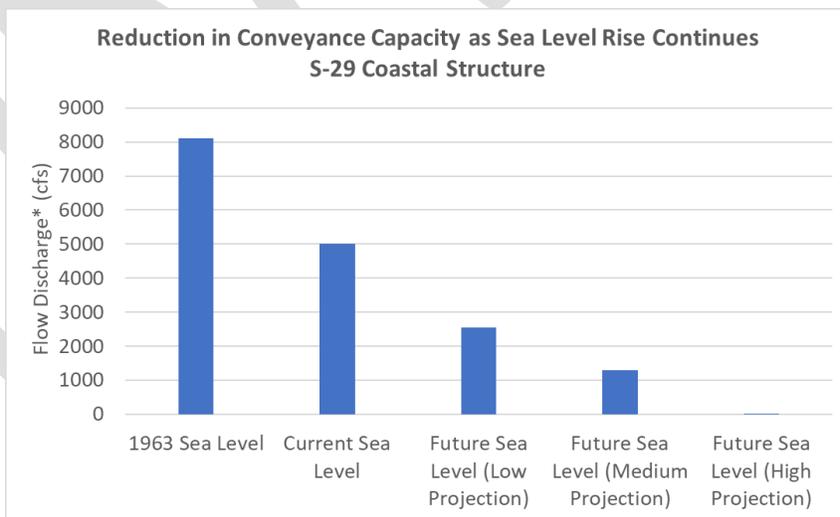


Figure 9-6. Reduction in conveyance capacity at S-29 as SLR continues.

429 controlled so that the gates open or close in accordance with the seasonal operational criteria. The structure's
430 original design did not account for SLR of the magnitudes that are being experienced today along the coastline
431 of south Florida. Figure 9-6 illustrates the impacts of SLR on conveyance capacity at the S-29 Structure over
432 time.

433 **Percent of Population Impacted**

434 One hundred percent of the population currently living in the C-9 basin, estimated at 549,964 people
435 (2022 Census), will either directly or indirectly benefit from this project. Overall flood protection levels of
436 service and water supply protection from saltwater intrusion are expected to improve. Flood modeling
437 results from the C-9 Basin Flood Protection Level of Service Study, as detailed here, demonstrate basin-
438 wide benefits.

439 **Community-Wide Benefits**

440 SFWMD, Broward and Miami Dade County have been shifting to incorporate a wider range of co-
441 benefits (social, environmental, operational) into their projects to consider equity community-wide. In the
442 context of the proposed project, "community-wide" refers to the historic, cultural, and recreational values
443 that South Florida residents share. This project is aligned with Miami Dade County's goals of promoting
444 resilience in a way that goes beyond environmental sustainability
445 (<https://www.miamidade.gov/global/management/strategic-plan/home.page>).

446 Miami Dade County encourages jurisdictions to take a holistic approach for resilience efforts across
447 four broad dimensions: Leadership and Strategy, Economy and Society, Health and Wellbeing, and
448 Infrastructure and Environment. Their vision is "Delivering excellent service today and tomorrow". The
449 SFWMD, as the agency responsible for the primary water control system, works closely with the County
450 and local jurisdictions to instill these values, particularly with respect to preparing for disasters and extreme
451 events.

452 **Impacts to Lifelines**

453 This project will reduce direct and cascading flood impacts to Community Lifelines, residents,
454 businesses, public services, infrastructure, and natural systems through three key lifelines: Food, Water,
455 Shelter, Transportation, and Energy. Food, Water, Shelter. The proposed project significantly reduces the
456 threat to property. Under the lifeline subcategory of shelter, the project increases the level of protection for
457 over 177,621 primary homes across the area. Without the project, it would take months for residents whose
458 homes may be significantly damaged, to stabilize their living situation. Given the level of damage expected,
459 residents would be displaced while repairs to homes occurred. Many of the basin's single-family homes are
460 on septic tank systems. The septic tank systems east of I95 are particularly vulnerable to SLR. In recent
461 years, several properties in this basin have had to retrofit their septic system due to system failure.
462 Alleviation of flooding would minimize future failures.

463 **Transportation**

464 The S-29 Structure is bordered by Highway U.S.1 to the west and SR826 to the south. These roads are
465 key evacuation routes and connectors for the region. The project would alleviate flooding and allow these
466 main arteries to function and be more easily accessible during extreme events.

467 **Safety and Security**

468 In addition, 162 critical assets would be protected under the proposed project. These include Airports
469 (5), Fire Stations (19), Hazardous Waste Transport Facilities (2), Heliports (3), Hospitals/Medical Facilities
470 (17), Law Enforcement Centers (6), and Public Schools (110). Overall flood protection levels of service

471 will improve and water supply protection from saltwater intrusion will increase. The proposed project
472 removes a portion of utility infrastructure from the floodplain.

473 **Impacts to Disadvantaged Communities**

474 To ensure forty percent (40%) of the overall project benefits flow to disadvantaged communities that
475 are marginalized, underserved, and overburdened by environmental stressors we used data available
476 through the Climate and Economic Justice Screening Tool (CEJST) and the Centers for Disease Control
477 and Prevention (CDC) Agency for Toxic Substances and Disease Registry (ATSDR) Social Vulnerability
478 Index (SVI). Based on these data, fifty-seven percent (57%) of the population within the project impact
479 area were identified as socioeconomically disadvantaged and will receive equal access to community wide
480 benefits from the implementation of this resiliency project. These benefits are mainly related to the flood
481 risk reduction measures, environmental benefits, and the opportunities created for education, recreation,
482 and development.

483 The CEJST identifies twenty-five percent (25%) of the population within the project impact area as
484 disadvantaged under the Climate Change category. The climate change category quantifies and considers
485 the percent low-income population and higher education non-enrollment as well as expected population,
486 building, and agricultural loss rates above pre-determined thresholds.

487 The CDC identifies twenty-seven percent (27%) of the population within the project impact areas as
488 having an SVI greater than 0.8 or higher, the highest vulnerability ranking, and thirty percent (30%) of the
489 population within the project impact area as having an SVI between 0.6 and 0.8, the second highest
490 vulnerability ranking. The CDC/ATSDR SVI ranks each census tract on 16 social factors, including
491 poverty, lack of vehicle access, and crowded housing, and groups them into four related themes.

492 **Project Scope**

493 The proposed project consists of flood mitigation and enhancement strategies at the C-9 Basin to build
494 flood resiliency and increase protection against saltwater intrusion. Specifically, the project includes:

495 FPLOS Phase II Recommendations:

- 496 • S-29 Coastal Structure Enhancement: converting the gate opening system to a more robust
497 mechanism, upgrading the existing gates to elevated, corrosion resistant stainless-steel gates and
498 enhancing, elevating, and hardening the control building, and adding a corrosion control system
499 to the structure.
- 500 • Forward Pump: building a new 2550cfs forward pump station that will convey flood waters to
501 tide when downstream water elevations are too high to allow gravity flow. The design of the
502 proposed forward pump station will be adaptable and will include the ability to add additional
503 pumps in the future as conditions continue to change.
- 504 • Tie Back Levee: constructing a tie back levee/salinity barrier to provide flood and storm surge
505 protection and supporting the required function of the spillway gates and pump during a 100-year
506 event with three-foot SLR.
- 507 • Canal Improvements: raising canal bank elevations, improving geometry, and widening. A
508 portion of approximately 7 miles of the C-9 Canal is being widened to include NBS enhancement
509 along canal banks (more details provided in the subsection below)
- 510 • Storage: Adding approximately 250-acre feet of distributed storage in the C-9 Basin.

511 Additional stormwater green infrastructure project components:

- 512 • Enhancing an approximately 16-acre flow-through wetland/stormwater detention area at
513 Pickwick Lake (Figure 9-7), which is owned by the City of North Miami Beach, to reduce local

- 514 runoff in the area. The stormwater detention area will incorporate Biosorption Activated Media
 515 (BAM), an innovative stormwater best management practice in South Florida that has been
 516 deployed across agencies and in varied use cases and has consistently reduced harmful nutrients
 517 such as nitrogen and phosphorus and other contaminants in stormwater.
- 518 • Installing 1,850 linear feet of living shoreline to assist in reducing bank erosion and improve
 519 aesthetics and storm resiliency. In addition, a shaded gathering area, educational signage, and
 520 other amenities to help increase community engagement and public use will be incorporated to
 521 the project.

522 **Adaptation and Mitigation Study for the C-9 Basin**

523 The proposed C-9 Basin Resiliency Project was advanced following completion of flood vulnerability
 524 assessments and findings of a need for major refurbishment of S-29 Structure, through the Structure
 525 Inspection Program. The project, a no-regret strategy at the time of its inception, is currently in design. The
 526 recently completed comprehensive study of the C-9 basin, (FPLOS Phase II Studies in the C-8 and C-9
 527 Basins, 2023), confirmed the C-9 Basin project elements, evaluated the potential downstream impacts and
 528 water quality impacts to Biscayne Bay, and identified additional adaptations necessary to achieve flood risk
 529 reduction and resiliency within the C-9 Basin. The study, completed in collaboration with water managers
 530 of the secondary and tertiary flood control system, identified and recommended a sequencing for the
 531 projects implementation. M2B implementation strategy is being recommended for near-term
 532 implementation, and M2C for longer-term implementation, addressing flood risks results from more than 2
 533 feet of SLR. Table 9-5 illustrates which project components were recommended as part of each
 534 implementation strategy. The study recommended that features of the M2C scenario such as the canal
 535 widening be opportunistically implemented to deliver immediate water quality and other social benefits
 536 along with flood risk reduction. The M2C features, once implemented, will achieve a level of service equal
 537 or greater than the existing conditions under the 25-year SLR0 event for the 25-year SLR3 scenario. In
 538 addition to these regional project features, there are local projects that will be developed in partnership with
 539 local partners – at secondary and tertiary systems.

540 **Table 9-5.** FPLOS Phase II project component recommendations for the C-9 Basin.

FPLOS Recommendation	M2A	M2B	M2C
➤ Forward pump station at S-29 Structure location	1550 cfs	2550 cfs	3550 cfs
➤ Tidal structure improvements and tieback levees/floodwalls	x	x	x
➤ Canal improvements (raised bank elevations)		x	x
➤ Canal improvements (Improved canal geometry)		x	x
➤ Canal improvements (Canal widening)			x
➤ 250 acre-feet of distributed storage		x	x



541

542 **Figure 9-7:** Pickwick Lake wetland restoration/stormwater detention area features.543 **Reducing Risk and to What Level**

544 Extensive land development and population increases within the basin have already exceeded the
 545 original design assumptions of the C-9 Canal and S-29 Structure. Significant changes in climate conditions
 546 and SLR have also impacted the area and are limiting flood protection operations. These risks and their
 547 potential impacts are multifaceted and involve flood hazards driven by storm surge, high tides, and extreme
 548 rainfall. This project will reduce flooding risk by reducing peak canal stages, bank exceedances and
 549 overland flood inundation throughout the C-9 Basin for the 5-year, 10-yr, 25-yr and 100-yr extreme storm
 550 events and under 1ft, 2ft and 3ft SLR scenarios, as demonstrated by hydrology and hydraulics model
 551 simulations. The project consists of local and regional flood mitigation strategies that reduce flood risk and
 552 enhance resiliency. These mitigation strategies will increase the resilience of the entire C-9 Basin. A range
 553 of critical assets including fire stations, emergency shelters, and medical facilities support several
 554 Community Lifelines and a variety of cultural, historic, and environmental resources in the basin.
 555 Additionally, the County has a high Building Code Effectiveness Grading Schedule (BCEGS) score of 2,
 556 which shows a commitment to reducing risk through strong building code adoption and enforcement
 557 activities.

581 benefits from implementation of the flow-through wetland/stormwater detention area and increased
582 opportunities for recreation.

583 **Leveraging Innovation**

584 This project will introduce green infrastructure features that have not been used previously in this area.
585 While Miami-Dade County is eager to pilot linear parks, living shorelines and expand Greenways and
586 Blueways, this project will be the first opportunity in this basin. The County conducted stakeholder
587 engagement to share the approaches and gather feedback. The community most enthusiastically supported
588 the green infrastructure approaches.

589 **Outreach Activities**

590 A comprehensive public outreach process is embedded in the SFWMD Sea Level Rise and Flood
591 Resiliency Plan – Annual Update process ensuring equal opportunity for all members of our region’s
592 communities to participate in the planning and decision-making process, as well as the Flood Protection
593 Level of Service Program (FPLOS) and the Miami Dade Sea Level Rise Strategy. The public and key
594 stakeholders contributed to informing the identification of priority adaptation strategies through several
595 workshops and public comments. The proposed project features will even further increase the ability to
596 leverage partners, enhance outreach activities and emphasize community engagement.

597 **C-9 Basin Cost Estimate**

Structure Enhancement and Pump Station (M2B)	
S-29 Structure Enhancement	\$19,057,000
Forward Pump (2550 cfs)	\$111,669,000
Forward Pump Backup Generator Facility	\$11,919,000
Structure Tie Back (Flood Barrier)	\$2,769,000
Design & Construction Management	\$21,812,000
Real Estate	\$16,000,000
Total Pump Station Cost	\$183,226,000
Storage (M2B)	
Distributed Storage (~250 Ac-Ft)	\$38,860,000
Design & Construction Management	\$5,829,000
Total Storage Cost	\$44,689,000
Canal Improvements (M2C)	
Raise Canal Banks (to 7.5 ft NGVD29)	\$7,119,000
Widen Canal (approx. 40,000 linear ft by ~40-50 ft, with NBS enhancements along canal bank)	\$53,860,000
Widen Canal (approx. 40,000 linear feet by 75 ft)	\$53,860,000
Design & Construction Management	\$17,227,000
Total Canal Improvements Cost	\$132,066,000
Stormwater Green Infrastructure / NBS (BRIC Proposal)	
Pickwick Lake and Living Shoreline	\$1,500,000
Total Cost Estimate for C-9 Basin	\$361,481,000

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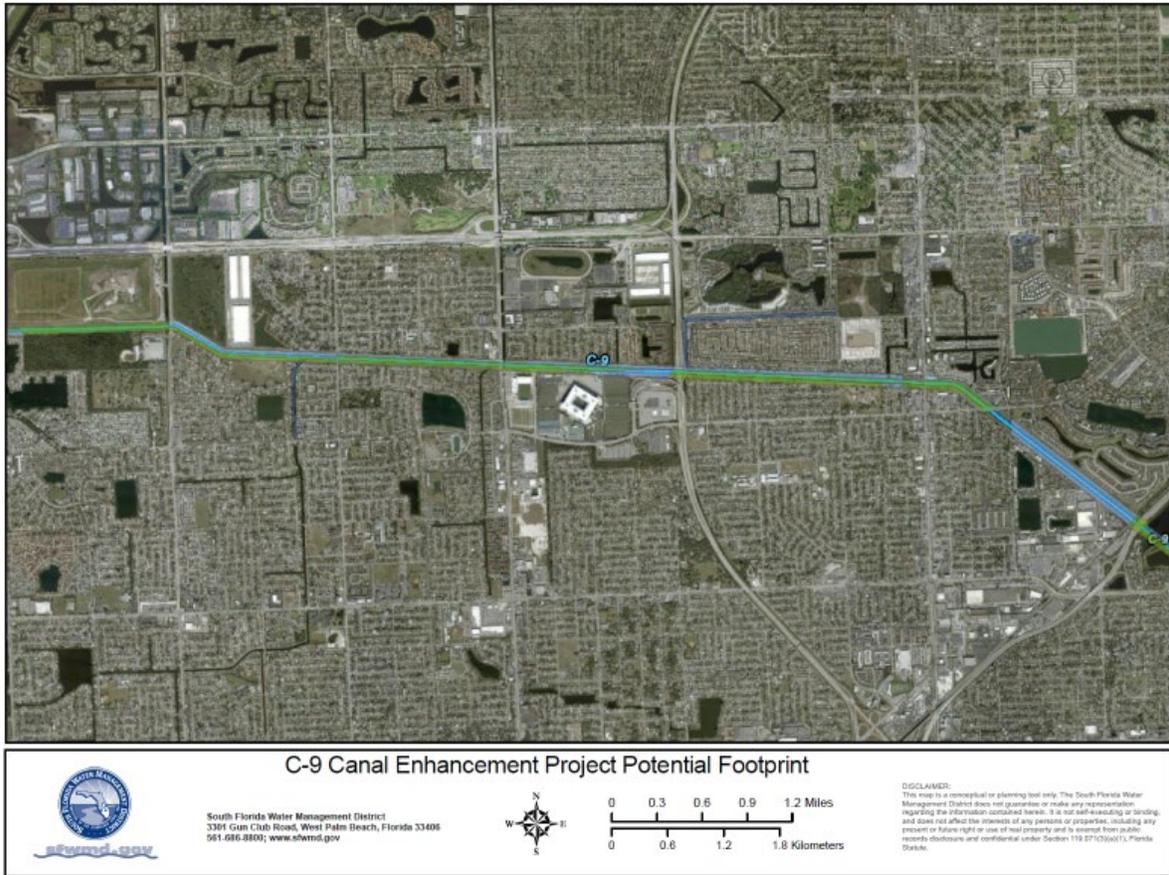
600 **C-9 Canal Widening and Enhancement with Nature-Based Features**

601 The FPLOS study results for the C-9 Basin recommended widening a portion of the C-9 Canal to
602 enhance conveyance and storage capacity. This project was identified as a future need within the basin.
603 Due to the opportunity to provide co-benefits (social environmental and water quality) along with flood
604 risk reduction the project was recommended for opportunistic implementation where conditions such as
605 right of way and land ownership allow. Adding a forward pump station at the S-29 Structure increased the
606 level of service. However, constrictions in the western portion of the canal limit the effectiveness of the
607 forward pump station. Full level of service improvements were found to be achievable by installing a
608 forward pump station at the S-29 Structure and widening a portion of the canal (40-75) feet wider depending
609 on the section. This component of the C-9 resiliency project includes the following features:

- 610 • Widening approximately seven miles of the C-9 Canal to increase storage and conveyance
611 capacity.
- 612 • Constructing a mosaic of ecotones (wetland, terrestrial and aquatic depending on topography)
613 adjacent to the C-9 Canal. A combination of features such as constructed wetland, living
614 shoreline, bioswales, vegetated buffers will be used to increase flood resilience, create
615 additional stormwater storage, restore floodplain connectivity, reduce erosion of the canal
616 banks, enhance water quality, and increase fish and wildlife habitat. Increased
617 evapotranspiration in the constructed wetland can contribute to reductions in peak flood stages
618 and durations.
- 619 • Constructing access roads along the banks of the C-9 Canal to improve operations and
620 maintenance of the canal as well as increase the potential for public access for recreational
621 purposes.
- 622 • Connecting the wetland to the C-9 Canal using gated culverts, low water crossings etc. This
623 will increase floodplain connectivity, increase the ability to store water, improve water quality,
624 including dissolved oxygen levels and improve fish and wildlife habitat.
- 625 • Constructing structural or nature-based measures at the outfalls of 8-10 secondary canals to
626 treat runoff before it enters the C-9 Canal and improve basin resiliency.
- 627 • Constructing temporary pump pads at secondary canal outfalls. The pads would make it easier
628 to deploy temporary pumps during and after extreme events.

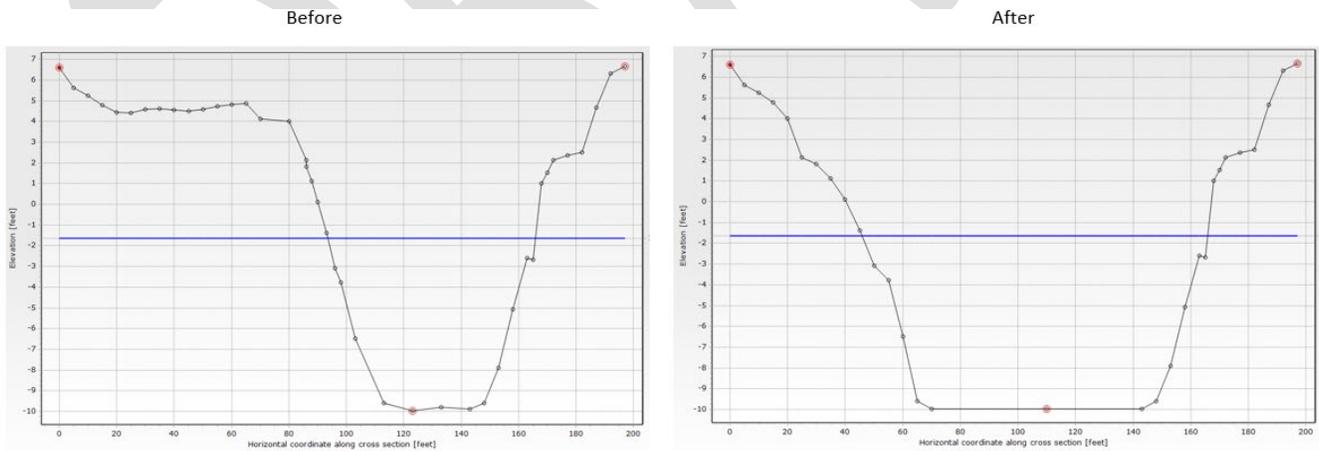
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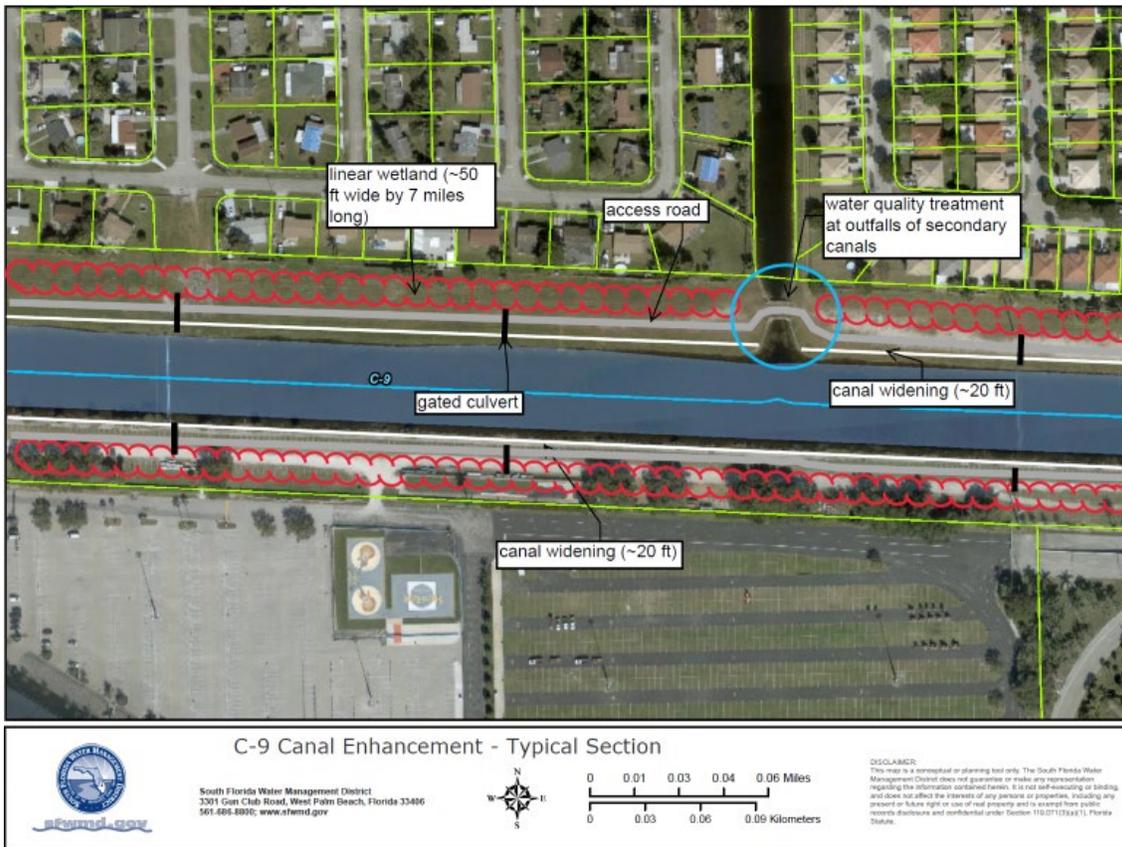
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Figure 9-9. Potential project footprint for C-9 Enhancement project.

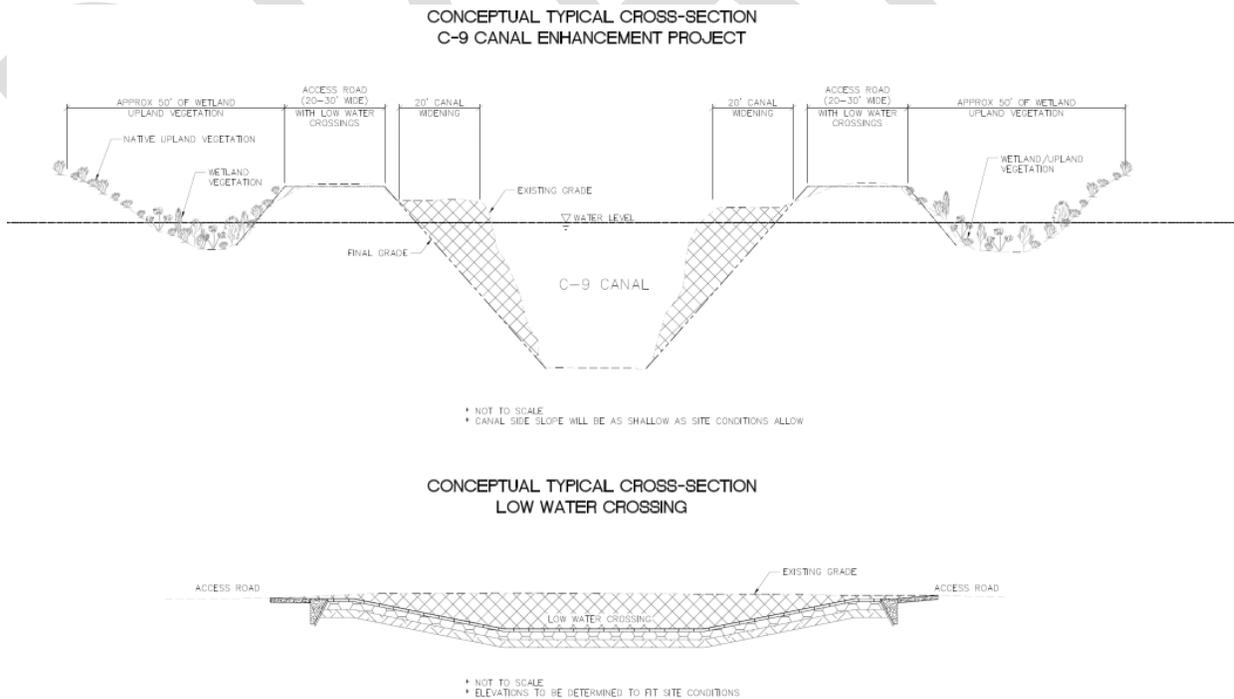


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Figure 9-10. Typical canal cross section before and after widening.



638
639 **Figure 9-11.** Typical section of the C-9 Canal Enhancement project showing potential project
640 features.



641
642 **Figure 9-12.** Typical cross-section of the C-9 Canal Enhancement project showing potential project
643 features.

644 S-27 COASTAL STRUCTURE AND C-7 BASIN RESILIENCY

645

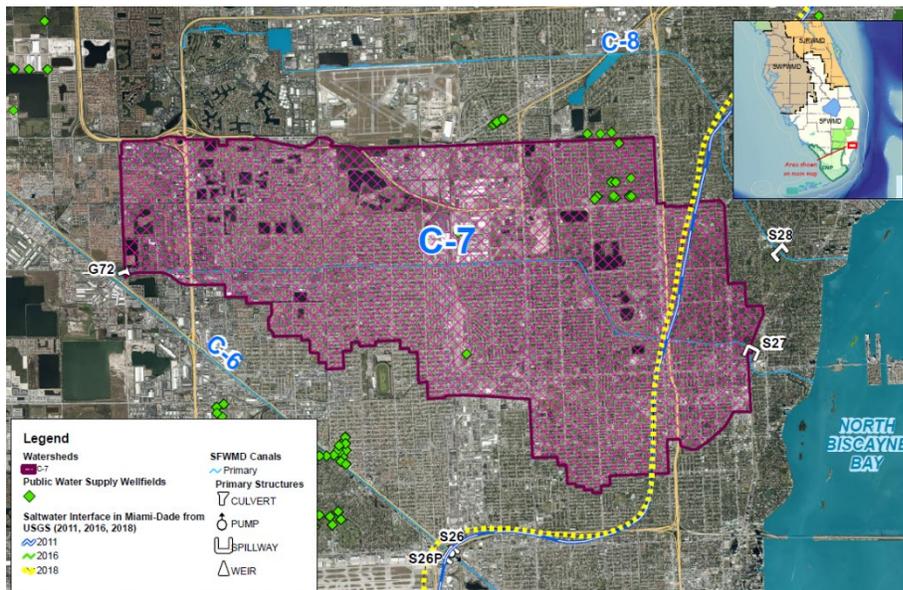


Figure 9-13. Map of C-7 Basin.

This resiliency project is mainly tied to the District’s mission to provide flood control, water supply protection, and ecosystem restoration. S-27 is a reinforced concrete, gated spillway, with discharge controlled by two vertical lift gates with a discharge capacity of 2,800 cfs. S-27 is a gravity structure, and the designed discharge capacity is achieved when the gradient between head and tail water are sufficient to pass the flow.

665 Operation of the gates is automatically controlled. The structure is in the City of Miami near the mouth of
 666 C-7 Canal about 700 feet from the shore of Biscayne Bay. The C-7 Basin has a population of about 270,000
 667 people within 32 square miles, in the northeastern portion of Miami-Dade County (Figure 9-13). The area
 668 drained by the C-7 Canal is fully developed with primarily residential and commercial uses. The C-7 Canal
 669 is the central flood control feature that receives and conveys basin flood waters by gravity through the
 670 S-27 Coastal Structure to sea. This structure was designed to 1) maintain optimum water control stages
 671 upstream in C-7 (Little River Canal), 2) release the design flood (75 percent of the Standard Project Flood)
 672 without exceeding upstream flood design stage 3) restricts downstream flood stages and discharge velocities
 673 to non-damaging levels, and 4) prevent saltwater intrusion during periods of high tides.

674 Percent of Population Impacted

675 One hundred percent of the population currently living in the C-7 basin, estimated at 254,000 people
 676 (2020 Census), will either directly or indirectly benefit from this project. Overall flood protection levels of
 677 service and water supply protection from saltwater intrusion are expected to improve. Flood modeling
 678 results from the C-7 Basin Flood Protection Level of Service Study, as detailed in this proposal, demonstrate
 679 basin wide benefits.

680 Community-Wide Benefits

681 SFWMD and Miami Dade County have been shifting to incorporate a wider range of co-benefits
 682 (social, environmental, operational) into their projects to consider equity community-wide. In the context
 683 of the proposed project, “community-wide” refers to the historic, cultural, and recreational values that South
 684 Florida residents share. This project is aligned with the SFWMD Sea Level Rise and Flood Resiliency Plan
 685 (https://www.sfwmd.gov/sites/default/files/2022_SFWMD_SLRFRP_Final.pdf) and Miami Dade
 686 County’s goals of promoting resilience in a way that goes beyond environmental sustainability
 687 (<https://www.miamidade.gov/global/management/strategic-plan/home.page>) The County encourages
 688 jurisdictions to take a holistic approach for resilience efforts across four broad dimensions: Leadership and
 689 Strategy, Economy and Society, Health and Wellbeing, and Infrastructure and Environment. Their vision
 690 is “Delivering excellent service today and tomorrow”. The SFWMD, as the agency responsible for the

691 primary control system, works closely with the County and local jurisdictions to instill these values,
692 particularly in respect to preparing for disasters and extreme events.

693 **Impacts to Lifelines**

694 This project will reduce direct and indirect flood impacts to Community Lifelines, residents, businesses,
695 public services, infrastructure, and natural systems through three key lifelines: Food, Water, Shelter,
696 Transportation, and Energy. Food, Water, Shelter - The proposed project significantly reduces the threat to
697 property. Under the lifeline subcategory of shelter, the project increases the level of protection for over
698 80,527 primary homes across the area. Without the project, it would take months for residents whose homes
699 may be significantly damaged, to stabilize their living situation. Given the level of damage expected,
700 residents would be displaced while repairs to homes occurred. Many of the basin's single-family homes are
701 on septic tank systems. The septic tank systems east of I95 are particularly vulnerable to SLR. In recent
702 years, several properties in this basin have had to retrofit their septic system due to system failure.
703 Alleviation of flooding would minimize future failures.

704 **Transportation**

705 The S-27 Structure is bordered by U.S. 1 to the east and SR934 to the south. These roads are key
706 evacuation routes and connectors for the region. The project would alleviate flooding and allow these main
707 arteries to function and be more easily accessible during extreme events.

708 **Safety and Security**

709 In addition, 118 critical assets would be protected under the proposed project. These include Airports
710 (2), Fire Stations (9), Hazardous Waste Transport Facilities (7), Heliports (1), Hospitals/Medical Facilities
711 (12), Law Enforcement Centers (11), and Public Schools (76). The proposed project removes a portion of
712 utility infrastructure from the floodplain.

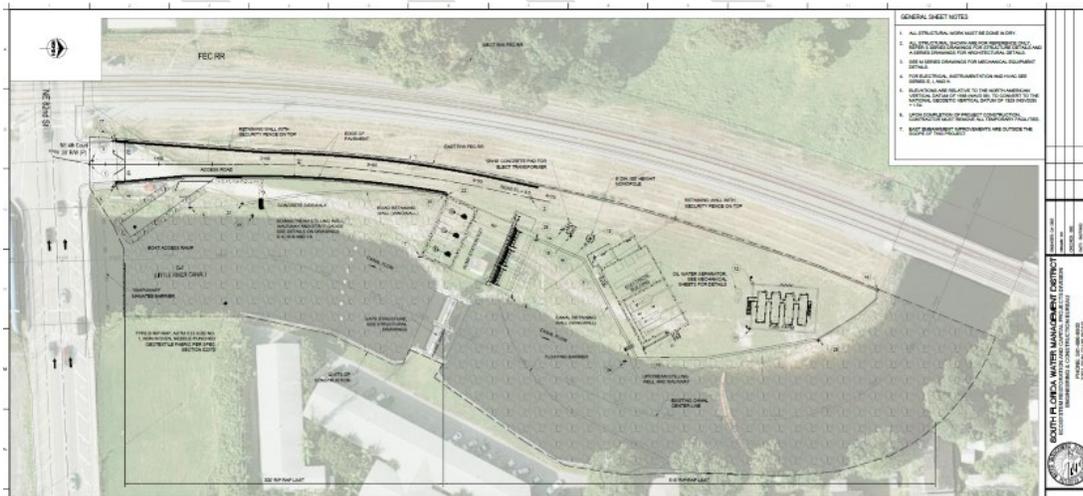
713 **Impacts to Disadvantaged Communities**

714 To ensure forty percent (40%) of the overall project benefits flow to disadvantaged communities that
715 are marginalized, underserved, and overburdened by environmental stressors we used data available
716 through the Climate and Economic Justice Screening Tool (CEJST) and the Centers for Disease Control
717 and Prevention (CDC) Agency for Toxic Substances and Disease Registry (ATSDR) Social Vulnerability
718 Index (SVI). Based on these data, ninety-four percent (94%) of the population within the project impact
719 area were identified as socioeconomically disadvantaged and will receive equal access to community wide
720 benefits from the implementation of this resiliency project. These benefits are mainly related to the flood
721 risk reduction measures, environmental benefits, and the opportunities created for education, recreation,
722 and development. The CEJST identifies forty-six percent (46%) of the population within the project impact
723 area as disadvantaged under the Climate Change category. The climate change category quantifies and
724 considers the percent low-income population and higher education non-enrollment as well as expected
725 population, building, and agricultural loss rates above pre-determined thresholds. The CDC identifies sixty-
726 seven percent (67%) of the population within the project impact areas as having an SVI greater than 0.8 or
727 higher, the highest vulnerability ranking, and twenty-seven percent (27%) of the population within the
728 project impact area as having an SVI between 0.6 and 0.8, the second highest vulnerability ranking. The
729 CDC/ATSDR SVI ranks each census tract on 16 social factors, including poverty, lack of vehicle access,
730 and crowded housing, and groups them into four related themes.

731 **Project Scope**

732 The proposed project consists of flood mitigation and enhancement strategies at C-7 Basin, known as
 733 Litter River, in Miami Dade County, to build flood resiliency and increase protection against saltwater
 734 intrusion. Specifically, the project includes:

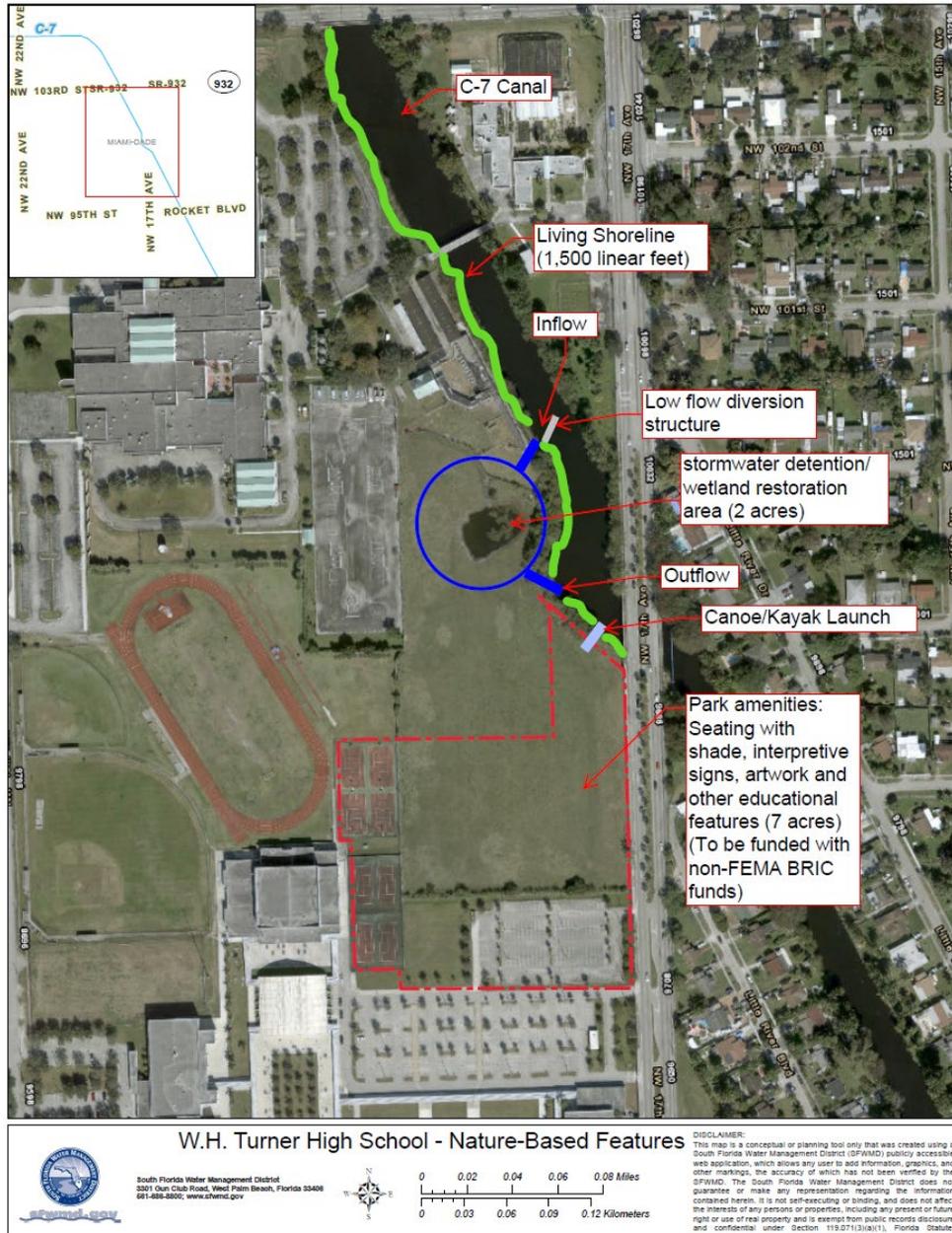
- 735 • Enhancing major components of the S-27 Structure and converting the gate opening system to a
 736 more robust mechanism, upgrading the existing gates with elevated, corrosion resistant stainless-
 737 steel gates, enhancing and elevating the control building, and adding a corrosion control system to
 738 the structure.
- 739 • Building a new forward pump station that will convey flood waters to tide when downstream water
 740 elevations are too high to allow gravity flow. The design of the proposed forward pump station will
 741 be adaptable and will include the ability to easily add additional pump capacity in the future as
 742 conditions continue to change.
- 743 • Constructing a tie back levee/salinity barrier to provide flood and storm surge protection and
 744 supporting the required function of the spillway gates and pump for the selected scenario of 100-
 745 year event with three-foot SLR.
- 746 • Building an approximately 2-acre flow-through wetland/stormwater detention area to reduce local
 747 runoff on the W.H. Turner High School property (owned by Miami-Dade County Public Schools).
 748 This project feature will increase the ability to leverage partners and enhance outreach activities
 749 and emphasize community engagement. This stormwater detention area will be incorporating
 750 Biosorption Activated Media (BAM), an innovative stormwater best management practice in South
 751 Florida that has been deployed across agencies and in varied use cases and has consistently reduced
 752 harmful nutrients such as Nitrogen and Phosphorus and other contaminants in stormwater. BAM is
 753 a patented unique combination of recycled tire crumb, silt, clay, and sand that is optimized for inert
 754 filtration, reactive filtration, and to provide an ideal habitat for microbes to facilitate biosorption &
 755 biological uptake.
- 756 • Installing 1,500 linear feet of living shoreline along the C-7 Canal Bank to assist in reducing bank
 757 erosion and improve aesthetics and storm resiliency. The flow-through wetland/stormwater
 758 detention area and living shoreline features will be incorporated into the W.H. Turner High School
 759 curriculum for environmental science students. In addition, a shaded gathering area, a community
 760 garden, educational signage, and outdoor classroom amenities for public use and to increase
 761 community engagement will be incorporated to the project.



762 **Figure 9-14: Site plan at S-27 Structure.**
 763

764 **Reducing Risk and to what level**

765 Extensive land development and population increases within the basin have already exceeded the
 766 original design assumptions of the C-7 Canal and S-27 Structure. Significant changes in climate conditions
 767 and SLR have also impacted the area and are limiting flood protection operations. These risks and their
 768 potential impacts are multifaceted and involve flood hazards driven by storm surge, high tides, and extreme
 769 rainfall. This project will reduce flooding risk by reducing peak canal stages, bank exceedances and
 770 overland flood inundation throughout the C-7 Basin for the 5-year, 10-yr, 25-yr and 100-yr storm events
 771 and under different SLR scenarios, as demonstrated by hydrology and hydraulics model simulations. The

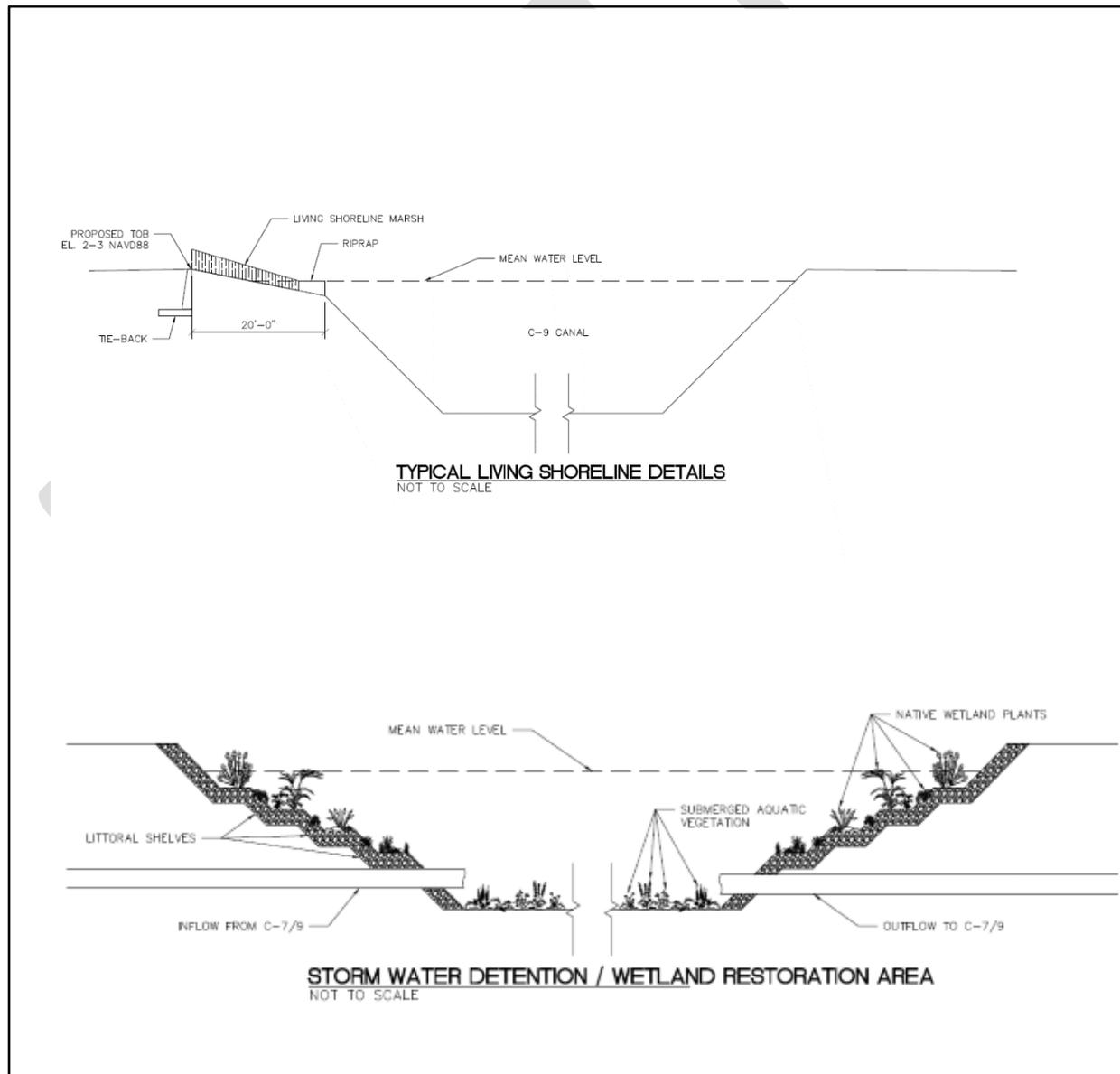


project consists of local and regional flood mitigation strategies that reduce flood risk and enhance resiliency. These mitigation strategies will increase the resilience of the entire C-7 Basin. A range of critical assets including fire stations, emergency shelters, and medical facilities support several Community Lifelines and a variety of cultural, historic, and environmental resources in the basin. Additionally, the County has a high Building Code Effectiveness Grading Schedule (BCEGS) score of 2, which shows a commitment to reducing risk through strong building code adoption and enforcement activities.

810 **Figure 9-15:** Nature-based features at W.H. Turner High School.

811 **Increase Resilience**

812 The project components to increase resilience include enhancements to S-27 Structure, and the addition
 813 of a forward pump and a tie back levee. The pump will maintain basin discharge capacity while sea levels
 814 rise. The new levee and increased elevation of the flood control gates, and service bridge will help prevent
 815 overtopping and reduce saltwater intrusion risk. A significant aspect of this project includes construction
 816 of demonstration project level nature-based features at W.H. Turner Technical High School in partnership
 817 with Miami-Dade County Public Schools. The proposed components include building a flow-through
 818 wetland/stormwater detention area, and installing living shoreline to reduce bank erosion, and indirectly
 819 enhance water quality and aquatic habitat. The overall strategy to reduce runoff in this densely urbanized
 820 basin includes implementation of a series of distributed storage solutions. This project can serve as an
 821 example regionally, as nearby jurisdictions are looking to implement similar measures. The project will
 822 also be incorporated into the school curriculum for environmental science students, adding an important
 823 educational component.



826

827 **Figure 9-16:** Typical living shoreline detail and stormwater detention area/wetland restoration
828 area.

829 **Ancillary Benefits**

830 Beyond enhancing the flood protection level of service, the project aims to maximize the risk reduction
831 benefits and co-benefits of NBS and improve the C-7 Basin's water quality and ecological functions.
832 Benefits include short and long-term environmental, economic, and social advantages that improve a
833 community's quality of life, emphasize community engagement, and increase recreational value in the
834 project area (kayaking, canoeing, wildlife observation and fishing). Ancillary benefits also include
835 improved fish and wildlife habitat from implementation of the living shoreline features, improved land
836 value due to reduced flood risk and enhanced aesthetics, prevention of canal bank erosion, water quality
837 benefits from implementation of the flow-through wetland/stormwater detention area and increased
838 opportunities for education and recreation (outdoor classroom activities).

839

840 **Leveraging Innovation**

841 This project will introduce green infrastructure features that have not been used previously in this area.
842 While Miami-Dade County is eager to pilot linear parks, living shorelines and expand Greenways and
843 Blueways, this project will be one of the first opportunities in this basin. The County conducted stakeholder
844 engagement to share the approaches and gather feedback. The community most enthusiastically supported
845 the green infrastructure approaches.

846 **Outreach Activities**

847 A comprehensive public outreach process to engage the public and key stakeholders is embedded as
848 part of the SFWMD Sea Level Rise and Flood Resiliency Plan Annual Update process, ensuring equal
849 opportunity for all members of our region's communities to participate in the planning and decision-making
850 process, as well as the Flood Protection Level of Service Program (FPLOS) and the Miami Dade Sea Level
851 Rise Strategy. The public and key stakeholders contributed to informing the identification of priority
852 adaptation strategies through several workshops and public comments.

853 **S-27 Cost Estimate**

Structure Hardening	\$5,642,523
Construction of 1400 cfs Forward Pump at S-27 Structure	\$67,200,000
Forward Pump Backup Generator	\$6,720,000
Structure Tieback Levee	\$2,000,000
Design & Construction Management	\$12,234,378
Real Estate	\$10,000,000
Total Cost for S-27	\$103,796,902
Adjusted 2023 Cost	\$125,370,188
Design and Permitting of Green Infrastructure	\$200,000
Construction of Green Infrastructure	\$1,300,000
Total Cost with Green Infrastructure	\$126,870,189

854

855

S-26 COASTAL STRUCTURE RESILIENCY

856

857
858 This resiliency project
859 is mainly tied to the
860 District's mission to
861 provide flood control and
862 water supply protection. S-
863 26 is a two-bay, reinforced
864 concrete gated spillway
865 located in the City of
866 Miami at the NW 36th
867 Street crossing of the
868 Miami (C-6) Canal,
869 between NW North River
870 Drive and NW South River
871 Drive, northeast of the
872 Miami International
873 Airport. The structure
874 consists of two 14.1 feet
875 high by 26.0 feet wide gates
876 with a discharge capacity of
877 3,470 cfs. The discharge
878 from the structure is



879 controlled by two hydraulically driven cable operated vertical lift gate mechanisms. The gates can either be
880 remotely operated from the District Control Room or controlled on-site. To maintain flood protection for
881 the C-6 basin, a 600 cfs. pump station was added to the S-26 spillway as part of the Miami Dade County
882 Flood Mitigation Program. The S-26 is the outlet to tide for the C-6 basin. The structure maintains optimum
883 water control stages upstream in the C-6 Canal. It was designed to pass 100% of the Standard Project Flood
884 (SPF) without exceeding upstream flood design stage and restricts downstream flood stages and discharge
885 velocities to non-damaging levels, and it prevents saltwater intrusion during periods of extreme high tides.
886 The structure is maintained by the Miami Field Station.

887 The purpose of this project is to build resiliency, restore the design discharge of the S-26 Structure and
888 decrease flood impacts within the C-6 Basin due to SLR, climate change and land use changes in the basin.
889 Project conceptual design is finalized. Final design will be based upon simulation of the combined regional
890 and local hydraulic measures in the C-6 Basin. The S-26 structure will be enhanced by raising the bridge,
891 converting the gate opening system to a more robust mechanism, replacing the existing gates with taller
892 corrosion resistant stainless-steel gates and replacing the control building with an elevated control building,
893 and adding a corrosion control system to the structure. Flood barriers will be constructed around the coastal
894 structure to tie it back to higher land. The design of a forward pump station will be adaptable and will
895 include the ability to easily add additional pumps in the future as environmental conditions change. The
896 current design includes a pumping capacity of 1735 cfs. There is an urgent need to identify and purchase
897 lands in this area to accommodate future structure modifications and pump station sizing.

898 In 2023, the District is replacing existing pumps at this location as part of the normal operations and
899 maintenance program. The pump capacity will not be increased as part of this maintenance because the
900 existing control building and structure cannot support increasing the pump size. One important
901 consideration at this site is that the system needs to be fully operational during construction.

902

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904

905 **Figure 9-17:** Land needs for S-26 Structure enhancements.

906 The entire population currently living in the C-6 Basin, estimated at 223,766, will directly or indirectly
 907 benefit from this project. The total number of critical assets vulnerable to flooding under current and future
 908 conditions in the C-6 Basin are 226. These include airports, faith-based facilities, fire stations, waste
 909 management facilities, hospitals and medical facilities, law enforcement centers, and schools. The state’s
 910 public schools have a vital role in our communities during emergency storm evacuations and post-storm
 911 recovery efforts, serving as shelters for displaced residents and emergency response staging areas. Overall
 912 flood protection levels of service are expected to increase in the entire basin with project implementation,
 913 as well as water supply protection from saltwater intrusion.

914 The project will provide 20-40 years of protection against SLR, depending on the scenario
 915 (Intermediate Low or NOAA Intermediate High). Peak canal stage can be reduced by 15% with each 500
 916 cfs increase in forward pumping capacity. The pump station facility will have a useful life of approximately
 917 50 years.

918 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 919 to vulnerable communities in the Basin is presented below.

920 **S-26 Cost Estimate**

Structure Enhancement	\$ 7,101,519
Forward Pump (1735 cfs)	\$83,280,000
Forward Pump Backup Generator Facility	\$ 8,328,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$15,106,428
Real Estate	\$ 2,404,512
Total	\$118,220,458
2023 Adjusted Cost	\$ 144,858,126

921 **G-57 COASTAL STRUCTURE RESILIENCY**

This resiliency project is mainly tied to the District's mission to provide flood control and water supply protection. G-57 is a reinforced concrete, gated spillway with discharge controlled by two stem-operated, vertical lift gates measuring 6 ft. high by 14 ft. wide. Discharge capacity at G-57 is 375 cfs. Operation of the gates is automatically controlled so that the gate operating system opens or closes the gates in accordance with the operational criteria. The structure is located on the Old Pompano Canal just east of Cypress Road. This structure maintains upstream water control stages in Old Pompano Canal. The G-57 Structure was designed to 1) release the design flood without exceeding the upstream flood design

stage, 2) restrict downstream flood stages and channel velocities to non-damaging levels, and 3) prevent saline intrusion. G-57 is serviced by the Fort Lauderdale Field Station. The SFWMD FPLOS developed advanced H&H models to evaluate system operations under changed current and future conditions and recommended infrastructure investments in critical locations. Recent observations and FPLOS model results show that the G-57 Structure needs adaptation. The FPLOS results and recent observations show the G-57 Coastal Structure is no longer providing the design level of service, which impacts the overall flood protection level of service in the C-14 Basin. The flood protection level of service in the C-14 Basin is currently equivalent to a five-year rainfall/flood event recurrence interval. Level of service is reduced to a less than five-year event under a two-foot SLR scenario.

The entire population currently living in the C-14 Basin, estimated at 302,629, will directly or indirectly benefit from this project. The number of critical assets vulnerable to flooding under current and future conditions at C-14 Basin are 57. These include faith-based facilities, fire stations, hospitals and medical facilities, law enforcement centers, recreational facilities and schools. The state's public schools have a vital role in our communities during emergency storm evacuations and post-storm recovery efforts, serving as shelters for displaced residents and emergency response staging areas. Overall flood protection levels of service are expected to increase in the entire basin, as well as water supply protection from saltwater intrusion contamination with project implementation.

Enhancing the G-57 structure will restore discharge capacity by adding a forward pump to convey flood waters when the downstream water elevations preclude gravity flow. These modifications will protect flood prone areas within the C-14 Basin. The proposed project will provide 20-40 years of protection against SLR depending on the scenario (NOAA Intermediate Low or NOAA Intermediate High). Peak canal stage can be reduced by 15% by for each 500 cfs increase in pump capacity.

The purpose of this project is to build resiliency, restore the design discharge of the G-57 Structure and decrease flood impacts within the C-14 Basin due to SLR, climate change and land use changes in the basin. Project conceptual design is finalized. Final design will be based upon simulation of the combined regional and local hydraulic measures in the C-14 Basin. The G-57 structure will be enhanced and hardened by raising the bridge, converting the gate opening system to a more robust mechanism, replacing the existing gates with corrosion resistant stainless-steel gates and increased height, replacing the control building with a hardened and elevated control building, and adding a corrosion control system to the structure. Flood barriers will be constructed around the coastal structure to tie it back to higher land. The design of a forward

970 pump station will be adaptable and will include the ability to easily add additional pumps in the future as
 971 environmental conditions change.

972 The design life for the facility is 50 years with consideration for mechanical equipment being
 973 rehabilitated or replace over the design life. The engines may require at least one major overhaul during the
 974 design life while the pump materials will be designed to provide long service life. The structural and
 975 architectural design of the pump stations will include elements that will require minimum maintenance and
 976 repair over the design life.

977 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 978 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 979 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 980 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 981 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 982 to purchase real estate for the project are included. Negotiations with private property owners for land
 983 purchase will initiate upon funding confirmation.

984 **G-57 Cost Estimate**

Structure Enhancement	\$ 5,316,285
Forward Pump (200cfs)	\$10,312,500
Forward Pump Backup Generator Facility	\$ 1,031,250
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 2,799,005
Real Estate	\$ 7,000,000
Total	\$28,459,040
Adjusted 2023 Cost	\$ 33,394,620

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988 **S-22 COASTAL STRUCTURE RESILIENCY**

989 This resiliency project is mainly tied to the District’s mission to provide flood control and water supply
990 protection. S-22 is a two-bay, reinforced concrete
991 gated spillway located in C-2 (Snapper Creek)
992 Canal, about 7,000 feet from the mouth of
993 Biscayne Bay and about ten miles southwest of
994 downtown Miami. The C-2 Canal has as an open
995 channel connection with the C-4 Canal, west of
996 intersection of Turnpike and Miami SW 8th Street.
997 The structure has two (2) 15.0 feet high by 17.7
998 feet wide gates and a discharge capacity of 1905
999 cfs. The gates are operated by an electric driven
1000 cable drum. The gates can either be remotely
1001 operated from the District Control Room or
1002 controlled on-site. The purpose of S-22 is to permit
1003 release of flood runoff from the tributary basin,
1004 prevent over-drainage, and prevent saltwater
1005 intrusion during periods of extreme high tides. The structure maintains optimum stages upstream in the C-
1006 2 Canal. The structure is maintained by the Miami Field Station.



1007 The project consists of enhancing the S-22 Coastal Structure and installing forward pumps to increase
1008 its resiliency and maintain basin discharge levels while sea levels rise. The SFWMD has developed
1009 advanced H&H models to evaluate system operations under changed current and future conditions and
1010 recommended infrastructure investments in critical locations. Recent observations and model results show
1011 that the S-22 Structure needs adaptation.

1012 The FPLOS Assessment for the C-2 Basin will be available in 2023. A similar study to assess the
1013 impacts of SLR at tidal structures was conducted. The Low-lying Tidal Structure Assessment Susceptibility
1014 to SLR and Storm Surge report models show the level of service of the S-22 structure is equivalent to a
1015 100-year event recurrence interval under current (sea level) conditions. The structure does not meet the
1016 design level of service under a 0.5-foot SLR scenario beyond a ten-year event and would not meet the
1017 design level of service under a one-foot SLR scenario for all return periods (2yr, 5yr, 10yr, 25yr, 50yr,
1018 100yr).

1019 Enhancing the S-22 Structure will restore discharge capacity by adding a forward pump to convey flood
1020 waters when downstream water elevations preclude gravity flow. These modifications will protect flood
1021 prone areas within the C-2 Basin (population 289,878). The project will provide 20-40 years of protection
1022 against SLR depending on the scenario (NOAA Intermediate Low or NOAA Intermediate High). Peak
1023 canal stage can be reduced by 15% by for each 500cfs increase in pump capacity.

1024 The purpose of this project is to build resiliency, restore the design discharge of the S-22 Structure and
1025 decrease flood impacts within the C-2 Basin due to SLR, climate change and land use changes in the basin.
1026 Project conceptual design is finalized. Final design will be based upon simulation of the combined regional
1027 and local hydraulic measures in the C-2 Basin. The S-22 structure will be enhanced and hardened by raising
1028 the bridge, converting the gate opening system to a more robust mechanism, replacing the existing gates
1029 with corrosion resistant stainless-steel gates and increased height, replacing the control building with a
1030 hardened and elevated control building, and adding a corrosion control system to the structure. Flood
1031 barriers will be constructed around the coastal structure to tie it back to higher land. The design of a forward
1032 pump station will be adaptable and will include the ability to easily add additional pumps in the future as
1033 environmental conditions change. The proposed design includes pumping capacity of 1000 cfs.

1034 The design life for the facility is 50 years with consideration for mechanical equipment being
1035 rehabilitated or replace over the design life. The engines may require at least one major overhaul during the

1036 design life while the pump materials will be designed to provide long service life. The structural and
 1037 architectural design of the pump stations will include elements that will require minimum maintenance and
 1038 repair over the design life.

1039 The entire population currently living in the C-2 Basin, estimated at 289,878, will directly or indirectly
 1040 benefit from this project. The number of critical assets vulnerable to flooding under current and future
 1041 conditions at C-2 Basin are 300. These include faith-based facilities, fire stations, hospitals and medical
 1042 facilities, law enforcement centers, recreational facilities, and schools. The state's public schools have a
 1043 vital role in our communities during emergency storm evacuations and post-storm recovery efforts, serving
 1044 as shelters for displaced residents and emergency response staging areas. Overall flood protection levels of
 1045 service are expected to increase in the entire basin, as well as water supply protection from saltwater
 1046 intrusion contamination.

1047 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1048 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1049 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1050 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1051 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1052 to purchase real estate for the project are included. Negotiations with private property owners for land
 1053 purchase will initiate upon funding confirmation.

1054 **S-22 Cost Estimate**

Structure Enhancement	\$ 5,997,785
Forward Pump (1000cfs)	\$47,625,000
Forward Pump Backup Generator Facility	\$ 4,762,500
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 9,057,792
Real Estate	\$ 7,000,000
Total	\$76,443,078*
Adjusted 2023 Cost	\$92,414,986

1055 *May need to be replaced rather than refurbished, costs may be higher.

1056 **S-37A COASTAL STRUCTURE RESILIENCY**

1057



This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. This structure is a reinforced concrete, gated spillway with discharge controlled by two stem-operated, vertical lift gates. The structure has a discharge capacity of 3,890 cfs. Operation of the gates is automatically controlled so that the gate operating system opens or closes the gates in accordance with the operational criteria. The structure is located on C-14, 150 feet east of Dixie Highway and just east of the F.E.C. Railroad. The S-37A Structure was designed to 1) maintain optimum upstream water control stages in C-14; 2) release the design flood (40% and 60% of the Standard Project Flood from the western and eastern portions of the drainage basin, respectively) without

1073 exceeding the upstream flood design stage, 3) restricts downstream flood stages and channel velocities to
 1074 non-damaging levels; and 4) prevent saltwater intrusion during periods of extreme high tides. S-37A is
 1075 maintained by the Fort Lauderdale Field Station. A total cost estimate to harden this Coastal Structure, to
 1076 address flooding, SLR and other related risks to vulnerable communities in the Basin is presented below.
 1077 The estimate includes modifications to the existing structure and control building, as well as an additional
 1078 forward pump. The supplementary pumping capacity will extend the conveyance performance for
 1079 additional years as sea levels rise, delay out of bank flooding, and reduce canal peak stages. Placeholder
 1080 funds to tie the structure to higher land elevations and to purchase real estate for the project are included.
 1081 Negotiations with private property owners for land purchase will initiate upon funding confirmation.

1082 **S-37A Cost Estimate**

Structure Enhancement	\$ 6,240,444
Forward Pump (2000 cfs)	\$81,761,744.58
Forward Pump Backup Generator Facility	\$ 10,453,117
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 15,068,300
Real Estate	\$7,000,000
Total	\$122,523,638
Adjusted 2023 Cost	\$ 149,094,074

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1084 **G-58 COASTAL STRUCTURE RESILIENCY**

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This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. G-58 is a four-barrel corrugated metal pipe culvert located on Arch Creek immediately downstream from the Florida East Coast Railroad bridge. Features include one 60-inch culvert and three 72-inch culverts. The discharge capacity of this structure is 300 cfs. The G-58 Structure was designed to maintain optimum upstream water control stages in Arch Creek, 2) release the design flood (60% of the Standard Project Flood) without exceeding upstream flood design stage, 3) restrict downstream flood stages and discharge velocities to non-damaging levels, and 4) prevent saltwater intrusion during periods of extreme high tides. G-58 is serviced by the

1100 Miami Field Station.

1101 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1102 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1103 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1104 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1105 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1106 to purchase real estate for the project are included. Adjacent lands are owned by the State of Florida, which
 1107 will result in reduced real estate costs.

1108 **G-58 Cost Estimate**

Structure Enhancement	\$ 6,136,884
Forward Pump (75cfs)	\$ 4,125,000
Forward Pump Backup Generator Facility	\$ 412,500
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 1,901,157
Real Estate	\$ 3,000,000
Total	\$17,575,542
Adjusted 2023 cost	\$20,927,917

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1112 **S-123 COASTAL STRUCTURE RESILIENCY**

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This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. S-123 is a fixed crest, reinforced concrete, gated spillway, with discharge controlled by two cable operated, vertical lift gates measuring 12.7 ft. high by 25.0 ft. wide. Discharge capacity at this structure is 2,300 cfs. Operation of the gates is automatically controlled so that the gate hydraulic operating system opens or closes the gates in accordance with the operational criteria. The structure is located near the mouth of C-100 below the junction of C-100, C100A and C-100B and about 600 feet from the shore of Biscayne Bay. The S-123 Structure was designed to 1) maintain optimum water control stages upstream in

1131 Canals C- 100, C-100A, and C-100B, 2) release the design flood (40 percent of the Standard Project Flood)
 1132 without exceeding upstream flood design stage, 3) restrict downstream flood stages and discharge velocities
 1133 to non-damaging levels, and 4) prevent saltwater intrusion during periods of extreme high tides. The
 1134 structure is maintained by Miami Field Station.

1135 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1136 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1137 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1138 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1139 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1140 to purchase real estate for the project are included. Adjacent lands are owned by the State of Florida, which
 1141 will result in reduced real estate costs.

1142 **S-123 Cost Estimate**

1143

Structure Enhancement	\$ 6,533,070
Forward Pump (1150 cfs)	\$55,200,000
Forward Pump Backup Generator Facility	\$ 5,520,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$10,387,960
Real Estate	\$ 7,000,000
Total	\$86,641,030
Adjusted 2023 Costs	\$ 104,958,469

1144 **S-20F COASTAL STRUCTURE RESILIENCY**

Inspection Summary/Issue Identification

FY20 Update to FY15019 – (Updated 1-31-20)

S-20F Major Half-Life Refurbishment		Date: 1-31-2020
Structure Type: Spillway	Field Station / Contact: Homestead / Sean Smith	Priority Score: 17.02
Inspector Information		Priority Level: 2
Lead Inspector: Tim Kunard	Inspection Date: 1-6-20	Phone: 561-882-6305
Previous Inspection Date: 2-12-15	Previous Inspector: Gary Dunmyer	
F/S Superintendent: Sean Smyth	F/S Bureau Chief: Jesus Carrasco	
Signature: <i>[Signature]</i>	Signature: <i>[Signature]</i>	
Structure Details		
Description: Spillway	# Gates: 3	# Pumps: 0
	# Barrels: 0	Lifting Mechanism: Hydraulic

Figure 1 – Aerial Image of the S20F Structure site



This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. S-20F is a three-bay, reinforced concrete gated spillway, located on the L-31E Levee at its junction with C-103 (Mowry) Canal, about 2,000 feet from the shore of Biscayne Bay and 190 feet east of SW 320th Street, approximately 8.7 miles southeast of the City of Princeton in eastern Miami-Dade County. The structure consists of three 13.0 feet high by 25.0 feet wide gates and has a discharge capacity of 2,900 cfs. Discharge from the structure is controlled by three hydraulically driven cable operated vertical lift gates. The gates can either be remotely operated from the District Control Room or controlled on-site. The S-20F Structure was designed to 1) maintain optimum stages upstream along the C-103 Canal, 2) restricts downstream flood stages and discharge velocities to non-damaging levels. And 3) prevent saltwater intrusion during periods of extreme high tides. The structure is maintained by the Homestead Field Station.

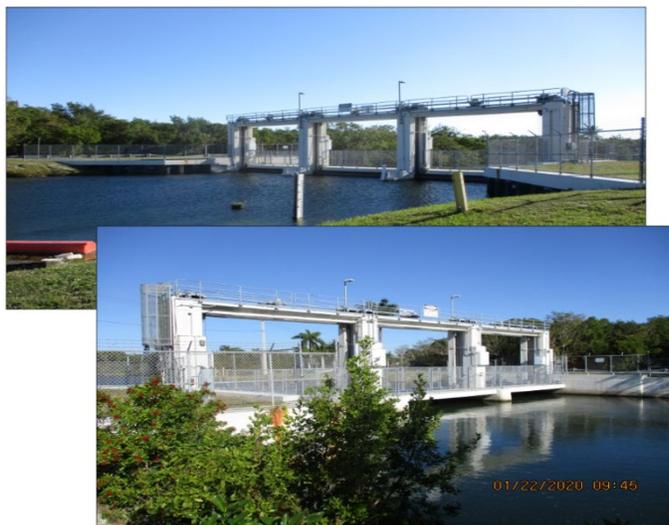
1165 address flooding, SLR and other related risks to vulnerable communities in the Basin is presented below.
 1166 The estimate includes modifications to the existing structure and control building, as well as an additional
 1167 forward pump. The supplementary pumping capacity will extend the conveyance performance for
 1168 additional years as sea levels rise, delay out of bank flooding, and reduce canal peak stages. Placeholder
 1169 funds to tie the structure to higher land elevations and to purchase real estate for the project are included.
 1170 Adjacent lands are owned by the United States of America and are part of Biscayne National Park, which
 1171 will result in reduced real estate costs.

1172 **S-20F Cost Estimate**

Structure Enhancement	\$ 7,312,238
Forward Pump (725 cfs)	\$36,975,000
Forward Pump Backup Generator Facility	\$ 3,697,500
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 7,497,710
Real Estate	\$ 7,000,000
Total	\$64,482,4450
Adjusted 2023 Cost	\$77,703,413

1173 **S-21 COASTAL STRUCTURE RESILIENCY**

1174



1190

This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. S-21 is a reinforced concrete gated spillway with three cable operated vertical lift gates, located near the mouth of C1 at its junction with L31E and about 3,500 feet from the shore of Biscayne Bay. Each gate measures 10.7 feet high by 27.8 feet wide. The discharge capacity of S-21 is 2,560 cfs. Operation of the gates is automatically controlled so that the hydraulic operating system opens or closes the gates in accordance with the operational criteria. The S21 Structure was designed to 1) maintain optimum water control stages upstream in C1, 2) restricts downstream flood stages and

1191 discharge velocities to non-damaging levels, and 3) prevent saltwater intrusion during periods of extreme
 1192 high tides. The gates can be remotely controlled by either the on-site controls or from the SFWMD Control
 1193 Room. Operation of the gate is automatically controlled so that the gate opens or closes in accordance with
 1194 the operational criteria.

1195 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1196 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1197 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1198 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1199 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1200 to purchase real estate for the project are included. Adjacent lands are owned by Miami-Dade County and
 1201 are part of a county park, which will result in reduced real estate costs.

1202 **S-21 Cost Estimate**

Structure Enhancement	\$ 7,328,487
Forward Pump (640 cfs)	\$32,640,000
Forward Pump Backup Generator Facility	\$ 3,264,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 6,784,873
Real Estate	\$ 7,000,000
Total	\$59,017,360
Adjusted 2022 Cost	\$70,981,354

1203

1204 **S-21A COASTAL STRUCTURE RESILIENCY**

1205 This resiliency project is mainly tied to the
 1206 District’s mission to provide flood control and
 1207 water supply protection. S-21A is a reinforced
 1208 concrete, two-bay, gated spillway located near
 1209 the mouth of C-102 canal (Princeton) at its
 1210 junction with the L-31E Levee, about a mile
 1211 from the shore of Biscayne Bay and
 1212 immediately east of SW 97th Avenue. The
 1213 structure consists of two 11.8 feet high by 20.8
 1214 feet wide gates and has a discharge capacity of
 1215 1300 cfs. The discharge from the structure is
 1216 controlled by two hydraulically driven cable
 1217 operated vertical lift gates. The gates can be
 1218 remotely controlled by either the on-site
 1219 controls or from the SFWMD Control Room.
 1220 Operation of the gate is automatically
 1221 controlled so that the gate opens or closes in accordance with the operational criteria. Upstream of S-21A,
 1222 the C-102 canal has an open junction with the L-31E canal on its north bank. The southern junction is
 1223 controlled by a gated project culvert. A new pump station (S-705) is scheduled to be constructed in this
 1224 junction as part of the Biscayne Bay Coastal Wetlands Project. The structure is maintained by Homestead
 1225 Field Station.



1226 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1227 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1228 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1229 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1230 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1231 to purchase real estate for the project are included. Adjacent lands are owned by Miami-Dade County,
 1232 which will result in reduced real estate costs.

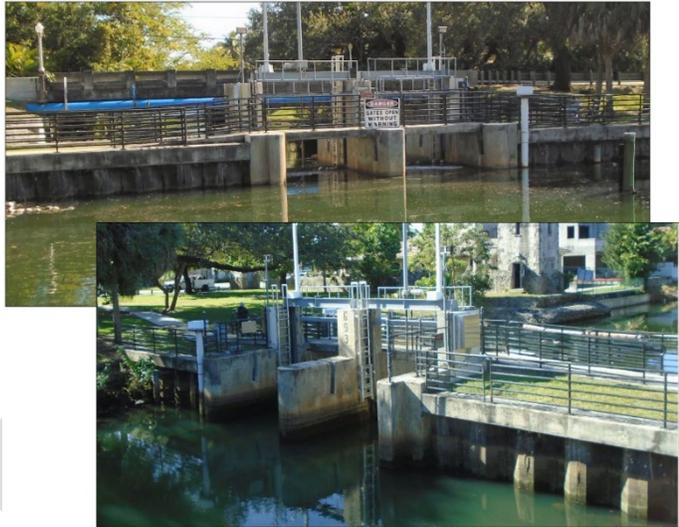
1233 **S-21A Cost Estimate**

1234

Structure Enhancement	\$ 6,288,289
Forward Pump (650 cfs)	\$33,150,000
Forward Pump Backup Generator Facility	\$ 3,315,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 6,712,993
Real Estate	\$ 7,000,000
Total	\$58,466,282
Adjusted 2023 Cost	\$ 70,303,527

1235 **G-93 COASTAL STRUCTURE RESILIENCY**

1236 This resiliency project is mainly tied to the
 1237 District’s mission to provide flood control and
 1238 water supply protection. G-93 is a two-bay,
 1239 reinforced concrete gated spillway with two
 1240 single stem vertical lift gates measuring 5.0
 1241 feet high by 10.0 feet wide on the C-3 (Coral
 1242 Gables) Canal, west of Southwest 57th Ave
 1243 (Red Road or SR959) in the City of Coral
 1244 Gables. This structure has a discharge capacity
 1245 of 640 cfs. The C-3 Canal has an open
 1246 connection to the C-4 Canal just east of the
 1247 Palmetto Expressway and continues about 4.1
 1248 miles downstream of G-93 through highly
 1249 urbanized South Miami areas before
 1250 discharging to Biscayne Bay at Sunrise
 1251 Harbor. The original structure, G-97, was
 1252 replaced in January 1990 by G-93. The structure maintains optimum upstream water control stages; it was
 1253 designed to pass 40% of the Standard Project Flood (SPF) plus a small discharge from the C-4 basin without
 1254 exceeding upstream flood design stage and restricts downstream flood stages and discharge velocities to
 1255 non-damaging levels; and it prevents saltwater intrusion during periods of high tides. The structure is
 1256 maintained by Miami Field Station.



1257 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1258 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1259 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1260 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1261 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1262 to purchase real estate for the project are included. Adjacent lands are owned by Miami-Dade County and
 1263 are part of Coral Gables Wayside Park, which will result in reduced real estate costs.

1264 **G-93 Cost Estimate**

Structure Enhancement	\$ 4,231,301
Forward Pump (320 cfs)	\$16,960,000
Forward Pump Backup Generator Facility	\$ 1,696,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 3,733,095
Real Estate	\$ 7,000,000
Total	\$35,620,397
Adjusted 2022 Cost	\$ 42,203,088

1265

S-25B COASTAL STRUCTURE RESILIENCY

1279

This resiliency project is mainly tied to the District's mission to provide flood control and water supply protection. S-25B is a two-bay, reinforced concrete gated spillway located in the City of Miami immediately east of the Northwest 42nd Avenue (Le Jeune Road) crossing of the C-4 (Tamiami) Canal, east of Miami International Airport. The structure consists of two 11.9 feet high by 22.8 feet wide gates with a discharge capacity of 2000 cfs. The gates are controlled by two hydraulically driven cable operated vertical lift gate mechanisms. The gates can either be remotely operated from the District Control Room or controlled on-site. Structure S-25B controls flow from the C-4 canal to the Miami Canal downstream of S-26. The structure maintains optimum stages

1280 upstream in the C-4 Canal. It was designed to pass 100% of the Standard Project Flood (SPF) for the eastern
 1281 portion of the C-4 basin without exceeding upstream flood design stage and restricts downstream flood
 1282 stages and discharge velocities to non-damaging levels; and it prevents saltwater intrusion from the Miami
 1283 Canal during periods of extreme high tides. This structure also includes a forward pump station. The S-25B
 1284 Forward Pump station is a reinforced concrete, electric pump station, with discharge controlled by three
 1285 200 cfs pumps. These pumps were added to the gravity structure S-25B in 2002 to maintain discharges
 1286 from the land side to the seaside of the structure when gravity capacity is limited, or the gates need to be
 1287 closed due to the threat of saltwater intrusion. The pumped water flows into the 120-foot box culvert that
 1288 runs under and along the edge of a golf course south of the S-25B spillway and discharges downstream
 1289 (east) of S-25B into the C-4 Canal. The culvert is 10 feet high by 8 feet wide and consists of segmental
 1290 sections with bell and spigot type connections. The pumps can either be remotely operated from the District
 1291 Control Room or controlled on-site. This structure is operated in coordination with the adjacent S-25B
 1292 spillway. The structure is maintained by Miami Field Station.

1293 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1294 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1295 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1296 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1297 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1298 to purchase real estate for the project are included. Adjacent lands are owned by Miami-Dade County,
 1299 which will result in reduced real estate costs.

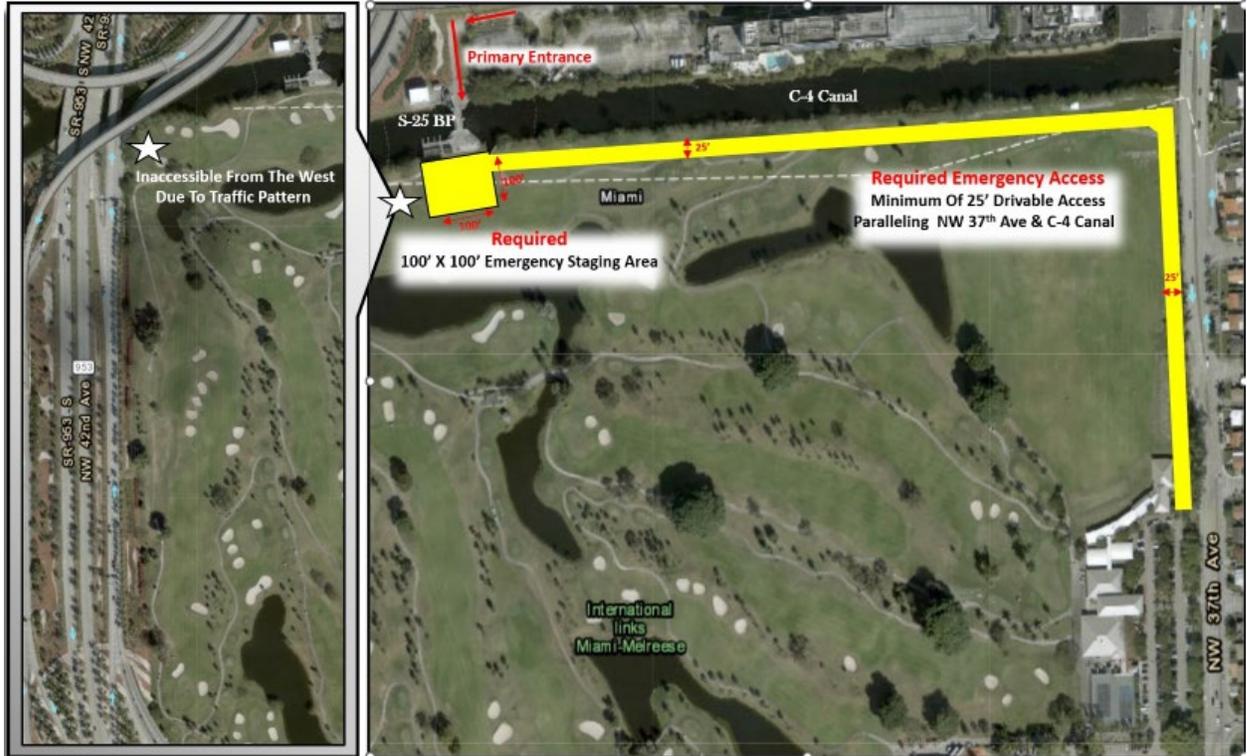


Figure 9-18: Real estate needs for S-25.

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S-25B Cost Estimate

Structure Enhancement	\$ 6,465,811
Forward Pump (1000 cfs)	\$48,000,000
Forward Pump Backup Generator Facility	\$ 4,800,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 9,189,872
Real Estate	\$ 7,000,000
Total	\$77,455,683
Adjusted 2023 Cost	\$ 93,660,490

1304

1305 **G56 COASTAL STRUCTURE RESILIENCY**

1306

1307 This resiliency project is mainly tied to the
 1308 District’s mission to provide flood control and
 1309 water supply protection. G-56 is a reinforced
 1310 concrete gated spillway, with discharge
 1311 controlled by three cable operated, vertical lift
 1312 gates. This structure has a discharge capacity of
 1313 3,760 cfs. The gates are operated on-site or
 1314 remotely from the District Control Room. The
 1315 new structure was completed in 1991 to replace
 1316 the old Deerfield Lock Structure. The structure
 1317 is located near the mouth of the Hillsboro
 1318 Canal, about two miles west of Deerfield
 1319 Beach. This structure maintains optimum water
 1320 control stages in the Hillsboro Canal. It passes
 1321 flood flows while limiting the upstream stage,
 1322 downstream stage and channel velocity. G56 is serviced by the Fort Lauderdale Field Station.



1323 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1324 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1325 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1326 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1327 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1328 to purchase real estate for the project are included. Negotiations with private property owners for land
 1329 purchase will initiate upon funding confirmation.

1330 **G-56 Cost Estimate**

Structure Enhancement	\$ 8,859,343
Forward Pump (1880 cfs)	\$90,240,000
Forward Pump Backup Generator Facility	\$ 9,024,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$16,518,501
Real Estate	\$ 7,000,000
Total	\$133,641,844
Adjusted 2023 Cost	\$162,769,468

1331

1332

1333 **G-54 COASTAL STRUCTURE RESILIENCY**

1334



This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. G-54 is a reinforced concrete gated spillway, located on the North New River Canal about 0.9 mile west of the intersection of I-595 and Florida’s Turnpike, west of Ft. Lauderdale. The structure consists of three 9.5 feet high by 16 feet wide gates with a discharge capacity of 1,600 cfs. The discharge from this structure is controlled by hydraulically driven cable operated vertical lift gates. The gates can either be remotely operated from the District Control Room or controlled on-site. Construction of G-54 was completed in 1992 to replace the old Sewell Lock Structure. This structure maintains optimum water control stages in the North New River canal. It passes watershed flows or regulatory releases from Water Conservation Area (WCA)-2 while

1354

1355 limiting the upstream stage, and channel velocity. G-54 is serviced by the Fort Lauderdale Field Station.

1356 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1357 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1358 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1359 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1360 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1361 to purchase real estate for the project are included. Negotiations with private property owners for land
 1362 purchase will initiate upon funding confirmation.

1363 **G-54 Cost Estimate**

Structure Enhancement	\$ 8,023,036
Forward Pump (800 cfs)	\$40,000,000
Forward Pump Backup Generator Facility	\$ 4,000,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 8,103,455
Real Estate	\$7,000,000
Total	\$ 69,126,492
Adjusted 2023 Cost	\$ 83,451,585

1364 **S-25 COASTAL STRUCTURE RESILIENCY**

1365 This resiliency project is mainly tied to the
 1366 District’s mission to provide flood control and water
 1367 supply protection. S-25 is a single barrel, corrugated
 1368 metal pipe culvert with a reinforced-concrete headwall
 1369 and operating platform on the upstream (west) side.
 1370 The structure is in the C-5 (Comfort) Canal, at the exit
 1371 ramp from the East-West Dolphin Expressway (SR
 1372 836) and the crossing of Northwest 27th Avenue in the
 1373 City of Miami. The structure consists of one 9.1 feet
 1374 high by 8.3 feet wide gate with a discharge capacity of
 1375 320 cfs. S-25 can either be remotely operated from the
 1376 District Control Room or controlled on-site. S-25
 1377 maintains an optimum upstream stage in C-5 Canal; it
 1378 was designed to pass 1-in-10 flood without exceeding
 1379 upstream flood design stage and restricts downstream
 1380 flood stages and discharge velocities to non-damaging
 1381 levels; and it prevents saltwater intrusion during
 1382 periods of extreme high tides. The structure is
 1383 maintained by Miami Field Station.



1384 A total cost estimate to harden this Coastal
 1385 Structure, to address flooding, SLR and other related risks to vulnerable communities in the Basin is
 1386 presented below. The estimate includes modifications to the existing structure and control building, as well
 1387 as an additional forward pump. The supplementary pumping capacity will extend the conveyance
 1388 performance for additional years as sea levels rise, delay out of bank flooding, and reduce canal peak stages.
 1389 Placeholder funds to tie the structure to higher land elevations and to purchase real estate for the project are
 1390 included. Negotiations with private property owners for land purchase will initiate upon funding
 1391 confirmation. A portion of the needed property is owned by the Florida Department of Transportation,
 1392 which may reduce land acquisition costs.

1393

1394 **S-25 Cost Estimate**

Structure Enhancement	\$ 3,695,352
Forward Pump (160 cfs)	\$ 8,800,000
Forward Pump Backup Generator Facility	\$ 880,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 2,306,303
Real Estate	\$ 7,000,000
Total	\$24,681,654
Adjusted 2023 Cost	\$ 28,748,435

1395

1396 **S-33 COASTAL STRUCTURE RESILIENCY**

1397



This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. S-33 is a reinforced concrete, gated spillway with discharge controlled by a cable operated, vertical lift gate that is 9.0 feet high by 20.0 feet wide. The structure has a discharge capacity of 920 cfs. The gates can be remotely controlled by either the on-site controls or from the SFWMD Control Room. Operation of the gate is automatically controlled so that the gate opens or closes in accordance with the operational criteria. The structure is located on C-12 about 1/2 mile east of State Road 7. This structure maintains optimum upstream water control stages in C-12; it passes the design flood (50% of the Standard Project Flood) without exceeding the upstream flood design stage and restricts downstream flood

1415 stages and channel velocities to non-damaging levels, and it prevents saltwater intrusion into the area west
 1416 of the structure. S-33 is maintained by the Fort Lauderdale Field Station.

1417 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1418 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1419 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1420 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1421 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1422 to purchase real estate for the project are included. Negotiations with private property owners for land
 1423 purchase will initiate upon funding confirmation.

1424 **S-33 Cost Estimate**

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1426

Structure Enhancement	\$ 4,237,616
Forward Pump (230 cfs)	\$12,650,000
Forward Pump Backup Generator Facility	\$ 1,265,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 3,022,892
Real Estate	\$ 7,000,000
Total	\$30,175,509
Additional 2023 Cost	\$ 35,505,876

1427 **S-20G COASTAL STRUCTURE RESILIENCY**

1428

1429 This resiliency project is mainly tied to the
 1430 District’s mission to provide flood control and water
 1431 supply protection. S-20G is a reinforced concrete gated
 1432 spillway located near the mouth of the Military Canal at
 1433 its junction with the L-31E Levee, about 2,300 feet from
 1434 the shore of Biscayne Bay. The structure is located
 1435 immediately north of SW 301 Street, approximately 8
 1436 miles east of the City of Homestead in eastern Miami-
 1437 Dade County. The structure consists of one 12.3 feet
 1438 high by 25.8 feet wide gate. The discharge capacity of
 1439 S-20G is 900 cfs. The structure is controlled by a
 1440 hydraulically driven cable operated vertical lift gate.
 1441 The gate can either be remotely operated from the
 1442 District Control Room or controlled on-site. Operation
 1443 of the gate is automatically controlled so that the hydraulic operating system opens or closes the gate in
 1444 accordance with the operational criteria. Upstream of S-20G, the Military Canal does not have open junctions
 1445 with the L-31E levee and both junctions are controlled by gated (flashboard riser) project culverts (L-31E PC-
 1446 17&18). The northern junction is controlled by Project Culvert L-31E PC-17, which controls flow between
 1447 the C-102 (S-21A) basin and the Military Canal (S-20G) basin. The southern junction is controlled by Project
 1448 Culvert L-31E PC-18, which controls flow between the C-103 (S-20F) basin and the Military Canal (S-20G)
 1449 basin. The structure maintains optimum stages upstream in the Military Canal and restricts downstream flood
 1450 stages and discharge velocities to non-damaging levels; and it prevents saltwater intrusion during periods of
 1451 extreme high tides. S-20G is maintained by Homestead Field Station.



1452 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1453 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1454 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1455 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1456 flooding, and reduce canal peak stages. The District owns all the adjacent lands, which will eliminate real
 1457 estate acquisition costs.

1458 **S-20G Cost Estimate**

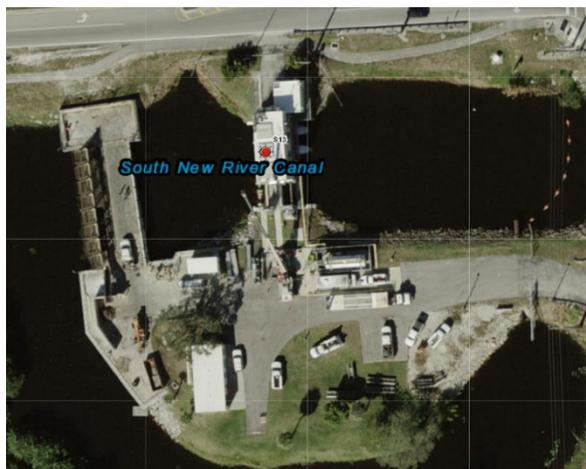
1459

Structure Enhancement	\$ 4,084,410
Forward Pump (225 cfs)	\$12,375,000
Forward Pump Backup Generator Facility	\$ 1,237,500
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 2,954,536
Real Estate	\$ 7,000,000
Total	\$29,651,446*
Adjusted 2023 Cost	\$34,861,279

1460 *May need to be replaced rather than refurbished, costs may be higher.

1461 **S-13 COASTAL STRUCTURE RESILIENCY**

1462



This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. S-13 is a pump station with a gated spillway that can control flow that bypasses the pumps. The structure is in C-11 (South New River Canal) about 300 feet west of U.S. Highway 441 and 5.5 miles southwest of Fort Lauderdale. It is a reinforced concrete structure with a concrete block superstructure. The pump station has a capacity of 540cfs at a 4-foot static head and is powered by a diesel engine. The gated spillway features a 16-foot wide by 11-foot-high vertical lift gate which is raised or lowered by means of stem hoists. Operation of the gate is normally controlled automatically but may be controlled

1477 manually during emergencies or for servicing. Other equipment includes a 5-ton manually operated
 1478 overhead bridge crane for general maintenance. The purpose of the structure is to release flood runoff from,
 1479 prevent over drainage of, and saltwater intrusion into the agricultural area served by C-11 (South New River
 1480 Canal) west of the structure. The spillway and pump station were designed to move surplus water from
 1481 agricultural areas in the western portion of the basin at a rate of 3/4 inch per day while keeping water levels
 1482 in the canal west of the structure at an optimum water control stages. The agricultural areas have almost
 1483 completely converted to residential and commercial use. This structure is maintained by the Fort Lauderdale
 1484 Field Station.

1485 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1486 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1487 existing structure and control building. The current site contains 3.5 acres. There is no additional room to
 1488 expand, which will eliminate land acquisition costs.

1489 **S-13 Cost Estimate**

1490

1491

Structure Enhancement	\$32,269,673
Forward Pump	\$ -
Forward Pump Backup Generator Facility	\$ -
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 5,140,451
Real Estate	\$ -
Total	\$39,410,124
Adjusted 2023 Cost	\$48,474,453

1492 **S-36 COASTAL STRUCTURE RESILIENCY**

1493

1494 This resiliency project is mainly tied to the
 1495 District’s mission to provide flood control and water
 1496 supply protection. S-36 is a reinforced concrete, gated
 1497 spillway with discharge controlled by a cable operated,
 1498 vertical lift gate that is 14.0 ft. high by 25.0 ft. wide.
 1499 The structure has a discharge capacity of 1,090 cfs.
 1500 Operation of the gate is automatically controlled so that
 1501 the gate electric motor opens or closes the gate in
 1502 accordance with the seasonal operational criteria. The
 1503 structure is located on C-13 west of Oakland Park. The
 1504 S-36 Structure was designed to 1) maintain optimum
 1505 water control stages upstream in C-13, 2) release the
 1506 design flood (50 percent of the Standard Project Flood)
 1507 without exceeding upstream flood design stage, 3)
 1508 restrict downstream flood stages and discharge
 1509 velocities to non-damaging levels, and



1510 4) prevent saltwater intrusion during periods of extreme high tides. S-36 is maintained by the Fort
 1511 Lauderdale Field Station.

1512 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1513 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1514 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1515 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1516 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1517 to purchase real estate for the project are included. Can only expand south into property owned by the City
 1518 of Oakland Park, which will reduce acquisition costs.

1519 **S-36 Cost Estimate**

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1521

1522

Structure Enhancement	\$ 4,619,722
Forward Pump (275 cfs)	\$14,442,500
Forward Pump Backup Generator Facility	\$ 1,444,250
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 3,375,971
Real Estate	\$ 7,000,000
Total	\$32,882,443
Adjusted 2023 Cost	\$ 38,835,405

1523 **S-197 COASTAL STRUCTURE RESILIENCY**

1524 This resiliency project is mainly tied to
 1525 the District’s mission to provide flood control
 1526 and water supply protection. S-197 is a four-
 1527 barrel cast-in-place concrete box culvert with
 1528 four vertical slide gates measuring 10.0 ft x
 1529 10.0 ft. The structure has a discharge capacity
 1530 of 2,400 cfs. S-197 is located upstream of the
 1531 mouth of the C-111 about three miles from the
 1532 shore of Manatee Bay and 750 ft east of U.S.
 1533 Highway 1. The gates are manually operated
 1534 by the field station. Real time stage data are
 1535 available through telemetry. The S-197
 1536 maintains optimum water control stages
 1537 upstream in the C-111 Canal, prevents
 1538 saltwater intrusion during high tides and blocks
 1539 reverse flow during storm surges. This
 1540 structure usually remains closed to divert
 1541 discharges from S-18C overland to the panhandle of the Everglades National Park. S-197 is opened for
 1542 flood control when the overland flow capacity, with S-197 closed, is insufficient. This structure is
 1543 maintained by the Miami Field Station.



1544 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1545 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1546 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1547 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1548 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1549 to purchase real estate for the project are included. Adjacent lands are owned by the District and Miami-
 1550 Dade County, which will reduce land acquisition costs.

1551 The Biscayne Bay and Southeastern Everglades Ecosystem Restoration (BBSEER) Project is
 1552 formulating plans to restore parts of the south Florida ecosystem in freshwater wetlands of the Southern
 1553 Glades and Model Lands, the coastal wetlands and subtidal areas, including mangrove and seagrass areas,
 1554 of Biscayne Bay, Biscayne National Park, Manatee Bay, Card Sound and Barnes Sound. As part of project
 1555 formulation, management measures being proposed as part of modeling alternatives under discussions
 1556 include the removal of S-197 Coastal and backfilling of lower C-111 canal from 19-c to C-197. As final
 1557 alternatives are formulated, there is need to ensure the flood protection level of service in the project
 1558 influence area is maintained.

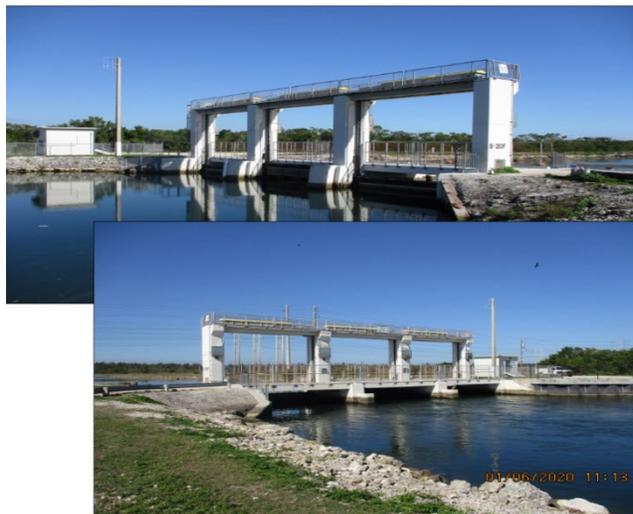
1559 **S-197 Cost Estimate**

1560

Structure Enhancement	\$ 6,358,510
Forward Pump (600 cfs)	\$30,600,000
Forward Pump Backup Generator Facility	\$ 3,060,000
Structure Tie Back (Flood Barrier)	\$ 2,000,000
Design, Implementation & Construction Management	\$ 6,302,776
Real Estate	\$ 7,000,000
Total	\$55,321,286
Adjusted 2023 Cost	\$ 66,435,182

1561 **S-20 COASTAL STRUCTURE RESILIENCY**

1562



This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. S-20 is a reinforced concrete, gated spillway located on L-31E about three miles from the shore of Biscayne Bay. The structure has a discharge capacity of 450 cfs, with discharge controlled by a cable operated, vertical lift gate that is 11.4 feet high by 16.8 feet long. Operation of the gate is automatically controlled so that the gate’s hydraulic operating system opens or closes the gate in accordance with the seasonal operational criteria. The S-20 Structure was designed to 1) maintain optimum water stages in the upstream agricultural area, 2) release the design flood (40 percent of the

1578 Standard Project Flood) without exceeding upstream flood design stage, 3) restrict downstream flood stages
 1579 and discharge velocities to non-damaging levels, and 4) prevents saltwater intrusion during periods of
 1580 extreme high tides. The structure is maintained by the Homestead Field Station.

1581 A total cost estimate to harden this Coastal Structure, to address flooding, SLR and other related risks
 1582 to vulnerable communities in the Basin is presented below. The estimate includes modifications to the
 1583 existing structure and control building, as well as an additional forward pump. The supplementary pumping
 1584 capacity will extend the conveyance performance for additional years as sea levels rise, delay out of bank
 1585 flooding, and reduce canal peak stages. Placeholder funds to tie the structure to higher land elevations and
 1586 to purchase real estate for the project are included. Adjacent lands are owned by the District and Florida
 1587 Power& Light, which may reduce land acquisition costs.

1588 **S-20 Cost Estimate**

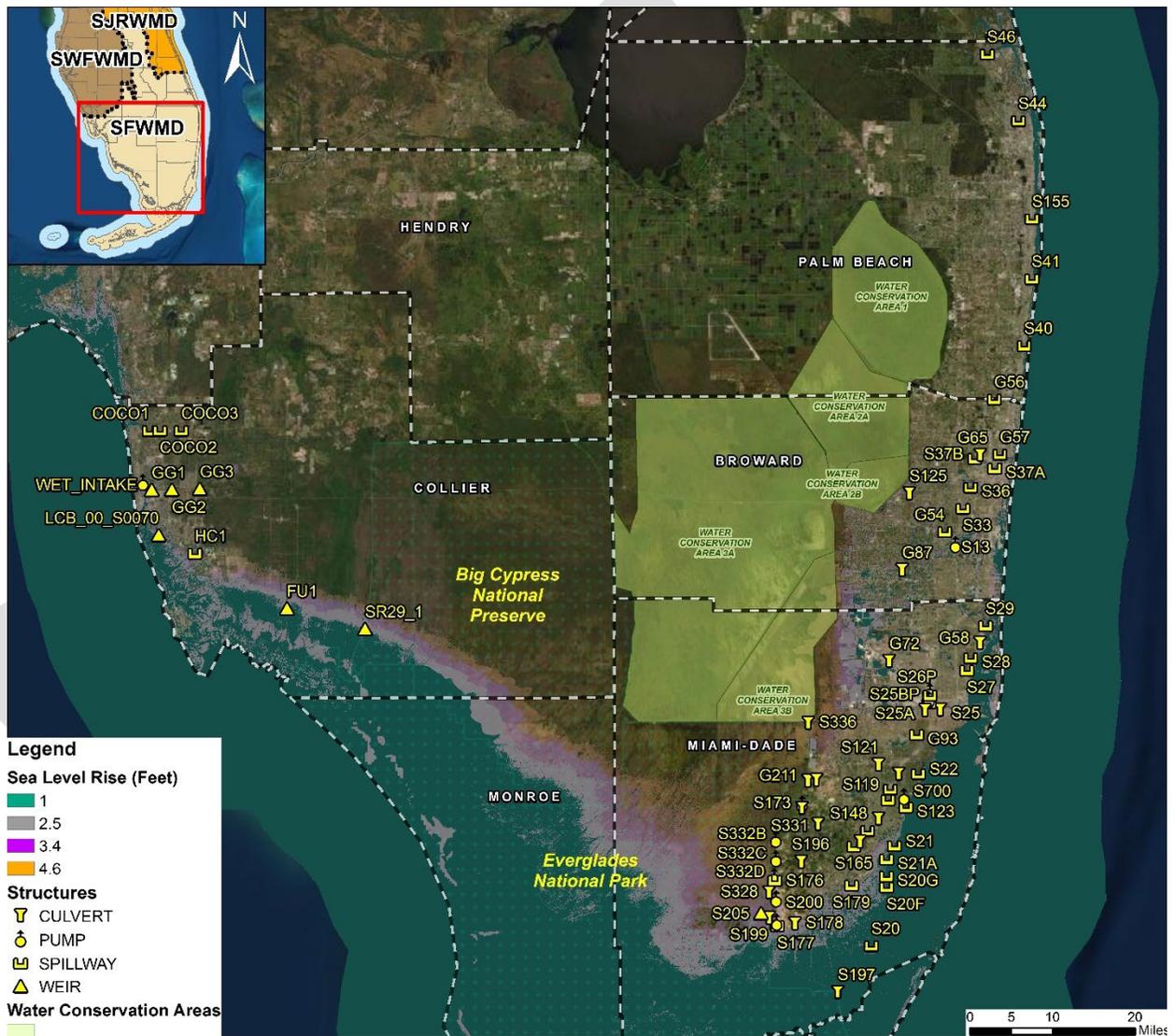
1589

Structure Enhancement	\$4,198,152
Forward Pump	\$6,187,500
Forward Pump Backup Generator Facility	\$618,750
Structure Tie Back (Flood Barrier)	\$2,000,000
Design, Implementation & Construction Management	\$1,950,660
Real Estate	\$7,000,000
Total	\$21,955,062*
Adjusted 2023 Cost	\$ 25,394,727

1590 *May need to be replaced rather than refurbished, costs may be higher.

1591 **REMAINING WATER CONTROL STRUCTURES RESILIENCY**

1592 These resiliency projects link to the District’s mission to provide flood control and water supply
 1593 protection. Additional water control structures are vulnerable to SRL and other changing conditions. As
 1594 estimated projections are realized into the future, there will be the need to enhance the remaining structures
 1595 not detailed in this Plan, to increase their resiliency, and maintain operational performance. Figure 9-19
 1596 below illustrate four SLR scenarios and inundation levels expected to occur by the end of this century, and
 1597 the location of critical water control structures that integrate the C&SF System and Big Cypress Basin, in
 1598 relation to these scenarios.



1599
 1600 **Figure 9-19.** Potential impacts of rising sea levels in South Florida to water control structures.

1601 An initial placeholder costs are being proposed for structures identified to be within the inundation
 1602 scenarios illustrated in figure 9-19 above. These structures have not yet been assessed through H&H
 1603 Models, and it will be refined during future modeling efforts and pre-design stages. The proposed costs are
 1604 estimated to enhance Coastal Structures identified in Table 9-6, to address flooding and other related risks
 1605 to vulnerable communities at the respective basin level due to land development and changed climate
 1606 conditions, including sea-level rise. The enhanced structures capacity will extend their performance for

1607 additional years as seas rise, delay out of bank flooding, and reduce canal peak stages. These investments
 1608 will need to be combined with additional upstream and downstream solutions to be characterized as part of
 1609 FPLOS Phase II Adaptation Strategies and detailed as part of future design phases. Additional projects costs
 1610 detailed below were estimated for project recommendations from FPLOS Phase I Studies, as summarized
 1611 in Appendix A.

1612 **Table 9-6.** Remaining Coastal Structures and placeholder costs.

Coastal Structures	Basin Name	Area (Acres)	Structure Enhancement Overall Estimated Costs (Placeholder)
G211	8.5 SQ. MILE AREA	4764.33	\$ 34,376,000.00
S119	C-100 WEST	16660.17	\$ 34,376,000.00
S148	C-1 WEST	32624.60	\$ 34,376,000.00
S155	C-51 EAST	47012.34	\$ 34,376,000.00
S165	C-102 WEST	8405.92	\$ 34,376,000.00
S178	C-111 AG	17563.47	\$ 34,376,000.00
S179	BD-C103 CENTRAL/WEST	22685.71	\$ 34,376,000.00
S200	FROG POND DETENTION AREA	1727.37	\$ 34,376,000.00
S331	L-31NS	16838.66	\$ 34,376,000.00
S332B	NDA	2788.98	\$ 34,376,000.00
S332C	SDA	2473.26	\$ 34,376,000.00
S332D	S332D DETENTION AREA	3155.06	\$ 34,376,000.00
S37B	C-14 WEST	32246.98	\$ 34,376,000.00
S40	C-15	39423.02	\$ 34,376,000.00
S41	C-16	39812.66	\$ 34,376,000.00
S44	C-17	22357.07	\$ 34,376,000.00
S46	C-18 / CORBETT	65735.53	\$ 34,376,000.00
			\$ 34,376,000.00
COCO1	COCOATCHEE	17628.52919	\$ 34,376,000.00
COCO2	COCOATCHEE	17628.52919	\$ 34,376,000.00
COCO3	COCOATCHEE	17628.52919	\$ 34,376,000.00
FU1	BIG CYPRESS BASIN	135740.3529	\$ 34,376,000.00
G65	C-14 EAST / C-14 WEST, POMPANO CANAL	36493.85798	\$ 34,376,000.00
G72	C-7 / C-6	54651.027	\$ 34,376,000.00
G737	FROG POND	1727.365874	\$ 34,376,000.00
G87	C-11 EAST / WEST, C-9 EAST / WEST	122772.61089	\$ 34,376,000.00
GG1	GOLDEN GATE MAIN	71253.58016	\$ 34,376,000.00
GG2	GOLDEN GATE MAIN	71253.58016	\$ 34,376,000.00
GG3	GOLDEN GATE MAIN	71253.58016	\$ 34,376,000.00
HC1	HENDERSON – BELLE MEADE	47538.70388	\$ 34,376,000.00
LCB_00_S0070	EAST NAPLES	7390.151115	\$ 34,376,000.00
S118	C-100 WEST	16660.16722	\$ 34,376,000.00

Coastal Structures	Basin Name	Area (Acres)	Structure Enhancement Overall Estimated Costs (Placeholder)
S120	C-100 WEST	16660.16722	\$ 34,376,000.00
S700	C-100 EAST/ C-100 WEST	25085.83454	\$ 34,376,000.00
S125	C-13 WEST, NORTH NEW RIVER CANAL WEST	33206.587	\$ 34,376,000.00
S149	C-1 WEST	32624.5955	\$ 34,376,000.00
			\$ 34,376,000.00
S195	C-102 WEST	8405.921685	\$ 34,376,000.00
S173	L-31NS, L-31 N CC	16923.28842	\$ 34,376,000.00
S176	L-31NS	16838.65942	\$ 34,376,000.00
S177	C-111 AG	17563.46884	\$ 34,376,000.00
S199	C-111 AG	17563.46884	\$ 34,376,000.00
S194	C-31NS, C-102 EAST / C-102 WEST	31884.239	\$ 34,376,000.00
S196	L-31NS, BD-C103 CENTRAL / WEST, BD-C103 EAST, NO-CANAL	46488.84507	\$ 34,376,000.00
S121	C-2	33654.88486	\$ 34,376,000.00
S205	S332D DETENTION AREA	3155.062	\$ 34,376,000.00
S328	S332D DETENTION AREA	3155.061629	\$ 34,376,000.00
S205	S332D DETENTION AREA	3155.061629	\$ 34,376,000.00
S33	C-12W	4780.585242	\$ 34,376,000.00
S173	L-31N CC	84.628584	\$ 34,376,000.00
S336	L-29 CC	225.026396	\$ 34,376,000.00
S338	L-29 CC, C-1 EAST / C-1 WEST	38089.795396	\$ 34,376,000.00
S125	C-13 WEST	15322.8794	\$ 34,376,000.00
S700	C-100 EAST / C-100 WEST	25085.83454	\$ 34,376,000.00
S79, S79_LOCK	WEST CALOOSAHATCHEE	349589.7829	\$ 34,376,000.00
SR29_1	BARRON RIVER	29690.7493	\$ 34,376,000.00
TOTAL			\$ 1,890,680,000.00

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1616 **SELF-PRESERVATION MODE AT CRITICAL STRUCTURES, COASTAL**
1617 **STRUCTURES ENHANCEMENT AND STORM SURGE PROTECTION**

1618



1654

This resiliency project is mainly tied to the District’s mission to provide flood control and water supply protection. Implementation of self-preservation mode at water control structures means building or retrofitting structures with systems that make the structure and its operation more resilient. A self-preservation mode system includes a backup system that can be programmed to operate the structure appropriately and independently, without the direct control of water managers. Adding self-preservation mode capabilities to critical water control structures will allow water managers to manage the system for flood control, water

1635 supply, environmental restoration, and saltwater intrusion prevention even when communication with the
1636 structure is lost due to weather or other circumstances.

1637 Currently, in advance of storm onslaught, storm surge modeling predictions are compared to the
1638 finished floor elevations of the coastal structures to determine which finished floor elevations are below the
1639 predicted surge elevation. District staff then disable the power and back-up generator with the structure
1640 gates fully open to avoid permanent damage to the electrical system which could occur if the structure were
1641 energized during the predicted storm surge event. This so-called “structure lockout” is performed with the
1642 gates open to reduce the risk of damage to the structure and so that storm generated runoff can pass through
1643 the structure even if the gates are no longer operational. However, this procedure also allows smaller storm
1644 surge events to pass through the structure and propagate upstream when it could have potentially been
1645 blocked by closing the gates.

1646 Manually operated structures require that decisions to release water be made long before storm impacts
1647 affect a given area. Water releases from non-automated structures must be done while it is safe for staff to
1648 visit the site to implement pre-storm operations. Automated structures allow water managers to delay water
1649 releases until they are warranted, which can help to avoid over-draining the area upstream, particularly
1650 when storm conditions do not occur as originally predicted. Structures with self-preservation mode
1651 capabilities can mitigate the consequences of a change in a storm’s path because they allow more flexible
1652 operational strategies. Structures with self-preservation mode capabilities can preserve environmentally
1653 sensitive lands and prevent damage to stormwater treatment areas, caused by over-draining the area
1654 unnecessarily. Structures with self-preservation mode capabilities can also help avoid prolonged drought
1655 conditions that can occur when water is released late in the wet season in anticipation of a storm that does
1656 not materialize.

1657

1658 Once self-preservation features are added to critical structures, gates will continue to be operable during
1659 the initial onslaught of the storm, well after it is no longer safe for personnel to travel to the site to manually
1660 disable the power and backup generator. Additionally, adding an independent system override to the gate
1661 controls and/or a pre-hurricane-initiated program to the local Remote Terminal Unit (RTU) and/or Backup
1662 Controller (BUC) so that the structure will operate as desired even if communications are lost. For example,
1663 if tailwater stage reaches a specific pre-determined high elevation, the structure will shut itself off by going
1664 into a lockdown mode that first opens all gates and then shuts off commercial power and disables the
1665 generator.

SELF-PRESERVATION MODE FOR COMBATTING STORM SURGE DAMAGES AND SALTWATER INTRUSION AT COASTAL WATER CONTROL STRUCTURES

- MAXIMIZING THE OPERATIONAL CAPACITY AT CRITICAL WATER CONTROL STRUCTURES
- DETERMINATION OF ELEVATION TO EXTEND GATES TO PREVENT REVERSE FLOW DURING A NON-STORM RELATED EXTREME HIGH TIDE OR MINOR STORM
- OPTIMIZING THE TIME TO OPEN AND CLOSE GATES BEFORE STORM SURGE INUNDATES CRITICAL EQUIPMENT AND/OR DAMAGES THE STRUCTURE
- AVOIDING UNNECESSARY LOCKOUTS

1666 The coastal structures were originally intended to provide a barrier to reduce saltwater intrusion without
1667 increasing flood risk from rainfall in the basin. They were not designed to provide robust storm surge
1668 protection; however, some surge protection can be achieved during less significant events. Therefore, the
1669 ability to operate structure gates for an extended period into a storm event is desirable. In many cases, the
1670 tops of structure gates can be extended to maximize the ability to protect against storm surge. The elevation
1671 for self-preservation mode to begin the lockdown procedure should be higher than a non-storm related
1672 extreme high tide which may already result in reverse flow over the closed gates, but low enough to allow
1673 time for all gates to open fully before the storm surge inundates critical equipment that could be damaged
1674 due to pressure on closed gates. The infrastructure to accomplish this must be hardened such that it is not
1675 susceptible to damage from windblown debris and/or storm surge. The lockdown would be lifted manually
1676 by District staff sent to the site to evaluate any damage to the mechanical and electrical systems after the
1677 all-clear has been issued after a storm event. Like the current pre-storm lockdown, after the storm has
1678 passed, if damage has occurred the gates would remain open or be operated by alternate means (portable
1679 generator, crane, other temporary measures) until repairs have been completed.

1680 The District will prioritize the implementation of a self-preservation mode system that will enhance
1681 electrical components and sensors in critical coastal structures to maximize our operational capacity and
1682 minimize the time gates need to be locked in the open position, given anticipated storm surge scenarios.

1683 Considering recently observed and projected increases in frequent storm surge/ high tailwater conditions,
1684 maximizing operational flexibility of coastal structures is necessary for optimal flood control and
1685 prevention of saltwater intrusion. Implementing self-preservation mode infrastructure is a relatively
1686 inexpensive investment that can pay dividends. The majority of District controlled structures already have
1687 backup generators (the most expensive component) and therefore they only need automation components
1688 such as hardened sensors, communication equipment and computer systems added.

1689 Other strategies that the District considers to be related to the self-preservation concept include
1690 maximizing the operation of secondary flood control system, increasing the ability to transfer water between
1691 basins and also optimizing the operation of stormwater treatment areas (STAs) and enhancing automation
1692 so that drawdowns can be avoided when not necessary.

1693 STAs depend on certain hydrologic conditions (water levels) to optimize nutrient removal, because
1694 aquatic plants require a certain water level range to grow and thrive. When the water level in an STA is
1695 kept within the optimal range, the STA can operate most efficiently. Drastic changes in water level can
1696 severely impact the efficiency of an STA and can even cause aquatic vegetation to die, thus turning an STA
1697 into a nutrient source instead of a nutrient sink. Adding remote control and automation to the pump stations
1698 that control water levels in STAs helps to ensure that water levels are kept at their optimal range even when
1699 a power failure occurs at the pump station and avoid unnecessary drawdown operations when storm
1700 prediction is highly uncertain.

1701 Maximizing the operation of secondary flood control system is another way to increase the resiliency
1702 of the C&SF System. For instance, the primary system (C&SF Project) may be operating at maximum
1703 efficiency, but if a secondary water control structure is clogged with debris or has suffered a power outage,
1704 flooding upstream of the secondary structure can occur. The District is committed to partnering with the
1705 entities that operate secondary water control systems to make modifications to the secondary systems that
1706 increase resiliency of the entire flood control system.

1707 Another strategy that is promising for making the C&SF Project more resilient is increasing
1708 connectivity between basins. Having the ability to move water from a flooded basin to an adjacent basin
1709 that can handle additional water could be a very effective tool that does not require discharging to tide.
1710 With increased connectivity between basins, water managers could have powerful additional tools for
1711 operating the system to optimize flood control efforts.

1712 Table 9-7 summarizes the self-preservation actions needed, at each prioritized C&SF structure, and
1713 initial estimated costs to implement additional programming costs, and backup controller instrument and
1714 platform; install backup controller and other automation features; modify gates for added high tide
1715 protection against reverse flow, according to the number of gates in each selected coastal structure; modify
1716 structure by adding seals and additional needs. In FY2023, this project was awarded 100% of funding needs
1717 through FDEP Resilient Florida Program and contract is currently under negotiation.

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1725 **Table 9-7.** Modifications and costs needed to harden coastal structures.

1726

1727 * This option will replace the need for raising the heights

ID	Name	Additional Programming; Storm Resilient Back Up Controller instrument and platform	Install Backup Controller and other automation features	Modify gates for added high tide protection against reverse flow	Modify Structure by adding seals*	Control Panel Upgrades / Hardening
1	S-123 (2)	\$150,000.00		\$100,000.00	\$50,000.00	
2	S-22 (2)	\$150,000.00		\$100,000.00		
3	S-27 (2)	\$150,000.00			*4	
4	S-28 (2)	\$150,000.00			*4	
5	S-21 (3)	\$150,000.00		\$150,000.00	\$75,000.00	
6	S-25 (1)	\$150,000.00		\$50,000.00		
7	S-20 (1)	\$150,000.00		\$50,000.00		
8	S-20F (3)	\$150,000.00		\$150,000.00		
9	S-20G (1)	\$150,000.00		\$50,000.00		
10	S-21A (2)	\$150,000.00		\$100,000.00		
11	S-25B (2)	\$150,000.00		\$100,000.00		
12	S-26 (2)	\$150,000.00		\$100,000.00		
13	S-29 (2)	\$150,000.00			*4	
14	S-197 (4)	\$25,000.00				
15	G-56 (3)	\$150,000.00		\$150,000.00		
16	COCO1		\$175,000.00			
17	GG-1		\$175,000.00			
18	HC1		\$175,000.00			
19	COCO2		\$175,000.00			
20	GG2		\$175,000.00			
21	COCO3		\$175,000.00			
22	GG3		\$175,000.00			
23	S487, S486, S488					\$3,050,000.00
24	G-420					\$600,000.00
25	G-57, S-381					\$300,000.00
26	Manatee Gates*2					\$5,000,000.00
27	S140, S7					\$1,000,000.00
28	S-179*3					\$500,000.00

1728 *2 G-36, S-127, S-131, S-33, G-93, S-123, S-22, S-25, S-25B, S-26, S-27, S-28, S-29, S-20F, S-20G, S-21, S-
1729 21A

1730 *3 Gate Hoist Conversion

1731 *4 Gates modifications are included in the major refurbishment proposals for these Coastal Structures

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1735

1736 **L-8 FEB / G-539 PUMP RESILIENCY UPGRADES**

1737 This resiliency project is mainly tied to the District’s mission to provide flood control and water supply
 1738 protection. The L-8 Flow Equalization Basin (FEB) consists of a 3,000 cubic feet per second (cfs) inflow
 1739 structure and a 450 cfs outflow pump station G-539. The L-8 FEB is located along the L-8 Canal in Palm
 1740 Beach County and receives flows from the C-51 West and S-5A drainage basins that were previously routed
 1741 to STA-1W and STA-1E for treatment prior to discharging into Water Conservation Area 1. The S-5A and
 1742 S-319 Pump Stations continue to provide the existing level of flood protection to the S-5A Basin and the
 1743 C-51 West Basin with the FEB adding an additional 45,000 ac-ft of storage capacity that reduces flows to
 1744 tide during storm events or sending water south when the system is at capacity by attenuating peak flows.
 1745 This project includes the refurbishment of a regionally significant asset, the G-539 pump and the L-8 FEB,
 1746 to reduce the impacts of flooding and SLR throughout the C-51 and S-5A drainage basins, by enhancing
 1747 the pump operation that will attenuate peak flows o tide during storm events, providing stormwater
 1748 management to areas beyond a single municipality boundary. This project replaces the six existing electrical
 1749 submersible pumps configured in 2 pumping stages to reduce the total static head on each pump.
 1750 Replacement pumps will ensure the reliability and resiliency for flood protection and flood attenuation.

1751 This project will enhance the reliability of G-539 pump, resulting in reduced flood risks and increased
 1752 water management flexibility. The project consists of replacement of six existing electrical submersible
 1753 pumps configured in two pumping stages (total static head reduction). The L-8 FEB receives flows from
 1754 C-51 West and S-5A drainage basins and adds 45,000 ac-ft of storage capacity that reduces flows to tide
 1755 during storm events or sends water south when the system is at capacity which allows for peak flows
 1756 attenuation benefits. Self-Preservation Mode will also be implanted so that the control room will be able to
 1757 monitor each engine of the pump station. Replacement pumps will ensure the reliability and resiliency for
 1758 flood protection. Water supply protection benefits are also expected through operation of C-51 reservoir.

1759 Current efforts from the Flood Protection Level of Service Program (FPLOS) to develop a
 1760 comprehensive assessment and understand frequency and severity of flooding in the project impact area, in
 1761 Palm Beach County, for current and future scenarios, is undergoing. Extreme rainfall events (i.e., Irma,
 1762 September 2017; May 2020 Storm; Tropical Storm Eta, November 2020) have caused flooding conditions
 1763 of different magnitude across Palm Beach County, and flood reports display different degrees of severity,
 1764 from ankle deep flooding to 2 feet. The L8 FEB G539 Pump project is key to improve flood attenuation
 1765 and help reducing the vulnerability of communities in the C-51 East and C-51 West Basins. In FY2023,
 1766 this project was awarded 100% of funding needs through FDEP Resilient Florida Program and contract is
 1767 currently under negotiation.

1768

1769 **L-8 FEB / G-539 Pump Resiliency Upgrades Cost Estimate**

L-8 FEB / G-539 Pump Resiliency Upgrades	\$8,000,000
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1770

1771 **HARDENING OF S-2, S-3, S-4, S-7, S-8 ENGINE CONTROL PANELS –**
 1772 **BUILDING RESILIENCY IN WATER MANAGEMENT SOUTH OF LAKE**
 1773 **OKEECHOBEE**

1774 The S2, S3, S7 and S8 pump stations were built in the 1950s and S4 was built in 1975. The purpose of
 1775 the S2, S3 and S4 structures is to pump water into Lake Okeechobee via the Hillsboro and NNR Canals,
 1776 the Miami Canal, and L-D1, C-20, C-21 and Industrial Canals, respectively, from the agricultural area south
 1777 of the structure. The S7 and S8 provide a hydraulic gradient for discharges from STA-3/4.

1778 The pump engine monitoring panels and equipment at these pump stations are at the end of their useful
 1779 service life, limiting the capacity of the pump station operator from taking critical actions necessary to
 1780 prevent failure of a pump engine. Replacement parts for the existing monitoring equipment / control panel
 1781 are not available. The District routinely performs inspection reports to assess the immediate enhancement
 1782 needs. This project is one of the priority needs established to increase resiliency of water resources in this
 1783 region.

1784 Failure of S2, S3, S4, S7 and S8 structures to pump water exceedances to Lake Okeechobee will result
 1785 in cascading effects downstream, such as the increase the water levels in canals, reduction in infiltration
 1786 capacity, wet antecedent conditions in watersheds and higher water tables that are likely to increase flooding
 1787 conditions in urban areas in Palm Beach and Broward Counties. Floodwaters are likely to propagate across
 1788 the agricultural areas towards WCA 2A or 3A, ultimately reaching the C11 and C9 urbanized areas or the
 1789 Everglades National Park.

1790 With the goal of increasing flood resiliency within its impact area, this proposed project is to replace
 1791 all engine control panels in these five pump stations with modern and standardized equipment and to install
 1792 equipment to implement new emergency shutdown features. These pump stations are critical features of
 1793 the stormwater infrastructure and need to be upgraded. The pump engine needs enhancements to reduce
 1794 flooding risks and increase water management flexibility. The engine control panel updates will improve
 1795 the efficiency and reliability of these structures. Finally, this project will reduce risk of compound flooding
 1796 across Palm Beach and down South in Broward County

1797 In FY2023, this project was awarded 100% of funding needs through FDEP Resilient Florida Program
 1798 and contract is currently under negotiation.

1799

1800 **Hardening Of S-2, S-3, S-4, S-7, S-8 Engine Control Panels – Building**
 1801 **Resiliency in Water Management South of Lake Okeechobee Cost Estimate**

Hardening Of S-2, S-3, S-4, S-7, S-8 Engine Control Panels – Building Resiliency in Water Management South of Lake Okeechobee	\$17,000,000
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1802

1803

1804 **JW CORBETT WILDLIFE MANAGEMENT AREA HYDROLOGIC**
 1805 **RESTORATION AND LEVEE RESILIENCY**

1806 **Background**



This resiliency project is mainly tied to the District's mission to provide flood control, water supply protection, and ecosystem restoration. In August of 2012, Tropical Storm Isaac brought unprecedented rainfall to areas of central Palm Beach County resulting in widespread flooding in the area. As part of the State's response to the Storm, the Indian Trail Improvement District's (ITID) Corbett Levee was identified as an area of critical concern for berm failure due to localized slope failures, excessive seepage, and the formation of boils (seepage pathways). In September 2012, the SFWMD was

1819 directed by the Governor's Office to immediately convene a multi-agency working group to develop a plan
 1820 for strengthening the Corbett Levee to meet current USACE and South Florida Water Management District
 1821 standards and to increase the level of flood protection in the area for over 40,000 residents. The project was
 1822 designed and constructed by the District following the latest engineering and construction technologies.
 1823 The first phase of the project included strengthening and upgrading 2.6 miles of levee along the north side
 1824 of ITID starting east of the ITID Reservoir. However, the remaining eastern levee section of 3.7 miles has
 1825 not been constructed due to lack of funding. Therefore, the project is currently not meeting its full flood
 1826 protection and habitat enhancement potential.

1827 **Corbett Wildlife Management Area**

1828 Corbett Wildlife Management Area (Corbett WMA), upstream of the Levee, consists of approximately
 1829 60,000 acres of cypress swamp, pine flatwoods, sawgrass marsh, and hardwood hammocks adjacent to the
 1830 L-8 canal and upstream of the C-51 canal. The Corbett WMA is home many wildlife species, including
 1831 deer, turkey, and feral hogs that draw hunters as well as threatened and endangered species like the red-
 1832 cockaded woodpecker, Everglade snail kite, gopher tortoise, and indigo snake. Other notable species that
 1833 are frequently encountered include bobcat, sandhill crane and numerous wading birds and waterfowl.

1834 The Corbett WMA has been held at artificially low water levels for years, resulting in fish and wildlife
 1835 habitat loss. Additionally, holding water levels at lower elevations requires increased discharge of
 1836 stormwater into the regional system, thereby diminishing the capacity for flood control in areas adjacent to
 1837 and downstream of the Corbett WMA. Completion of construction of the Corbett Levee would allow water
 1838 managers to restore a more natural hydroperiod and therefore improve wildlife habitat within the Corbett
 1839 WMA while simultaneously increasing the resilience, storage capacity and functionality of the flood control
 1840 system. This is particularly beneficial to create wildlife corridors and habitat connectivity within the C-18
 1841 Basin and nearby areas close to lake Okeechobee.

1842 **Loxahatchee River Watershed Restoration Project**

1843 The Loxahatchee River Watershed Restoration Project (LRWRP) will restore 10,000 acres of existing
 1844 disturbed wetlands in the J.W. Corbett Wildlife Management Area (WMA), Loxahatchee Slough, Pal-Mar
 1845 East, Cypress Creek Natural Area and Kitching Creek. Specifically, the LRWRP will restore 1,642 acres
 1846 of wetlands within the J.W. Corbett WMA.

1847 Completion of the Corbett Levee will provide flood protection to adjacent residential communities and
 1848 ecological benefits that are consistent with the planning objectives of the LRWRP. The planning objectives

1849 include restoring water flows to the National Wild and Scenic Northwest Fork of the Loxahatchee River,
 1850 increasing the natural area extent of wetlands within the watershed, restoring connections between natural
 1851 areas to improve hydrology and natural storage, and restoring native plant and animal abundance and
 1852 diversity within the natural areas of the Loxahatchee River Watershed.

1853 The Corbett Levee will retain additional freshwater within the J.W. Corbett WMA that can be used to
 1854 supplement the C-18W Reservoir and ASR well system to provide additional flow to the Loxahatchee
 1855 River. The Corbett Levee will also enhance storage capacity in J.W. Corbett WMA, which will improve
 1856 hydroperiods for wetland communities. An improved hydroperiod will benefit wetland habitat and function,
 1857 which further strengthens the connectivity between adjacent natural areas within the LRWRP.

1858 **Flood Protection**

1859 In addition, the completion of this project will address excess flooding due to the impacts of climate
 1860 change such as an increase in the number and intensity of tropical cyclones. The urban areas adjacent to the
 1861 Corbett Levee highly rely on the ability of the inner canal system to drain water to the M-O canal. Flooding
 1862 conditions as a result of channel overbank flow diminish the drainage capacity of the system, exacerbating
 1863 flood inundation depth and extent across the basin. For instance, rainfall impacts from Tropical Storm Isaac
 1864 were well beyond the design capacity of the berm that existed prior to the construction of the Corbett Levee.
 1865 Finishing this project would increase the District’s operational flexibility and therefore improve the
 1866 system’s resiliency to flooding.

1867 The proposed final section of levee is approximately three miles long. In addition, the project proposes
 1868 the concurrent construction of a 0.6 N/S levee portion, that is part of the CERP Loxahatchee Project - C18-
 1869 W Impoundment Project (L-101W, 0.6-mile segment from the east end of ITID’s M-O Canal to 100th Ln
 1870 North) to allow full operational change to JW Corbett WMA. Total project costs below include the 0.6-
 1871 mile segment, which will be built as a separate project. Without the north south segment the operational
 1872 changes to Southeast JW Corbett WMA will be limited. IN FY2023, Palm Beach County was awarded
 1873 100% of funding needs through FDEP Resilient Florida Program and the contract is currently under
 1874 negotiation, including an interagency agreement with the District for the construction of the project.

1875 **Bahiagrass Pilot Study**

1876 Landscape turf represents a major draw on Florida’s water resources, and it requires intensive
 1877 maintenance such as mowing and fertilization. Bahiagrass requires very little supplemental irrigation and
 1878 fertilization. This proposed pilot study would be located on the Corbett Levee. The goals of the study are:

- 1879 • Retain the persistence and resilient nature of bahiagrass.
- 1880 • Improve color and density of bahiagrass to increase its utilization in landscapes and therefore
- 1881 reduce the need for fertilization and irrigation.
- 1882 • Increased seed yield during fewer months of the year to increase seed production and reduce the
- 1883 price of seed.
- 1884 • Reduce the rate of leaf elongation to reduce the need for mowing.
- 1885 • Produce seed heads only in June, July, and August to concentrate seed production times and reduce
- 1886 the need for mowing.

1887 To accomplish these goals, both traditional methods of plant breeding and more advanced genetic
 1888 technologies/gene editing would be used.

1889 **Corbett WMA Hydrologic Restoration and Levee Resiliency Cost Estimate**

JW Corbett Wildlife Management Area Hydrologic Restoration and Levee Resiliency	\$13,000,000
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1890

1891 **C-29, C-29A, C-29B AND C-29C CANAL CONVEYANCE IMPROVEMENT**

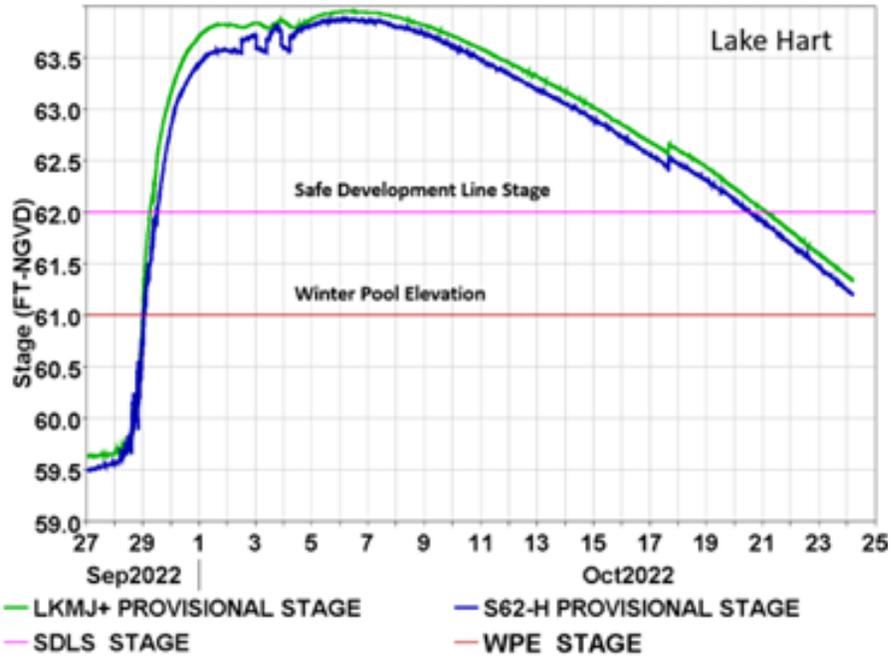
1892 This resiliency project is mainly linked to the District’s mission to provide flood control. The C-29, C-
 1893 29A, C-29B and C-29C Canals are part of the Lake Hart basin in Orange and Osceola counties. The C-29
 1894 canal is 1.1 miles long and connects Lake Hart with Lake Mary Jane. The direction of flow in the C-29
 1895 canal is generally from Lake Mary Jane to Lake Hart. C-29A canal which is 1.5 miles long connects Lake
 1896 Hart with the
 1897 downstream
 1898 Ajay Lake, and
 1899 the C-29B
 1900 canal connects
 1901 Ajay Lake with
 1902 Fells Cove,
 1903 and the C-29C
 1904 canal connects
 1905 Fells Cove
 1906 with the
 1907 downstream
 1908 East Lake
 1909 Tohopekaliga.

1910 The S-62
 1911 structure in the
 1912 C-29A canal at
 1913 the outlet of
 1914 Lake Hart,
 1915 regulates the
 1916 lakes Hart and
 1917 Mary Jane. The
 1918 regulation
 1919 schedule
 1920 ranges



1921 between 59.5 ft and 61.0 ft. NGVD, and the design discharge of the structure is 450-640 cfs. Lake Ajay,
 1922 Fells Cove and East Lake Tohopekaliga are regulated by the S-59 structure located in the C-31 canal at the
 1923 outlet of Lake Tohopekaliga. The lakes are maintained between 54.5 and 59.0 ft. NGVD. As a result of the
 1924 heavy Hurricane Ian heavy rainfalls, equivalent to more than 200-year recurrence frequency for the region,
 1925 water levels at Lake Mary, Lake Hart and Ajay Lake stayed above the safe development line stages for
 1926 approximately 20 days, as illustrated above, showing Lake Hart Stages. A total of 75 cfs of temporary
 1927 pumping capacity was operated at Lake Hart during Hurricane Ian response.

1928 As part of response actions, it is recognized that canal conveyance capacity needs to be closely
 1929 reassessed and appropriate mitigation measures need to be developed. Overall recommended strategies
 1930 include widening, deepening the canal, and/or elevating the canal banks and providing appropriate canal
 1931 benches and berms. The currently proposed measures for improving conveyance at C-29, C29-A, C29-B
 1932 and C29-C canal include dredging the canal for deepening and widening, adhering to the 1:3 slope, up to
 1933 the existing extension of District’s right of way. Canal bank stabilization is not included in this initial project
 1934 recommendation and respective cost estimates. Canal bank stabilization will be done in a future phase of
 1935 this project, with an estimated cost up to \$5M per mile.



1936
1937 **Figure 9-20.** Lake Hart Water Stages resulting from Hurricane Ian heavy rainfall event.

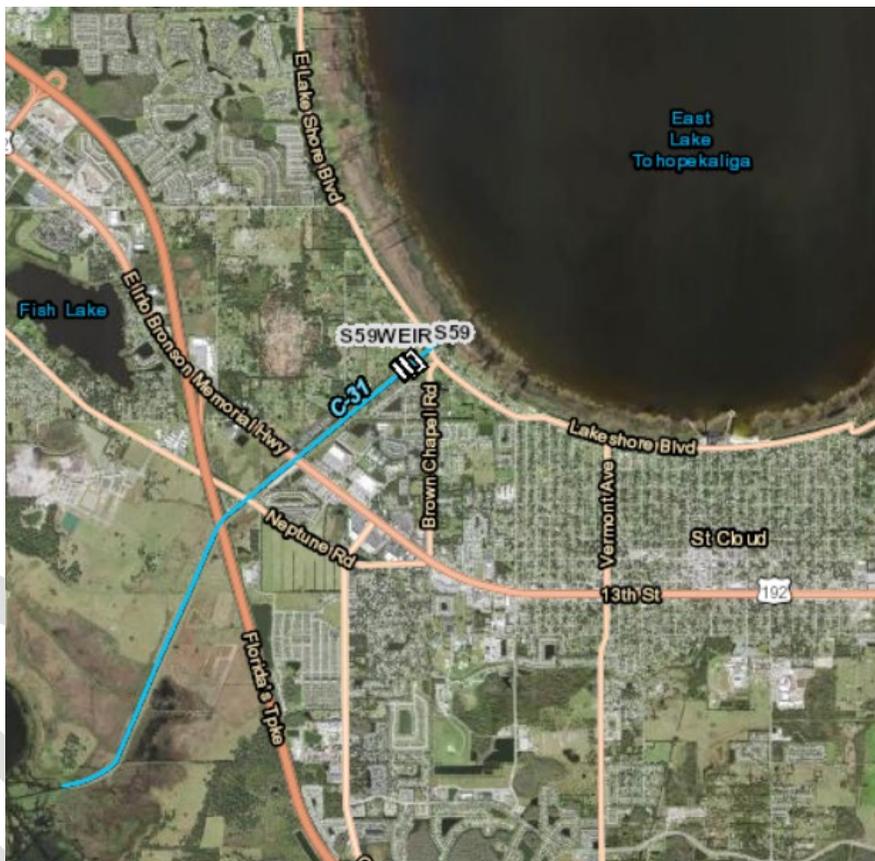
1938 **C-29, C-29A, C-29B AND C-29C Canal Conveyance - Cost Estimate**

C-29 Dredging (0.5 miles widening and deepening)	\$ \$1,279,270
C-29A Dredging (1.41 miles widening and deepening)	\$ 3,249,152
C-29B Dredging (1.06 miles widening and deepening)	\$ 2,499,975
C-29C Dredging (0.77 miles widening and deepening)	\$ 1,851,267
Total Construction Cost	\$ 8,879,664

1939

1940 **S-59 STRUCTURE ENHANCEMENT AND C-31 CANAL CONVEYANCE** 1941 **IMPROVEMENTS**

1942 This resiliency project is mainly tied to the District’s mission to provide flood control. The S-59
1943 structure is a gated spillway on the C-31 canal at the outlet of East Lake Tohopekaliga in Osceola County
1944 in the Upper Kissimmee Chain of Lakes. The structure can be remotely operated from the SFWMD
1945 Operations control center.
1946 The structure has a design
1947 capacity of 590-820 cfs and
1948 is operated to maintain
1949 optimum stages in the
1950 upstream C-31 Canal and in
1951 East Lake Tohopekaliga.
1952 The structure is operated in
1953 accordance with USACE
1954 Master Water Control
1955 Manual for Upper and lower
1956 Kissimmee basins, focusing
1957 on the East Lake
1958 Tohopekaliga Regulation
1959 Schedule which ranges
1960 between 55.0-58.0 ft.
1961 NGVD. The C-31 canal is
1962 3.9 miles long and connects
1963 East Lake Tohopekaliga to
1964 the downstream Lake
1965 Tohopekaliga to the south.
1966 The C-31 canal design
1967 elevations are 52.0-55.0 ft.
1968 NGVD. The two major
1969 sources of inflow to Lake
1970 Tohopekaliga are Shingle
1971 Creek and C-31 Canal.



1972 As a result of Hurricane 2022 Ian’s heavy rainfall, equivalent to more than 200-year recurrence
1973 frequency for the region, water levels at East Lake Toho stayed above the safe development line stage of
1974 59 ft. NGVD for approximately 25 days. During Hurricane Ian, temporary pumps were deployed to
1975 facilitate the conveyance between East Lake Toho and Lake Toho for the period of 10/01/22 to 10/31/22
1976 with daily flow rates as high as 290 cfs.

1977 As part of response actions, it is recognized that this structure needs to be upgraded to include an
1978 additional gate to address the single-gate vulnerability issue, along with an improved erosion protective
1979 measure that would not constrain the capacity at this structure and canal conveyance improvements. The
1980 currently proposed measures include removing existing structure and adding 2 (two) gated spillways and
1981 enhancement of the sheet pile weir with a more robust stilling basin with flow deflector and associated rip
1982 rap. Such design would remove major structure capacity limitations and potentially can result in a structure
1983 that has no maximum Allowable Gate Openings (MAGOs) constraints. Additionally, conveyance
1984 improvement along the C-31 conveyance is being proposed, especially as C-31 enters Goblet Cove in West
1985 Lake Toho and include canal dredging (deepening) and riprap augmentation. The Osceola Parkway
1986 expansion project includes widening of the Partin Settlement Rd near C-31 Canal, and Coordination with
1987 FDOT is recommended.

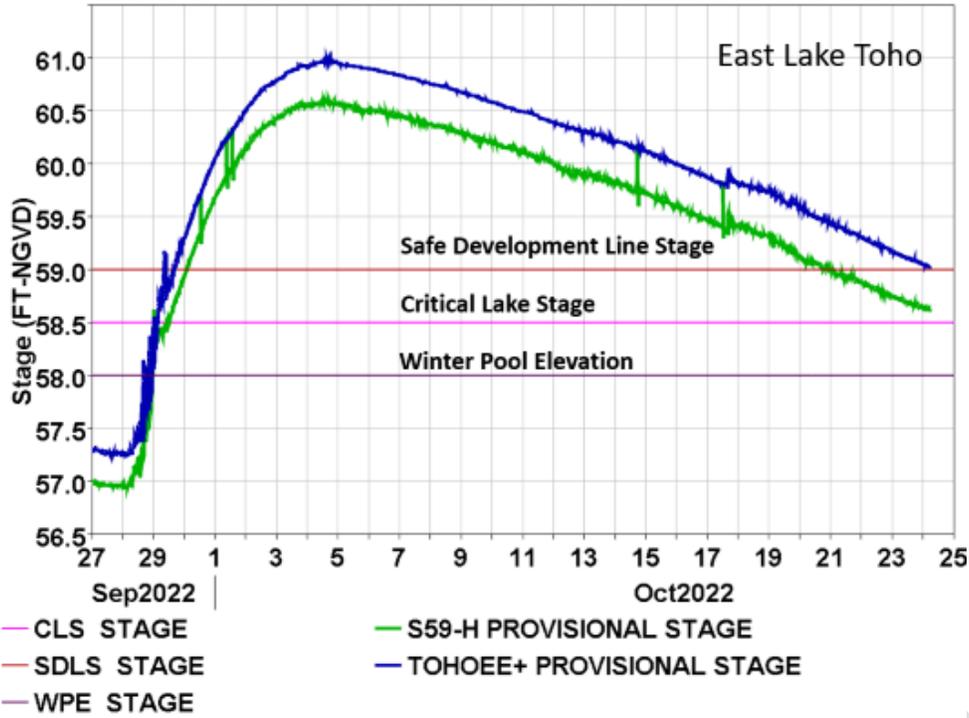


Figure 9-21. East Lake Toho Water Stages resulting from Hurricane Ian heavy rainfall event.

1988
1989
1990
1991

Erosion Control at S-59 and C-31 Conveyance Improvements Cost Estimate

Demolish old Structure and Build a New Spillway	\$23,731,532
S-59 Electrical Work	\$743,497
C-31 Canal Widen, Including Rip Rap Work	\$ 8,412,576
Total Construction Cost	\$32,887,605
Total Construction Cost	\$39,308,208

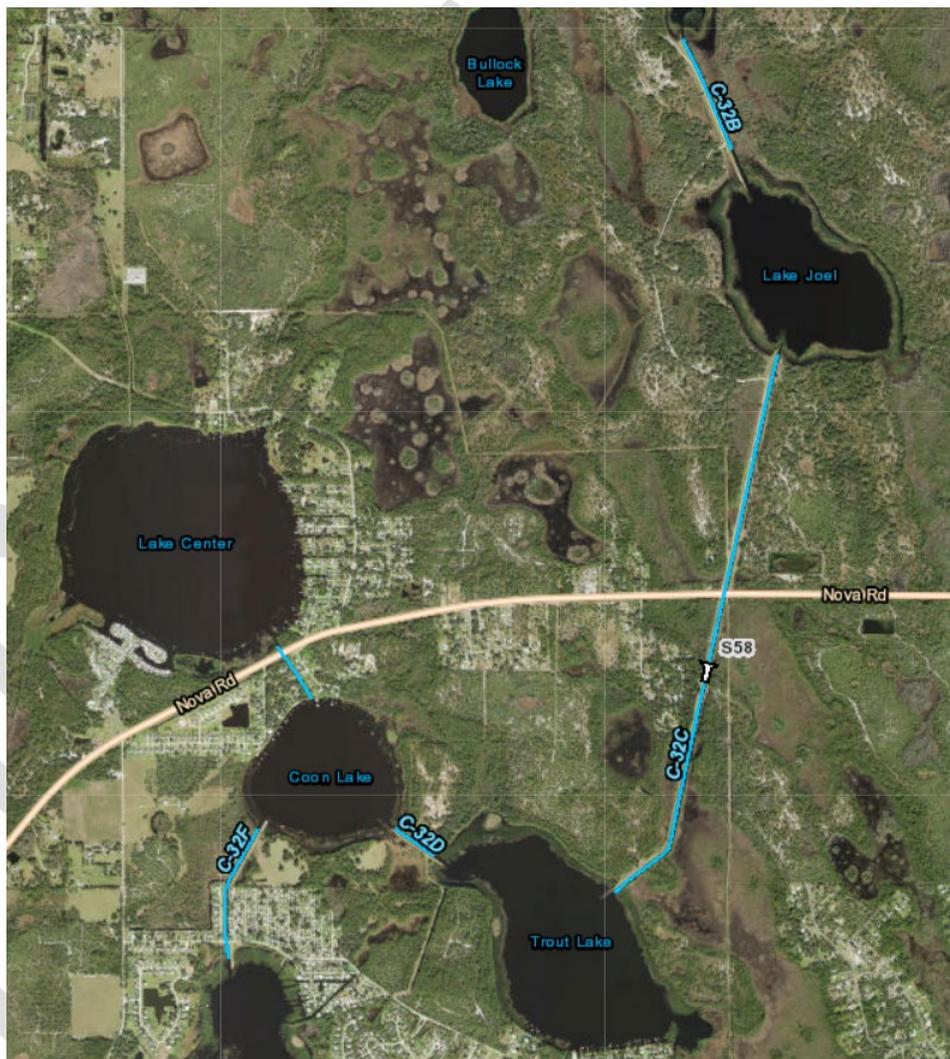
1992
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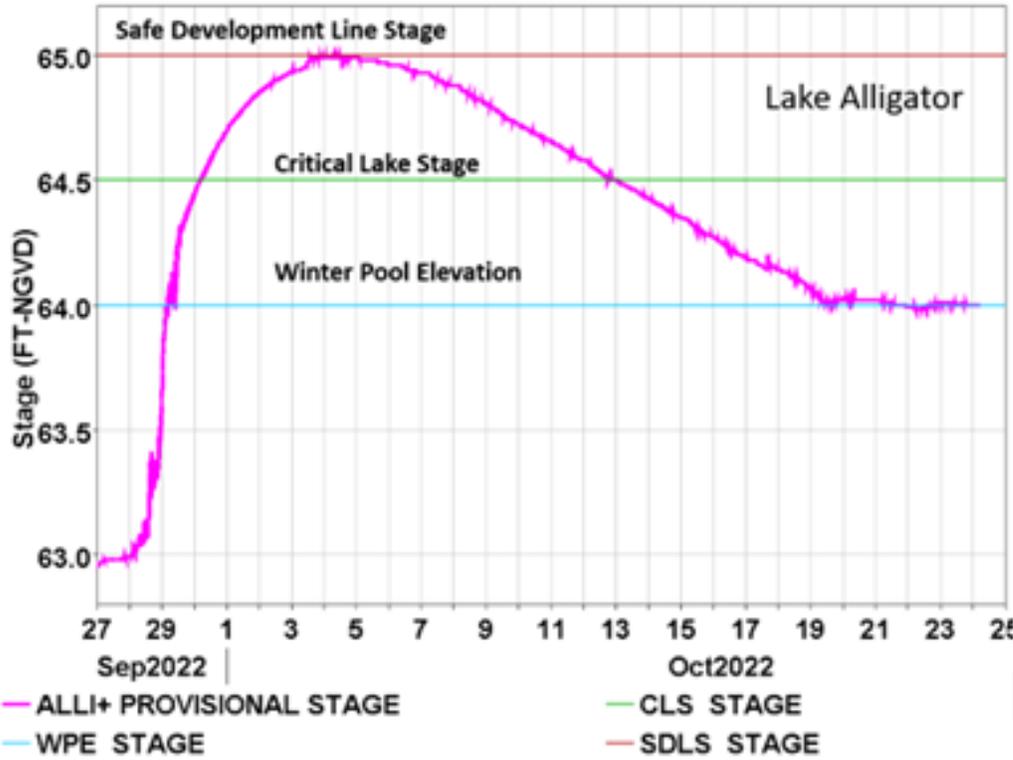
1994 **S-58 STRUCTURE ENHANCEMENT AND TEMPORARY PUMP**

1995 This resiliency project is mainly tied to the District’s mission to provide flood control. The S-58 culvert
 1996 structure with two barrels is located in Osceola County on the C-32C canal, 3700 ft downstream from Lake
 1997 Trout connects Lakes Trout and Joel. Flow is south to north in the C-32C canal, and the structure maintains
 1998 stages in the range 62.0 – 64.0 ft. NGVD in accordance with the Lake Alligator Regulation schedule. The
 1999 structure which has a design discharge of 160 cfs was originally designed to pass sufficient discharge during
 2000 dry periods to maintain downstream stages and water supply demands. S-58 Structure is currently the only
 2001 structure in main canals in
 2002 this region that does not
 2003 have the ability for remote
 2004 operation.

2005 As a result of
 2006 Hurricane Ian’s heavy
 2007 rainfall, equivalent to
 2008 more than 200-year
 2009 recurrence frequency for
 2010 the region, water levels at
 2011 Alligator Lake stayed near
 2012 the safe development line
 2013 stage of 65 ft. NGVD for
 2014 approximately 3 days.
 2015 During Hurricane Ian,
 2016 temporary pumps were
 2017 deployed to facilitate the
 2018 discharge to Alligator
 2019 Lake for the period of
 2020 10/01/22 to 10/12/22 with
 2021 daily flow rates as high as
 2022 316 cfs.

2023 As part of response
 2024 actions, it is recognized
 2025 that this structure needs to
 2026 be upgraded along with
 2027 the need to augment the S-
 2028 58 structure with a pad for
 2029 a temporary pump station
 2030 to alleviate flood
 2031 conditions between Lakes
 2032 Myrtle and Alligator. The
 2033 region is under intense land development and rapidly growing population that need to be provided with
 2034 compatible flood control and operation capacity. The currently proposed measures include removing the
 2035 existing structure and adding 2 (two) gated spillways with fully remote operation capability, along with
 2036 permanent installation of pump platforms to make temporary pump deployment quicker/easier and purchase
 2037 of two-way temporary pump(s) to have on hand for deployment. Pump capacity should take into
 2038 consideration canal limitations downstream, as C-32 Canal might not be able to handle more than 250cfs.
 2039 Platform should be constructed in a way that allow pump deployment from both direction.





2040
2041
2042 **Figure 9-22.** Lake Alligator Water Stages resulting from Hurricane Ian heavy rainfall event.

2043 **S-58 Structure Enhancement Cost Estimate**

Removal of the existing structure	\$4,568,189
Addition of 2 (two) gated spillways with fully remote operation capability	\$31,346,062
Purchase of two-way temporary pump(s) and permanent installation of pump platforms	\$6,631,180
Total Project Cost	\$42,545,431

2044

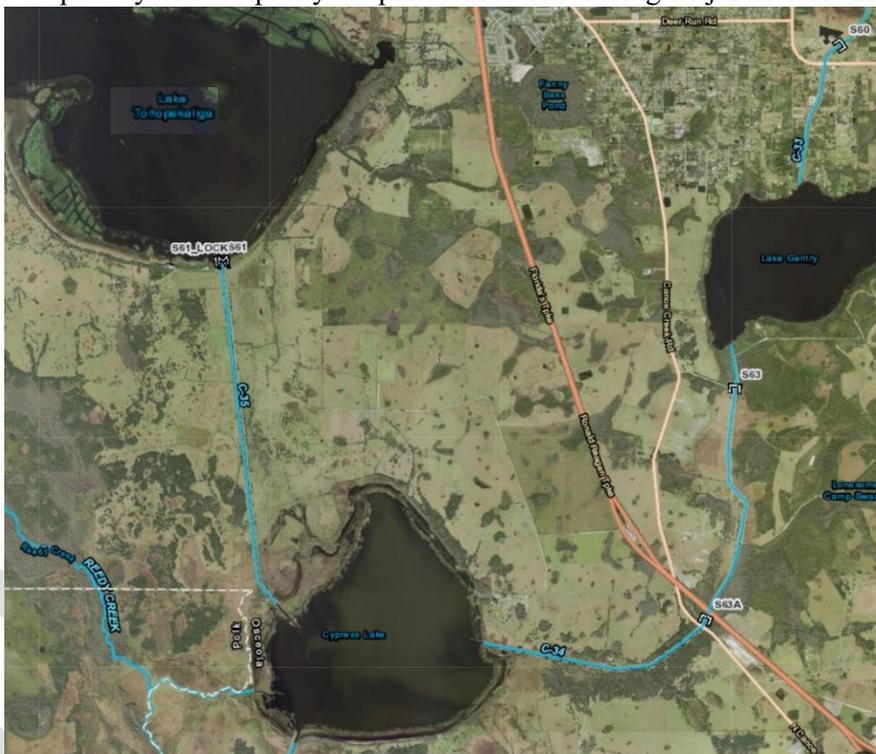
2045 **S-61 SPILLWAY ENHANCEMENT AND EROSION CONTROL**

2046 This resiliency project is linked to the District’s mission to provide flood control, The S-61 lock is 90
 2047 feet by 30 feet with two pairs of gates and permits passage of vessels between the Lake Tohopekaliga and
 2048 other canals/lake downstream all the way to Kissimmee River. It is operated for flood control when Lake
 2049 Toho stage exceeds 48.5 ft NGVD. The S-61 lock was not designed for flood control purposes; however, it
 2050 is used to supplement the S-61 spillway flow capacity to pass floodwater during major storms and
 2051 emergency response. This is
 2052 a delicate operation that
 2053 must be closely monitored
 2054 and appropriately
 2055 coordinated with the US
 2056 Army Corps of Engineers.

2057 In 2017, during and after
 2058 Hurricane Irma (when the
 2059 lock was used for flood
 2060 control operations), the
 2061 scour hole downstream of
 2062 this lock increased to 7-feet.
 2063 Further erosion damage was
 2064 observed during emergency
 2065 response operations from
 2066 Hurricane Ian.

2067 As part of response
 2068 actions, it is recognized that
 2069 this navigational lock needs
 2070 to be augmented with the
 2071 enhancement of S-61
 2072 Spillway to handle flood
 2073 control operations during emergency events, as well as to continue serving navigation purposes. The
 2074 currently proposed measures include construction of two new gated spillway to allow for improved
 2075 conveyance/discharge capacity. After completion of the new spillway, demolition of the existing spillway
 2076 will be performed and rebuild the peninsula. Canal enhancement will allow for flow to be directed to the
 2077 new structure, along with proper erosion control measures, sloped rip rap on the south side of the structure.

2078 Additionally, the area downstream of the 1 S-61 Lock needs to be redesigned and repaired with
 2079 appropriate erosion protection measures.



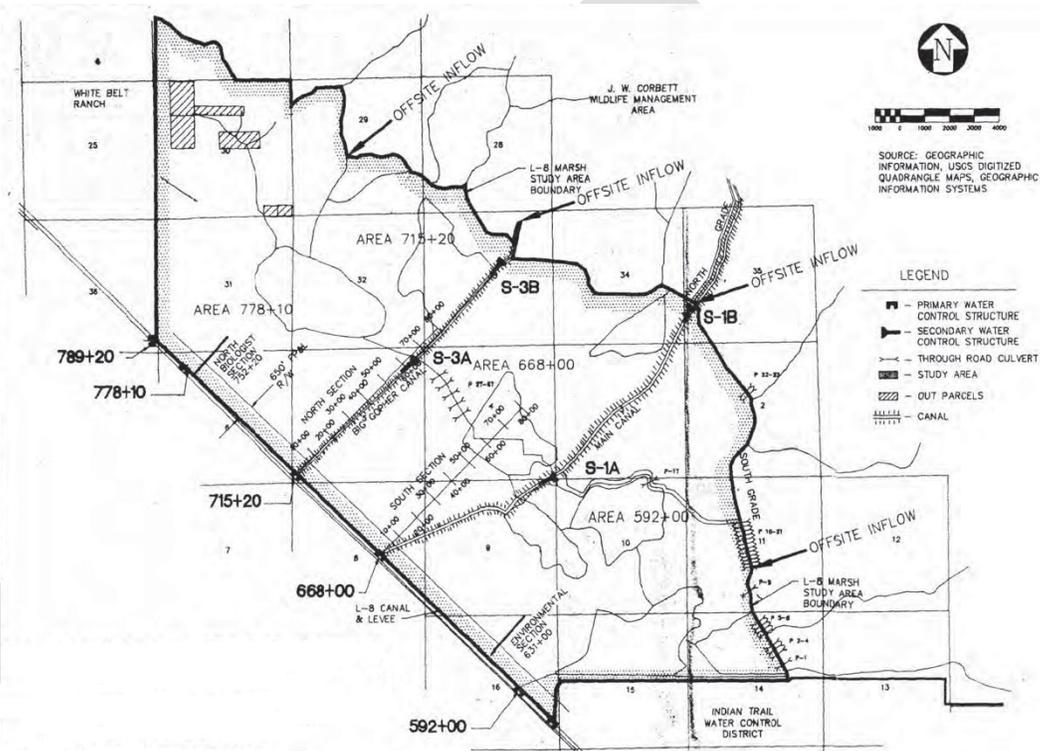
2080 **S-61 Spillway Enhancement Cost Estimate**

Existing S-61 Demolition and Removal	\$4,568,189
New S-61 Two (2) Gated Spillway, including Canal Excavation	\$31,346,062
Repairing The Scour Hole in S-61 Boat Locks	\$4,113,361
Total Project Cost	\$40,027,611

2081

2082 **CORBETT LEVEE WATER CONTROL STRUCTURES**

2083 This resiliency project is mainly tied to the District’s mission to provide flood control and ecosystem
 2084 restoration. Several existing culverts that pass through the L-8 Levee are currently owned, operated, and
 2085 maintained by Florida Fish and Wildlife Conservation Commission (FWC) that could create a flood risk if
 2086 failure were to occur. During Hurricane Ian a partial failure of one of these structures occurred requiring
 2087 emergency response to block the free flow of water from the adjacent property through the damaged culvert
 2088 into the L-8. This temporary protective measure provides an earthen berm around the structure to block
 2089 water from entering the L-8. The remaining culverts owned by FWC were also exhibiting failure modes
 2090 with depressions in the levee crown adjacent to the structure and the initiation of failure in the sandbag
 2091 wingwalls.



2092 Therefore, it no longer allows normal discharge into the L-8. This could have a negative impact on the
 2093 environment due to excessive stages in the adjacent property but also increases the flood risk by the
 2094 potentially higher stages creating increased pore pressure against the L-8 Levee which could then lead to
 2095 higher seepage and ultimately potential for a breach of the Levee if backward erosion piping were to occur.
 2096 The replacement of these culverts is critical to resume normal operations and reduce these flood risks. As
 2097 the entity responsible for maintenance of the L-8 levee it is beneficial for SFWMD to replace these and the
 2098 other similar structures to protect the levee and manage the appropriate stages with controlled discharges
 2099 into the L-8. SFWMD is currently taking over ownership, maintenance and operational responsibilities
 2100 which would warrant the replacement water control structures be designed to the District current standards
 2101 which meet the minimum life expectancies of 75-100 years rather than structures which may require
 2102 replacement at 25–30-year intervals.

2104
 2105
 2106

2107



Note that several of these structures had originally been installed as small spillways during the construction of the L-8 but were replaced by the FWC culverts when it was identified that higher stages upstream were desired to provide environmental benefits. Returning these to the responsibility of SFWMD will continue to provide the intended environmental benefit while mitigating risks of flooding that could be caused by failure of the structures. The recommended project includes demolishing the existing ones and replacing the existing culverts with

2123 five new water control structures and associated riprap/erosion control. Each new structure will have a
 2124 conveyance capacity of approximately 600-800 cfs. Additional work will be performed at the 9-mile road,
 2125 using the 60-inch lime rock.

2126 **Corbett Water Control Structures Cost Estimate**

Project Construction Cost for Box Culvert 1	\$3,440,946
Project Construction Cost for Box Culvert 2	\$2,280,743
Project Construction Cost for Box Culvert 3	\$3,440,946
Project Construction Cost for Box Culvert 4	\$3,440,946
Project Construction Cost for Box Culvert 5	\$1,403,153
Construction Cost (9) Miles Road Repair at Corbett Levee	\$3,764,542
Total Project Cost	\$17,771,277

2127

2128 **BIG CYPRESS BASIN MICROWAVE TOWER**

2129 This resiliency project is mainly tied to the District’s mission to provide flood control and water supply
 2130 protection. A new Microwave Tower and Electronic Equipment Shelter will be located in Immokalee,
 2131 Collier County near Lake Trafford. This new tower is required to complete communications for flood
 2132 control operations for the western spur and bring reliability and resiliency to the Big Cypress Basin (BCB)
 2133 area. This important project will help make flood control efforts in the Big Cypress Basin more resilient
 2134 during storms and hurricanes. Currently our communications are through cell phone towers which go offline
 2135 during storm events, leaving our system without communications and operations.

2136 **Cost Estimate**

Microwave Tower construction	\$7,400,000
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2137 **L-31E LEVEE IMPROVEMENTS**

2138 This resiliency project is mainly
 2139 tied to the District’s mission to
 2140 provide flood control and water
 2141 supply protection. The proposed
 2142 strategy consists of enhancement of
 2143 the L-31E Levee. Addressing
 2144 coastal structures vulnerability to
 2145 SLR and storm surge is a high
 2146 priority in South Florida. Funding
 2147 will be used to harden L-31E Levee, a
 2148 component of the 72-year-old
 2149 Central and Southern Florida
 2150 Project, to address storm surge risks
 2151 and SLR vulnerability. The L-31E
 2152 Levee is one of the priority projects
 2153 on the District’s CIP list.



2154 Funds are needed to advance resiliency strategies to reduce vulnerability of communities upstream of
 2155 the L-31E Levee. Future modeling efforts will determine additional resiliency needs at other levee
 2156 structures, based on the determination of what cross sectional change that a vulnerable levee would need to
 2157 provide more protection from storm surge and SLR.

2158 **L-31E Levee Storm Surge Study**

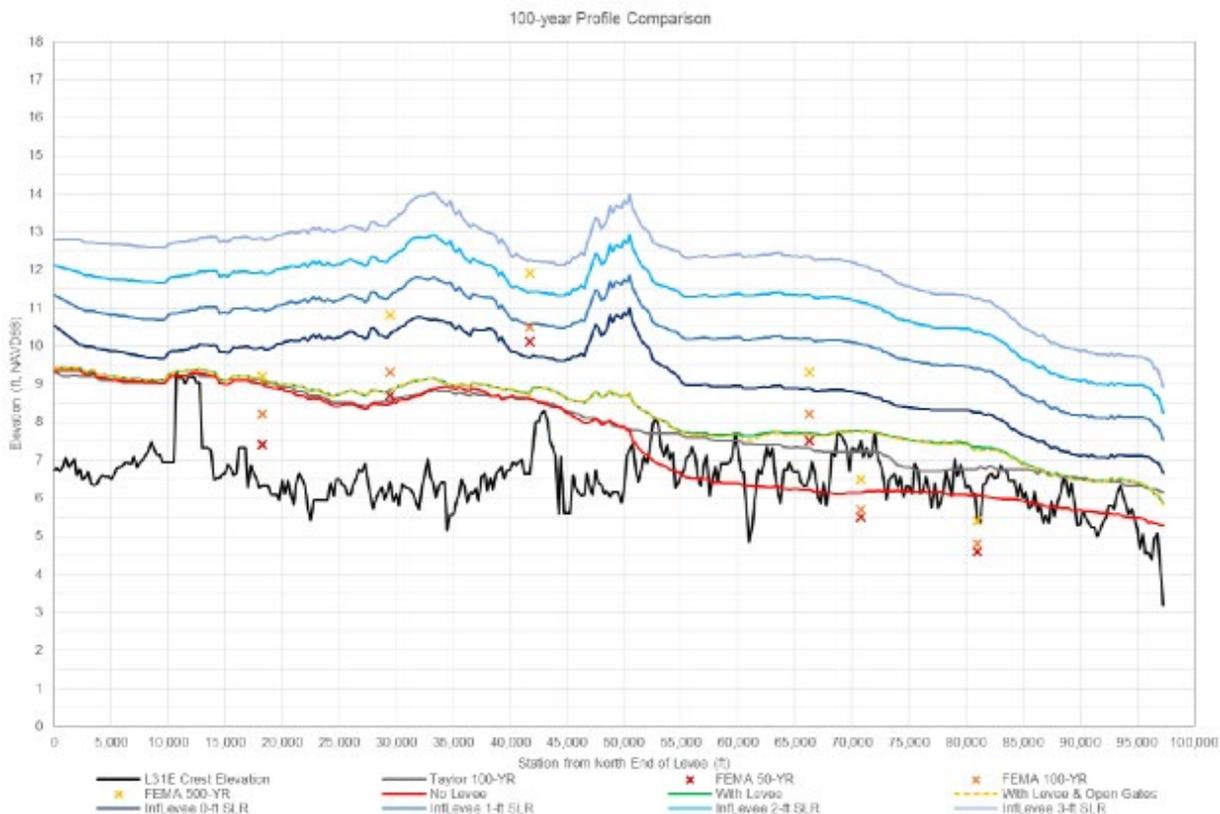
2159 A storm surge study was performed on the L-31E Levee to determine the level of resiliency of the levee
 2160 as it currently exists as well as to determine the levee crest elevation required to effectively counteract SLR
 2161 and storm surge. The study was performed using a combination of ADCRIC/SWAN and Delft3D models
 2162 of Biscayne Bay, information from previous studies, and using the FEMA/Taylor Engineering study of 391
 2163 synthetic storms. The L-31E Levee has six concrete spillway structures and twelve culverts. The following
 2164 modeling scenarios were run as part of the storm surge study:

- 2165 • No Levee and Present-day sea level
- 2166 • Existing Levee Crest with open gates and present-day sea level
- 2167 • Existing levee crest with closed gates and present-day sea level
- 2168 • Non-overtopping levee with closed gates and present-day sea level
- 2169 • Non-overtopping levee with closed gates and Sea Level Rise (SLR) + 1 foot

- 2170 • Non-overtopping levee with closed gates and Sea Level Rise (SLR) + 2 foot
2171 • Non-overtopping levee with closed gates and Sea Level Rise (SLR) + 3 foot
2172 The study recommendations are summarized as follows:

- 2173 1) Start planning and define goals for the levee, integrated with additional efforts being advanced in
2174 the region, including:
2175 a. Return period, time horizon, sea level.
2176 2) Start design considerations using the following:
2177 a. 100-year surge elevation
2178 b. Non-overtopping levee simulation
2179 c. Present-day and Future sea level scenarios, starting at a 2ft increase.
2180 d. Add freeboard according to FEMA and USACE guidance.
2181 3) Gate opening has negligible impact on crest elevation.
2182 4) Edge effects need to be evaluated.
2183 5) Take in consideration wave overtopping, and inland drainage.

2184 The next steps will be to draft a Project Definition Report (PDR) and Work Order Scope of Work
2185 (SOW) to request the design of an increased levee crest elevation to at least four feet along the entire levee
2186 based on the chart in Figure 9-23. The 100-year return period will be the target plus an additional two feet
2187 per FEMA to get the levee certified. The current FEMA maps underpredict surge because the L-31E levee
2188 was neglected: the L-31E Levee adds approximately two feet to the 25-year surge and more than one foot
2189 to the 100-year surge. The L-31E Levee as-builts suggest that the levee was built with an average crest
2190 elevation of 7.5ft NGVD 29. We are proposing to raise the levee two feet from current average elevation
2191 and another two feet per FEMA requirements above the 100-year return period. A rough estimate projected
2192 that approximately between \$39M to \$45M will achieve this design goal. Final design plans will provide
2193 the final recommended elevation, which might differ from the recent Study recommendation, as well as
2194 additional project features. A PDR will be developed with collaboration between the Engineering and
2195 Construction Bureau and the Resiliency Team to determine the most effective scope of work to bring the
2196 levee to a robust resiliency level for future generations. The remaining studies and the design of the levee
2197 crest elevation will be performed by a consultant.



2198

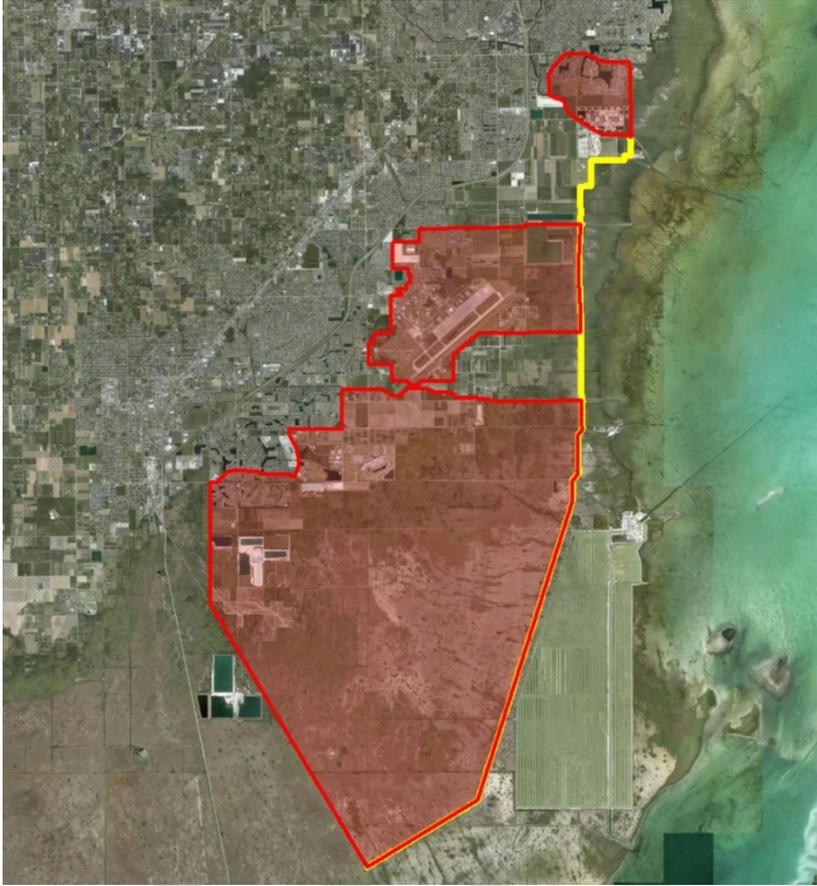
2199 **Figure 9-23.** 100-Year Profile for Levee Crest Elevation Consideration.

2200

2201

2202 **Areas of Influence**

2203 The area of influence on the south and west side of the levee is agricultural land that will need protection
 2204 during storm surge and SLR. Going north along the levee, the Homestead Air Reserve Base is an area of
 2205 influence that will need protection during storm surge and SLR. Further North is a mostly residential area,
 2206 and they also will need protection, however, in that area of influence the impact will be major when it comes
 2207 to raising the levee crest elevation as the levee elevation coincides with the actual road. One possible
 2208 solution might be to decommission two to four miles of the levee in that area. These areas of influence are
 2209 depicted with the red diamonds in Figure 9-24 below. The following canals will also be affected by the
 2210 levee under SLR: C-103, G95, C102 and C-1 since they drain the inland areas west of the levee. All these
 2211 areas of influence will need to be examined closely in the additional modeling that will need to be performed
 2212 to successfully design a levee crest elevation increase.



2213

2214 **Figure 9-24.** Location of L31E Levee (yellow) and area of influence (red).

2215 **L-31 Levee Cost Estimate**

L31E Levee Improvements	\$39M - \$45M
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2216

2217 **DIRECTING COASTAL ECOSYSTEM RESILIENCE PHASE 2: THE** 2218 **EVERGLADES MANGROVE MIGRATION ASSESSMENT (EMMA)**

2219 This resiliency project is mainly tied to the District’s mission to provide flood control, water supply
2220 protection, and ecosystem restoration. EMMA is designed to capture the adaptive foundational resilience
2221 of the coastal wetlands within the SFWMD, with an emphasis on nutrient depleted mangroves. By adaptive
2222 we mean that this resiliency project will demonstrate the ability of coastal wetlands to adapt to rising sea
2223 levels via enhanced soil elevation change. This pilot study will evaluate and implement the ability of coastal
2224 communities to shift to foundational plant communities that are more resilient to higher water depths and
2225 salinities, which in turn, are able to accrete more peat, capture more sediments, sequester more carbon and
2226 keep up with SLR. This is a foundational project because it is focused on the plant communities such as
2227 mangrove swamps and sawgrass plains, that are endemic to the historic and extant ecology of Florida.
2228 Resilience is the ability of the foundational communities to shift rates of productivity, community structure
2229 and spatial extent, in the face of SLR, to minimize wetland conversion to open water habitats and maximize
2230 shoreline retention. EMMA is focused upon the hydrologic attributes needed to enhance, restore and
2231 preserve wetland function and extent, and as such, has direct relevance to water management, hydrological
2232 models, planning and decision making.

2233 EMMA is a large-scale, landscape field manipulation of sediment and dredge material, with the
2234 potential to be incorporated into the USACE Beneficial Use Program ([The Role of the Federal Standard in
2235 the Beneficial Use of Dredged Material from U.S. Army Corps of Engineers New and Maintenance
2236 Navigation Projects \(PDF\)](#)), in the scrub mangrove ecosystem of the Model Lands, which is owned by
2237 Miami Dade County, and is not subject to the WQ or soil nutrient constraints associated with the Everglades
2238 Forever Act. Results of EMMA will have implications for and application to all coastal wetlands of Florida
2239 that are vulnerable to SLR.

2240 EMMA would take advantage of the new Thin Layer Placement (TLP) technology associated with
2241 distributing dredge spoil across an existing wetland to add elevation and, when needed, additional soil
2242 phosphorus (Berkowitz et al. 2019, VanZomeren et al. 2018). Beneficial uses of dredged material such as
2243 TLP will build landscape resiliency by improving soil aeration in the root zone, thereby increasing redox
2244 potentials (Eh), plant productivity, soil accretion, and by supplying a medium for greater carbon
2245 sequestration, which allows coastal wetlands to keep pace with SLR (DeLaune et al 1990, Baustian et al
2246 2015).

2247 **Goals and Objectives**

2248 Changes in water management in concert with SLR, has caused coastal wetlands to subside, tidal creeks
2249 to fill in (Meeder et al 2018)), peat to collapse (Wilson et al 2019), and plant communities to shift to slow
2250 growing, transgressive, open water habitats (Meeder et al, 2018). Peat collapse causes rapid declines in soil
2251 surface elevation (Chambers et al. 2019), converting wetlands in a vegetated state to an open water state
2252 (Cahoon et al. 2003; McKee et al. 2011; Baustian et al. 2012; Voss et al. 2013; Wilson 2018). In South
2253 Florida, peat collapse has been observed in sawgrass (*Cladium jamaicense*) peat marshes and coastal
2254 mangroves, which are highly organic (>85%), and depend on inputs of organic material to maintain and
2255 raise soil elevation, as they receive little inorganic sediment input (Rejmankova and Macek 2008, Chambers
2256 et al 2019). Since changes in soil surface elevation in mangrove and sawgrass peat marshes is largely a
2257 function of primary productivity, there is growing concern that saltwater intrusion will increase coastal
2258 marsh degradation.

2259 Without intervention, the current trajectory of SLR will result in significant land loss and loss of
2260 stormwater protection. Intervention that promotes accretion rates that act to maintain or outpace SLR in
2261 key coastal communities (e.g., those adjacent to historic tidal creeks) will result in a myriad of ecosystem
2262 and socio-economic benefits. The goal of this Pilot is to advance our understanding of biological vs.
2263 physical controls on the capacity of coastal wetlands to persist under increased SLR. Our objectives are to:

- 2264 1. Develop demonstration scale evidence that supports managed wetland transgression to include
2265 sediment augmentation via a TLP strategy.
- 2266 2. Evaluate the adaptive resilience of coastal mangroves to phosphorus enrichment in combination
2267 with enhanced soil elevations.

2268 Study Design

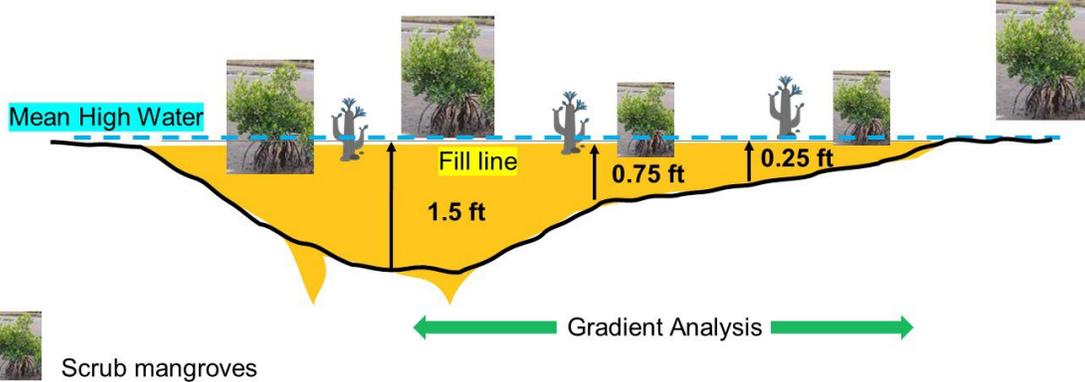
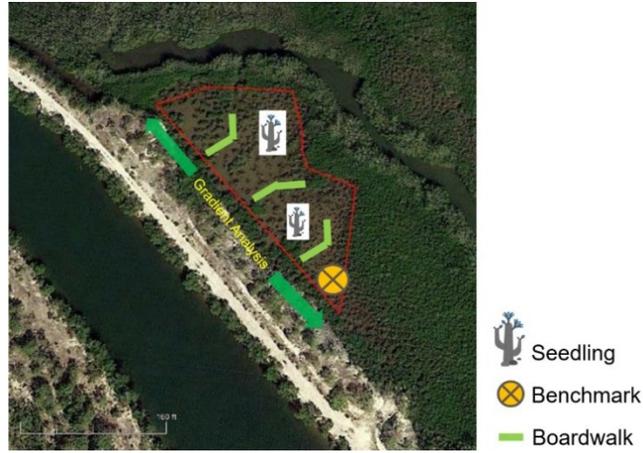
2269 The study will consist of three assessment locations (Figure 9-25) – the Charly Site located on the
2270 southeastern tip of the C-111 canal, the Pocket Site located along the C-111 just west of the S-197 structure,
2271 and the Baby EMMA Site located just west of US-1 and north of the C-111 canal. Peat accumulation and
2272 mangrove plant growth will be measured along transects that have been elevated by TLP in comparison to
2273 mangroves that have been locally spiked with elevated phosphorus. The multifactorial design (Figures 9-
2274 26 through 28) will divide each transect into control transects and TLP treatment transects to document
2275 costs and benefits of TLP and help establish the protocols for effective beneficial use of dredge materials
2276 in coastal habitats. Project implementation monitoring, as detailed below, will be conducted to measure
2277 changes in soil surface elevation, quantify belowground and aboveground biomass production, and track
2278 observable changes in water quality and exchange fluxes between surface water and groundwater in the
2279 spaces between sediments – inside and outside of the study area. It should be noted that all EMMA sites
2280 will have special sediment capture fences in place to retain sediments and prevent downstream turbidity
2281 plumes.



2282

2283 **Figure 9-25.** EMMA Assessment Locations (From left to right: Charly Site and Pocket Site)

2284

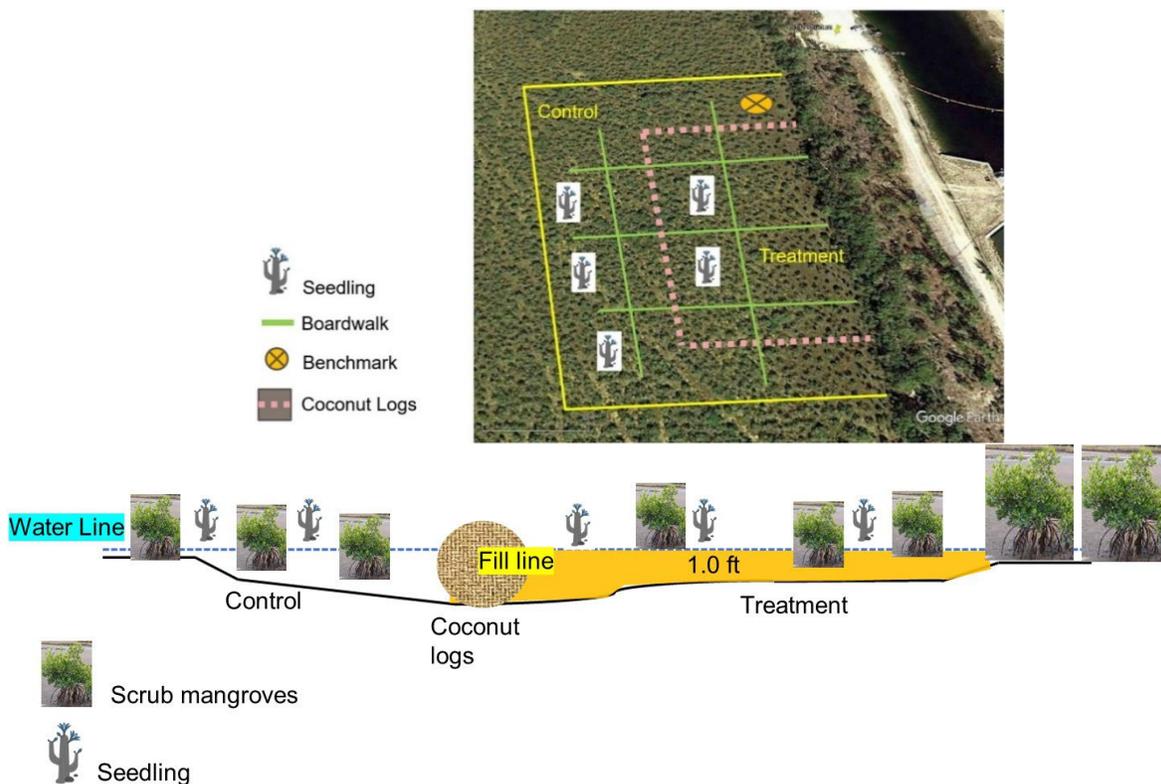


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2286

Figure 9-26. Pocket Site study design.

2287



2288

2289 **Figure 9-27.** Pocket Site study design.

2290 **Permanent Benchmarks and Soil Elevation Surveys**

2291 Permanent benchmarks will need to be installed in and around the study area to preserve relevance to
 2292 SL and SLR. Six Class “B” (Stainless Steel rod driven to refusal) NGS stability standard monuments will
 2293 be established. The work will include, but not limited to, processing the data, Quality Assurance, describing,
 2294 typing, and reconnaissance. If no published NGVD 29 elevations were available at the site, NGVD 29
 2295 elevations will be derived from the NAVD 88 elevations by means of applying a site-wide, uniform datum
 2296 shift, or offset value, of -0.456 meter (-1.496 feet). The sense of the algebraic sign of this value is NAVD
 2297 88 elevation minus NGVD 29 elevation. This value will be obtained from the NGS VERTCON model and
 2298 was computed by both the NGS VERTCON Online web site
 2299 (<http://www.ngs.noaa.gov/TOOLS/Vertcon/vertcon.html>, accessed May 2007, version 2.0) and by means of
 2300 the software CORPSCON version 6.0.1 (which itself uses the NGS-developed VERTCON software).

2301 The horizontal datum for this survey will be the North American Datum of 1983 (NAD 83). Soil
 2302 Elevation surveys will be conducted using real-time kinematics referenced to the 1988 North American
 2303 Vertical Datum (NAVD88) with Trimble R8 global navigation satellite system receiver equipment (Trimble
 2304 Inc., Sunnyvale, CA, USA) with a horizontal accuracy of ± 1 cm and a vertical accuracy of ± 2 cm. Soil
 2305 elevations will be set out with respect to the North American Vertical Datum of 1988 (NAVD 88) and the
 2306 National Geodetic Vertical Datum of 1929 (NGVD 29). NAVD 88 elevations will be determined by
 2307 differential leveling from benchmarks.

2308 **Sediment Elevation Table (SET)**

2309 The SET is an extremely accurate and precise leveling device designed to sit on a permanent benchmark
 2310 pipe or rod and measure changes in elevations in inter-tidal and sub-tidal wetlands (Boumans and Day 1993,

2311 Cahoon 1995). Once installed on the benchmark, the SET establishes a constant reference plane with respect
 2312 to the benchmark, allowing for repeated measurements of the sediment surface (Cahoon et al. 2002).
 2313 Changes in the elevation of the soil surface over time will be measured using the surface elevation table–
 2314 marker horizon (SET–MH) methodology, which has been widely used and recommended for monitoring
 2315 intertidal surface-elevation trajectories in coastal wetlands (Cahoon 1995).

2316 **Biotic Monitoring: Above and belowground biomass**

2317 Mangroves are considered ‘bottom heavy plants’ as they invest much of their biomass into their root
 2318 system (Komiyama et al., 2008, 2000). Mangroves have two kinds of root systems adapted to the anoxic
 2319 and saline conditions of mangrove habitats: aerial roots that grow above the soil surface, and belowground
 2320 roots. Belowground root biomass in mangroves generally contributes up to 60% of the total tree biomass
 2321 (Khan et al., 2009; Komiyama et al., 1987; Tamooh et al., 2008). It is critical that we understand the
 2322 belowground processes in this pilot study. At each plot, duplicate root cores (that is, sampling units; 0–45
 2323 cm depth; shallow root zone) will be randomly collected using a PVC coring device (10.2 cm diameter 9
 2324 45 cm length. Roots will be sorted into diameter size classes of less than 2 mm, 2–5 mm, and greater than
 2325 5 mm (fine, small, and coarse roots, respectively). Each root sample will be oven-dried at 60 °C to a constant
 2326 mass and weighed.

2327 Composition, tree density, and basal area in tall and scrub mangroves will be quantified through
 2328 measurements of the species and diameter at 1.3 m height (DBH) of all trees rooted within a designated
 2329 study plot, which will be 154 m² (radius of 7 m). Similarly, due to the lower density of the scrub mangroves,
 2330 tree density and biomass will be measured in six 2 m radius plots. The diameter of trees of *R. mangle* will
 2331 be measured at the main branch, above the highest prop root. In scrub mangroves, the diameter of the main
 2332 branch of the tree will be measured at 30 cm from the ground (D30).

2333 **Water and Soil Analysis**

2334 Soil carbon and nutrients: At each plot, soil samples for bulk density and nutrient concentration will be
 2335 collected using a peat auger consisting of a semi-cylindrical chamber of 6.4 cm radius attached to a cross
 2336 handle. Soil cores will be systematically divided into depth intervals of 0–15 cm, 15–30 cm, 30–50 cm, 50–
 2337 100 cm. Root and soil samples will be analyzed for Total Carbon, Total Nitrogen and Total Phosphorus.

2338 Porewater turbidity and salinity, and soil chemistry, may change during this study and may accretion
 2339 rates as they relate to belowground and aboveground biological production. Interstitial chemistry and
 2340 physical properties will be analyzed by extracting water from the ground at 30 cm using a syringe and an
 2341 acrylic tube. The syringe is rinsed twice before obtaining a clear water sample from which salinity was
 2342 measured using an YSI-30 multiprobe sensor.

2343 **Surface water chemistry.** To monitor possible impacts to water quality downstream from TLP, surface
 2344 water samples will be analyzed to identify any changes to physical and chemical properties over time.

2345 **Schedule and Costs:**

2346 Total costs, shown below, do not reflect the current efforts to integrate this pilot study with (1) funding
 2347 from the USACE Regional Sediment Management (RSM) Division to locate and distribute TLP spoil
 2348 materials or (2) funding from the National Science Foundation, given to FIU for its Long-Term Ecological
 2349 Research (LTER) to address the dynamics of ecosystem change in South Florida due to climate change.
 2350 The exact amounts of the USACE and the FIU LTER combined contributions to EMMA and the creation
 2351 of an adaptive foundational resilience protocol is not yet known and will need to be negotiated.

2352 **EMMA Cost Estimate**

2353 Everglades Mangrove Migration Assessment	\$2,760,000
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2354 **DIRECTING COASTAL ECOSYSTEM RESILIENCE PHASE 1: THE**
 2355 **MANGROVE EXPERIMENTAL MANIPULATION EXERCISE (MEME)**

2356 In order for the coastal wetland landscape to adapt to the impacts of increasing salinity and inundation
 2357 with increasing SLR (in the absence of restored freshwater flows), marsh species must maintain
 2358 productivity levels that enable the rate of positive soil elevation change to increase at a greater rate than SL
 2359 (e.g., wetland adaptive capacity). In this experiment, we will test the overarching hypothesis that increased
 2360 phosphorus availability and sediment elevation will confer the greatest adaptive capacity in a marl-forming
 2361 coastal marsh (greatest increase in annual and long-term soil elevation rate relative to the rate of SLR). We
 2362 further hypothesize that given the same environmental conditions (phosphorus and elevation), sawgrass
 2363 species will support the same adaptive capacity as low-density red mangrove species. At higher density of
 2364 red mangrove, we postulate that the degree of adaptive capacity will outpace that conferred by sawgrass
 2365 and low-density red mangrove. To improve coastal wetland ecosystem function degraded by saltwater
 2366 intrusion, this experiment will help elucidate environmental factors limiting positive wetland soil elevation
 2367 change and illuminate optimum approaches for enhancing ecological resilience of coastal Everglades
 2368 sawgrass and low-productivity mangrove wetlands.

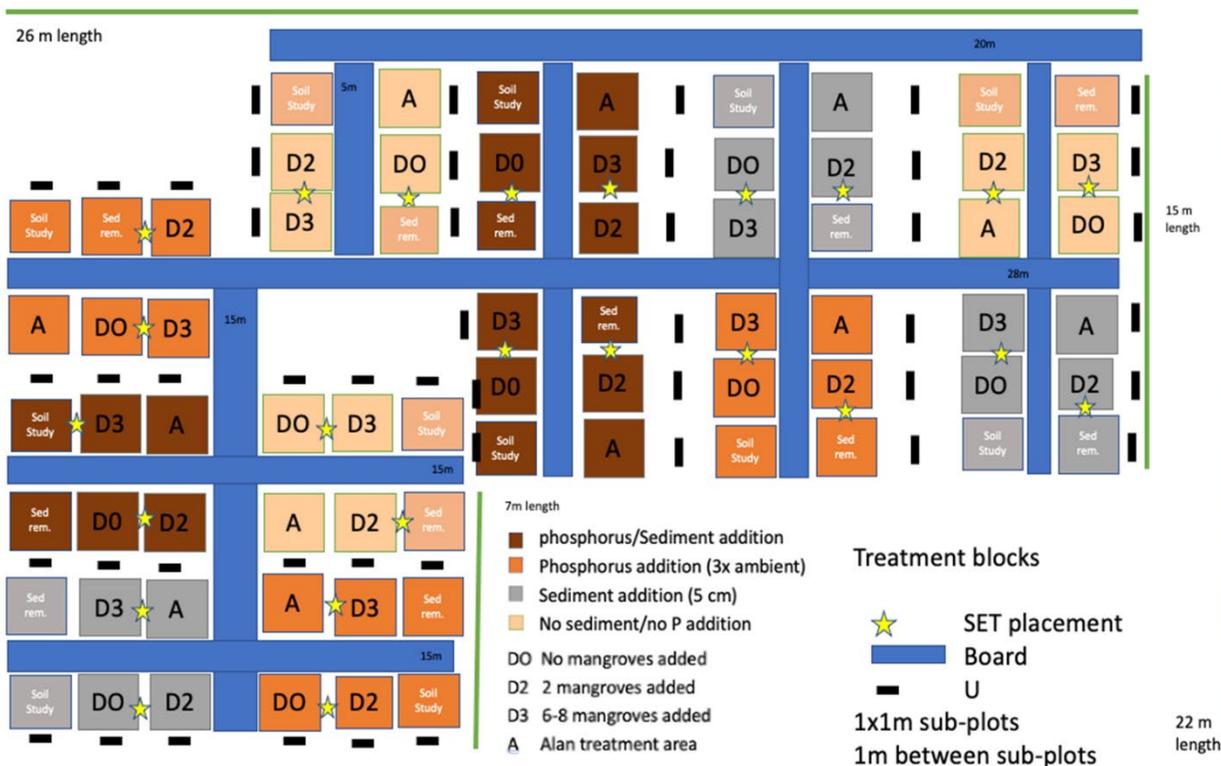
2369 The site is located within an area of the South Florida Water Management District, at approximately
 2370 25°17'25.02"N, 80°26'51.10"W, immediately north of the C111 canal and west of US1 (Figure 9-28). The
 2371 experimental plots support treatments of phosphorus, sediment elevation, and sawgrass with different red
 2372 mangrove densities.



2373 **Figure 9-28.** Study plot location in the South Florida, just south of the L-31E canal, east of Card
 2374 Sound Road. A. approximate plot location and B. plot location relative to US1 and Card Sound Road.
 2375 The total extent of the proposed study site is 572m² in area.
 2376

2377 This pilot study uses small 1-meter test plots to assessment a number of approaches that could enhance
 2378 the flood protection and ecological diversity of the coastal mangroves in the face of SLR. The distribution
 2379 of these plots within a scrub mangrove community along the C-111 canal, just west of FL Highway 1, are
 2380 shown in Figure 9-29. MEME manipulations are replicated and include three treatments: a planting
 2381 treatment, a soil addition treatment, and a phosphorus addition treatment. Due this multi-factorial design,
 2382 MEME requires some 60 plots.

2383



2384

2385 **Figure 9-29.** MEME study design. Legend for the above MEME Study (*NA = No Amendment; S =
 2386 Shallow (amendment +/-5cm); M=Moderate (+20-25cm); D = Deep (+50cm).

2387 Many of the techniques and analyses identified as part of EMMA are also part of MEME. These include
 2388 SET's, soil nutrient changes, soil elevation changes, plant growth and plant recruitment. Primary response
 2389 variables include soil elevation and surface accretion; porewater salinity, dissolved nutrients, carbon (C)
 2390 and sulfide; sawgrass and red mangrove aboveground standing biomass (non-destructive technique;
 2391 belowground biomass and root productivity; periphyton biomass and accumulation; water level and
 2392 hydroperiod; and soil and plant tissue C, nitrogen and phosphorus. A continuous water level and salinity
 2393 monitoring gauge will be deployed. Shallow 2.5cm diameter PVC samplers, installed to sample soil
 2394 porewater at 15 cm below the soil surface, will be installed in each sub-plot. Secondary response variables
 2395 include leaf and root decomposition rates. Red mangrove saplings will be planted at 2 saplings per meter
 2396 squared and 6 per meter squared.

2397

2398

2399 **MEME Cost Estimate**

Mangrove Experimental Manipulation Exercise	\$375,000
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2400

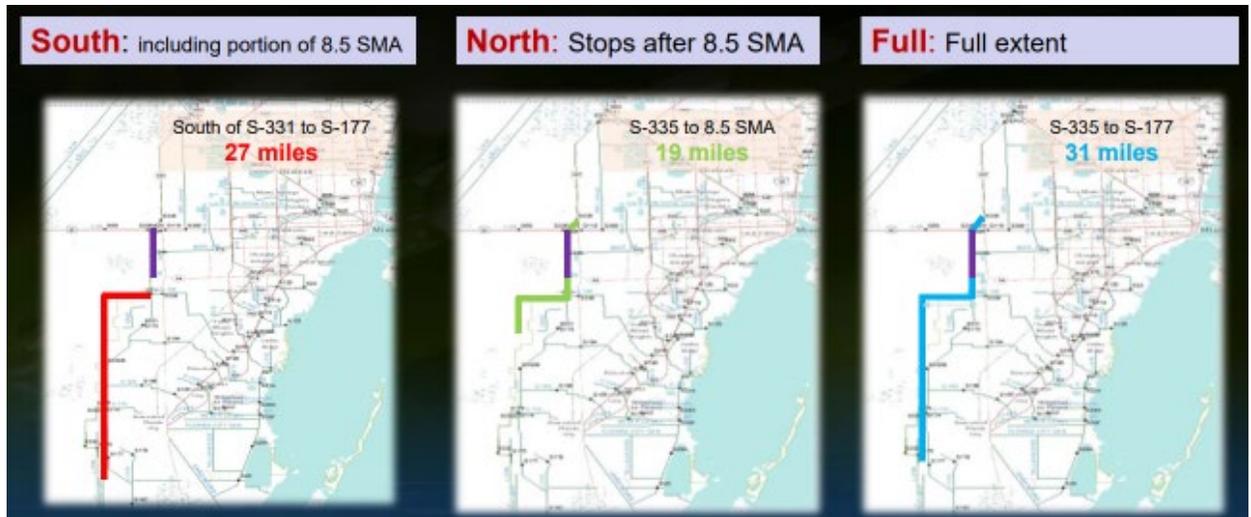
2401 **SOUTH MIAMI-DADE CURTAIN WALL**

This resiliency project is mainly tied to the District’s mission to provide flood control, water supply protection, and ecosystem restoration. The South Miami Dade Curtain Wall Project is being implemented by the District in the southern part of its water management system, adjacent to southwest Miami-Dade County developed areas and Everglades National Park. Curtain Walls are in-ground groundwater and seepage barriers that help to limit water flow in South Florida’s porous aquifer. The South Miami-Dade Curtain Wall Project will increase the District’s ability to manage water levels in Water Conservation Area 3A in Everglades National Park. Benefits associated with these established engineering features include flood protection, water supply maintenance, saltwater intrusion prevention, and ecosystem restoration, by improving water flow to Florida Bay and other estuaries. More specifically, this project will help prevent seepage of water from Everglades National Park while keeping the water in the park to support restoration goals and promote flow south toward Florida Bay, instead of seeping eastwards towards developed areas of South Dade where such seepage contributes to a reduction in flood protection level of service.

2429 Extensive hydrologic and hydraulic modeling efforts allowed the District to evaluate the most effective
 2430 alternatives in terms of the alignment, depth and extension of these proposed barriers, and associated
 2431 impacts. Feasibility Assessments developed since this project was first conceptualized, describe project
 2432 alternatives in combination with the current and future condition operations of the C&SF water
 2433 management features and CERP projects in the region. This project has been positively received in many
 2434 of the public meetings that have been held and is of interest to private, public, local, state and federal
 2435 stakeholders in the region.

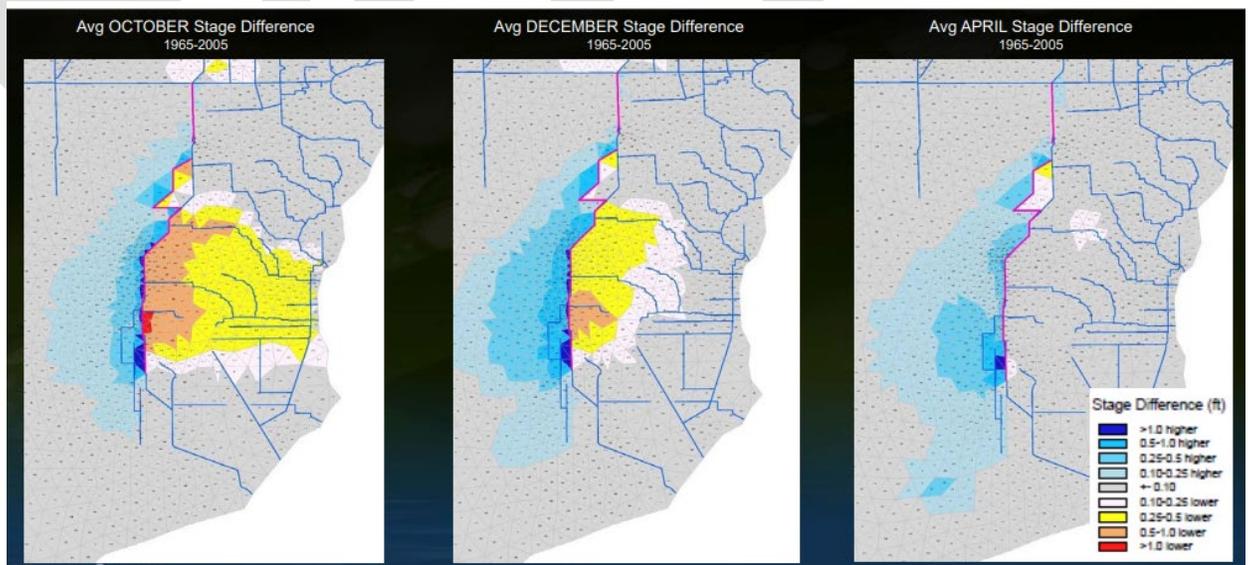
2436 The recent modelling effort completed by the District in 2018 demonstrated the benefit of the curtain
 2437 wall for both restoration and flood control. Several curtain wall configurations were examined. Figure 9-30
 2438 illustrates three different scenarios; a 27-mile South a 19-mile scenario, from Structure S-331 to Structure
 2439 S-177, including a portion of the 8.5 Square Mile Area (Las Palmas Community) in unincorporated Miami
 2440 Dade County; a 19-mile North scenario, from Structure S-335 including all of the 8.5 Square Mile area;
 2441 and a 31-mile Full Extent scenario from Structure S-335 to Structure S-177. The 27-mile South scenario,
 2442 with gaps in the curtain wall, was recommended for more detailed study and implementation because it
 2443 provided the best outcome for restoration and flood control while mitigating impacts to Biscayne Bay,
 2444 Taylor Slough and water supply.

2445 The results of the H&H modeling, illustrated in Figure below, demonstrate the flood control and
 2446 restoration improvements resulting from the 27-mile South scenario. Wetter conditions were observed in
 2447 Everglades National Park and drier conditions were observed in the eastern developed areas and in the
 2448 South Dade agricultural areas demonstrating improved restoration and flood protection conditions,
 2449 respectively.



2450
2451 **Figure 9-30:** Location and extension of three curtain wall configuration scenarios examined in 2018.

2452 Results of all three scenarios also show increased average annual overland flows to Shark River Slough,
 2453 during wet and dry seasons, compared to the No Wall scenario, as illustrated in Figure 9-31 and Table 9-8
 2454 below. Flows to Taylor Slough also improved with the Full and South wall scenarios. Successfully
 2455 intercepting and redirecting flows back into Everglades National Park reduces the availability of regional
 2456 water to Biscayne Bay, therefore, ongoing studies and future opportunities to ensure flows to Biscayne Bay
 2457 are maintained or enhanced are being advanced as part of parallel efforts. The Biscayne Bay Southeastern
 2458 Everglades Ecosystem Restoration Project (BBSEER) is being advanced in collaboration with the USACE
 2459 with the goals of making progress towards restoration of depth and duration of freshwater at Biscayne Bay,
 2460 as well as ecosystem structure and function with improved native plant and animal abundances and
 2461 diversity. The study recommended additional data collection and more rigorous modeling which was
 2462 authorized and funded by the Governing Board in 2020. The project, public planning process that engages
 2463 stakeholders and partner agencies is ongoing.



2464
2465 **Figure 9-31.** H&H modeling results illustrating the average water stage difference with and without the
 2466 full extent curtain wall scenario.

2467 **Table 9-8.** Average Annual Overland Flows to Shark River Slough during wet and dry seasons for three
 2468 curtain wall scenarios compared to the no wall scenario.

	No Wall	South Wall	North Wall	Full Wall
Shark River Slough	833	890	873	884
Wet Season (Jun-Oct)	466	501	486	491
Dry Season (Nov-May)	367	389	387	393
Taylor Slough	85	109	82	99
Wet Season (Jun-Oct)	61	74	59	69
Dry Season (Nov-May)	24	35	23	30
Biscayne Bay	927	874	897	889
North Bay	561	534	571	570
Central Bay	120	114	121	121
South Bay	246	226	205	198

2469
 2470
 2471 In March 2021, the SFWMD Governing Board approved the construction of the initial phase of the
 2472 South Miami Dade Curtain Wall Project / Seepage Cut-off wall, which consists of a 2.3-mile-long, 26-inch
 2473 wide curtain wall along the 8.5 Square Mile Area (Las Palmas Community) in unincorporated Miami Dade
 2474 County, along the C-358 Canal and the L-357W Levee. The 8.5 Square Mile Area Curtain Wall is nearing
 2475 completion. The total costs for the initial 2.3 miles - \$15M is fully funded with State Funds in a multiyear
 2476 project. The project was bid on a per unit length basis to allow continuation of the wall subject to additional
 2477 funding.

2478 In August 2002, the SFWMD Governing Board approved the construction of additional 4.9 miles of
 2479 seepage cut-off wall along the L-357W Levee from the end of the 2.3-mile segment to the junction with the
 2480 L-31N Levee, as part of the Central Everglades Planning Project (CEPP). This additional project continues
 2481 to minimize seepage from Everglades National Park (ENP) and mitigate regional flooding in urbanized
 2482 areas downstream.

2483 Additional new funding will facilitate construction of incremental curtain wall sections, increasing the
 2484 ability of water managers to address high water events in Water Conservation Areas and the Central
 2485 Everglades, promote flows to Florida Bay, and better utilize assets built for achieving restoration goals and
 2486 providing flood mitigation.

2487 The cost estimates below propose to incrementally build the curtain wall assuming five to ten miles
 2488 every three to five years at an average cost of \$8M-\$10M per mile escalated for inflation for the out years.
 2489 The final design of the full wall will be established at the end of the public planning process and may exceed
 2490 the total miles recommended in the initial study. Additional project refinement and confirmation of the final
 2491 extension of the seepage wall will be defined based on further model analyses and monitoring efforts.

2492
 2493
 2494
 2495

2496 **South Miami-Dade Curtain Wall Cost Estimate**
 2497

Implementation Timing	Amount*	Incremental Strategy
Immediate Needs (FY22-FY25)	\$75,000,000	Construction of 5-10 Miles
Near Term (FY25-FY28)	\$75,000,000	Construction of 5-10 Miles
Intermediate Term (FY28-FY31)	\$75,000,000	Construction of 5-10 Miles
Long Term (FY31-FY34)	\$75,000,000	Construction of 5-10 Miles

2498 *Cost in 2020 dollars will be adjusted for future years, assuming 7.5 Miles

2499

2500 **RENEWABLE ENERGY PROJECTS**

2501 **Solar Canopy at District Headquarters**



Among renewable energy projects, the District is proposing the installation of a solar canopy in the District Headquarters parking lot. Fleet vehicles could be parked under the canopy to keep them protected from the elements. The solar canopy would use net-metering to offset a portion of the energy usage and carbon footprint at District Headquarters. Electric vehicle charging stations could also be installed to utilize power generated by the solar canopy.

2510 **Floating Solar Panel Pilot Project**

2511 A floating solar panel pilot project on Lake
 2512 Freddy at District Headquarters would help to offset
 2513 energy costs. Floating solar panels have a lifespan of
 2514 25+ years and are designed to withstand hurricane-
 2515 force wind conditions. Additional benefits include
 2516 Increased energy production due to cooling effect of
 2517 water (in some cases 10+%), neutral or positive
 2518 environmental impact, improves water quality and
 2519 reduces algal blooms due to shading of the water
 2520 column.



Total Amount of Funding Request	Duration
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\$ 885,674	1 year
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2521 **Solar Panel Installations at C-43 and C-44**

2522 In addition, the District is initiating coordination with Florida Power and Light to potentially install
 2523 solar panel facilities at the C-43 and C-44 Reservoir adjacent lands with the goals of reducing energy costs
 2524 at these facilities as well as offsetting carbon emissions from existing and new proposed pump stations that
 2525 rely at non-renewable sources. Different options are under consideration, including both smaller 2–5-
 2526 megawatt projects to power local energy needs, and solar farms up to 75 megawatts to generate power to
 2527 the grid, using District lands.

Total Amount of Funding Request	Duration
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C-43 Solar Panel Installation Costs (2-5MW: \$8,000,000 – 10,000,000)	1 year
	1 year

C-44 Solar Panel Installation Costs (2-5MW :
\$8,000,000 – 10,000,000)c

2528



Chapter 10: Priority Planning Studies

SUMMARY

Various planning projects and efforts are being prioritized as part of the District's Resiliency Program. These studies are an integral part of providing South Florida with a robust and resilient flood infrastructure, now and in the future. Planning projects help support the South Florida Water Management District's (SFWMD or District) Resiliency mission, by coordinating scientific data and research needs to ensure the projects are founded on the best available science.

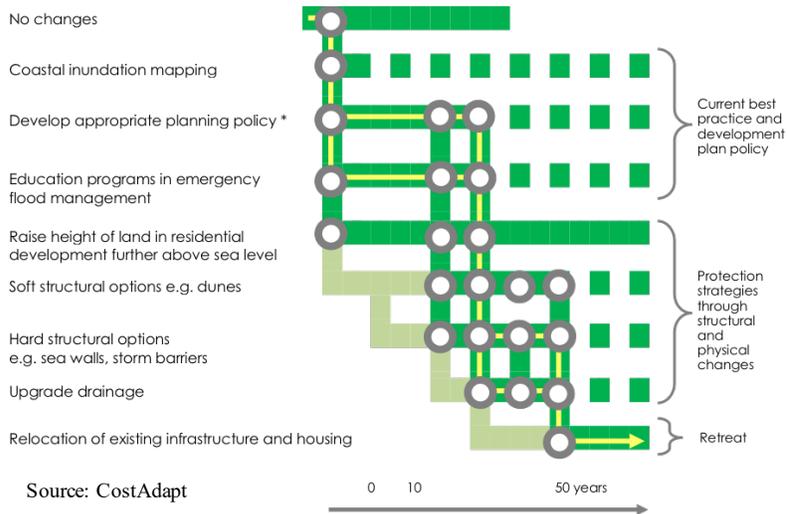
Hydro-meteorological monitoring has played an important role in managing the water control system in South Florida. Through its DBHYDRO tool, the District stores and makes hydrologic, water quality, and hydrogeologic data available to the public and partner agencies. Continuing efforts to enhance monitoring are important to combat a changing climate and increasing sea levels. Science and data are required to build a resilient water management system and infrastructure that addresses current and future impacts. Hydro-meteorological data such as seawater level, air temperature, incoming solar radiation, rainfall, and evapotranspiration rate can provide trends that can help with prediction of climate change. Due to the relatively slow process of climate change, monitoring stations must be of high quality and structurally stable to minimize environmental disturbances to the station. In this context, the District is implementing a set of water and climate resilience metrics to track and document shifts and trends in District-managed water and climate data. These efforts support the assessment of current and future climate condition scenarios and District resiliency investment priorities. As part of the District's communication and public engagement, the effort will provide information to stakeholders, and public and partner agencies, while supporting local resiliency strategies. Key planning projects are detailed below, to support the continued monitoring and metrics development.

In addition to observed and projected data analysis and monitoring processes, hydraulic and hydrologic modeling efforts are fundamental in evaluating the effectiveness of the District's flood control assets which include canals, structures, and pump stations. Modeling efforts help to determine if the flood control system meets and will continue to meet flood protection needs. The Flood Protection Level of Service (FPLOS) Program is being implemented at a regional and local scale using a suite of tools and performance indicators for evaluating structures and canals in selected watersheds, as well as a framework for establishing the level of service at each basin. The program incorporates input from meetings and workshops with local planning and stormwater management efforts, stakeholders, and resource managers. The results provide support for local flood vulnerability assessments, based on the latest modeling tools and most advanced dynamic H&H models, simulating existing drainage infrastructure to determine flood inundation scenarios, the necessary integration between surface and groundwater systems, and tidal/storm surge and rainfall scenarios for current and future conditions. Modeling efforts also include future conditions groundwater modeling to evaluate sea level rise (SLR), the saltwater intrusion monitoring network, and climate change impacts that may influence future water use vulnerability.

Recurring funding needs to continue to advance Phase I - Assessments and Phase II Adaptation Studies in priority basins, annually, as well as groundwater / water supply modeling efforts, are detailed below.

40 **FPLOS ADAPTATION AND MITIGATION PLANNING (PHASE II**
 41 **STUDIES)**

42 FPLOS Phase II studies will
 43 build upon previously developed
 44 FPLOS Phase I water management
 45 (H&H) models to identify feasible
 46 flood adaptation and mitigation
 47 solutions in critical basins. Results
 48 of these studies will help develop
 49 recommendations for regional and
 50 local integrated strategies and
 51 priority infrastructure investments
 52 and operational changes that may
 53 be required to ensure continued
 54 long-term performance of the at-
 55 risk parts of the system. When the
 56 FPLOS assessment (Phase I
 57 Studies) identifies a deficiency in



58 the flood control system, a detailed public planning study is initiated to identify appropriate resilient
 59 adaptation strategies. This public planning approach ensures the agency, in collaboration with partners and
 60 stakeholders, determines the best local and regional solutions that are not limited to the primary system.
 61 The comprehensively evaluated and coordinated course of action, based on robust technical assessments,
 62 will ensure that the District’s flood protection systems maintain their level of service, in response to
 63 population growth, land development, SLR and climate change.

64 It is crucial that this phase of the FPLOS program be properly funded, preferably with recurring funds,
 65 because it identifies projects that are ready to design and build, both for the District and for local
 66 stakeholders that are responsible for secondary and tertiary flood control assets. Results from this phase
 67 may (on a project-by-project basis) provide recommendations for cost-share opportunities with Federal,
 68 state or local partners. A constant stream of properly, regionally evaluated project features across the three
 69 tiers of the flood control system will position the region well to compete for state and Federal funds for
 70 flood control and flood resilience infrastructure.

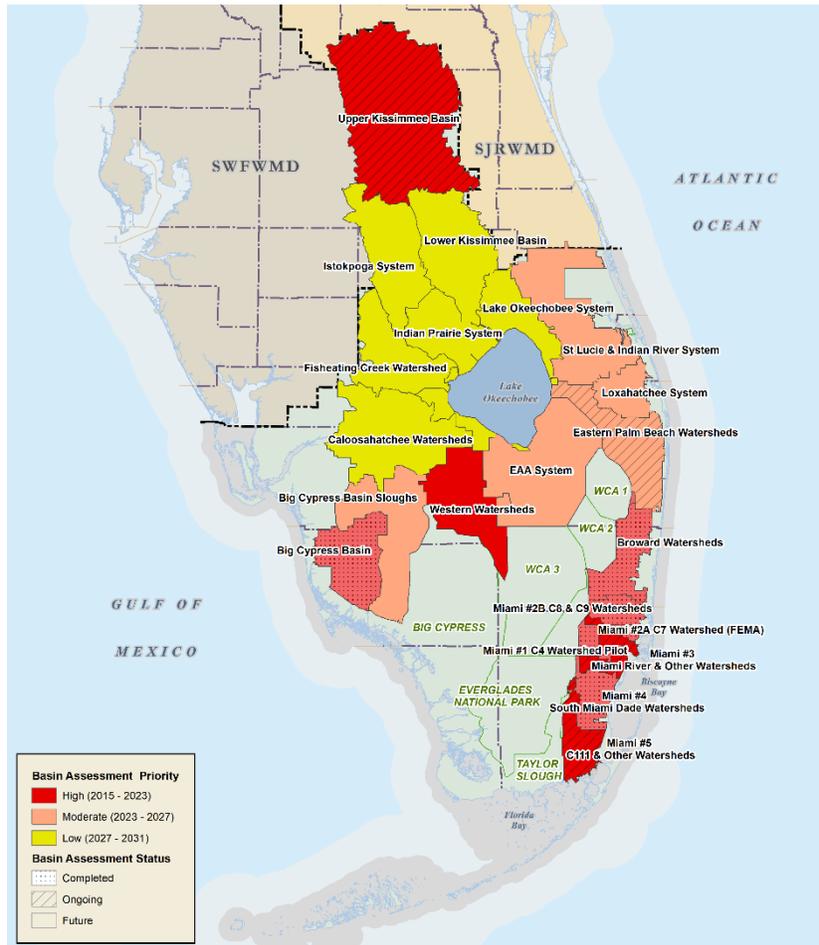
71 An adaptation pathway approach is incorporated into the Phase II studies to support the definition of
 72 an implementation strategy for the recommended projects (sequences and combinations of flood adaptation
 73 and mitigation strategies). If an individual flood mitigation alternative is not able to achieve the specified
 74 target of a predetermined performance criterion, additional mitigation strategies are triggered, setting up a
 75 plan on how multiple strategies can be implemented over time.

76 In FY23, Phase II Studies were completed for the C-9 and C-8 Basins in Broward and Miami-Dade
 77 counties. The C-7 Pilot Phase II Study is under initiation. . The Program annual budget is \$2M with at least
 78 one new start every year. Design costs are not included as part of this phase and will be completed upon
 79 funding confirmation for each individual recommended flood adaptation project.

Total Amount of Funding Request	Duration
\$2,000,000	Yearly - recurring

80 **FPLOS ASSESSMENT (PHASE I STUDIES)**

81 FPLOS Phase I Studies have
 82 been ongoing for the past eight
 83 years. These studies identify and
 84 prioritize long-term infrastructure
 85 improvement needs, in response
 86 to population growth, land
 87 development, SLR and climate
 88 change. Requested funding will
 89 be used to advance the
 90 development of water
 91 management (H&H) models to
 92 evaluate the flood protection
 93 system operations under changed
 94 current and future conditions.
 95 This phase identifies issues in the
 96 flood control system in 8- to 10-
 97 year cycles through a
 98 comprehensive, regional
 99 approach to addressing flood
 100 risks, intensified by SLR. Phase I
 101 studies also properly characterize
 102 flood vulnerability, risks to
 103 critical assets, and potential co-
 104 benefits of integrated solutions.
 105 This effort is integrated into the
 106 District’s Capital Improvement
 107 Program to ensure its structures,
 108 pumps, and canals are functioning
 109 as designed, and will remain
 110 operational under future climate conditions.



111 This cost estimate detailed below is for full funding, which will allow the FPLOS program to meet its
 112 planned schedule of two new assessments each year, to meet the goal of cycling through all District basins
 113 every 8 to 10 years. All FPLOS H&H models, input data and output results developed as part of assessment
 114 and adaptation planning efforts are being and will continue to be stored in the statewide model management
 115 system (<https://apps.sfwmd.gov/smmsviewer/>).

Total Amount of Funding Request	Duration
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\$2,000,000

Yearly - recurring

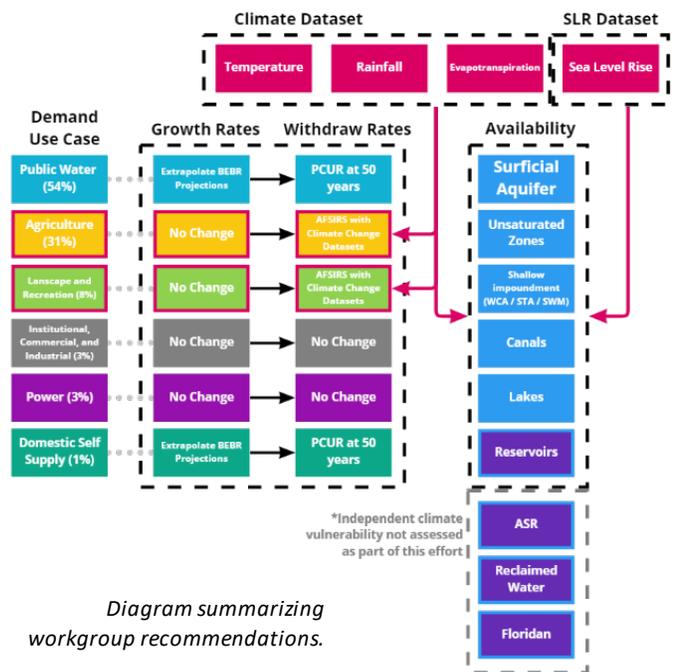
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118 **WATER SUPPLY VULNERABILITY ASSESSMENT**

119 The South Florida Water Management District (SFWMD) is conducting a Water Supply Vulnerability
 120 Assessment aimed at understanding how future development and climate conditions impacts our regional
 121 water supply. As an initial effort, SFWMD is developing the East Coast Surficial Groundwater Model
 122 (ECSM) to be density dependent allowing for SLR scenarios to be incorporated into the model simulations.
 123 Additionally, SFWMD has contracted Florida International University (FIU) and the US Geological Survey
 124 (USGS) to develop future conditions
 125 rainfall, evapotranspiration (ET), and
 126 temperature datasets to support scenario
 127 formulation for the ECSM model runs and
 128 other regional modeling.

129 SFWMD created an internal
 130 workgroup with representation from
 131 various bureaus to develop an approach for
 132 identifying and assessing vulnerabilities.
 133 Initial scenarios, modeling assumptions,
 134 input data selection and limitations,
 135 research, scope, time, and cost were
 136 considered in the development of the
 137 proposed approach. The following
 138 illustrations summarize a subset of initial
 139 recommendations and assumptions that are
 140 integrated into the proposed approach.
 141 More detailed information on the approach,
 142 and next steps are described in the
 143 upcoming report: Water Supply
 144 Vulnerability Assessment – Scoping
 145 (Appendix C).



143 *Diagram summarizing*
 144 *workgroup recommendations.*

146 To properly analyze the effects of climate change, including SLR, each of the water availability sources
 147 will be analyzed as independent “buckets” and model outputs will highlight the effects of select parameters.
 148 Initial scenario formulation is proposing less and more conservative estimate ranges, with degrees of
 149 warming, dryness, and sea level rise, along with growth scenario ranges. The outputs of these scenario runs
 150 should allow for SFWMD to understand how future conditions may impact source characteristics, water
 151 management operations, and overall water availability. Future iterations may include the analysis of water
 152 management strategies and their effects.

153 The vulnerability assessment will be in addition to the 5-year update to the Lower East Coast Water
 154 Supply Plan anticipated to be completed in 2024, and other upcoming water supply plan (WSP) efforts. The
 155 assessment will therefore be based on WSP methodologies by independently analyzing climate effects on
 156 growth rates, withdrawal rates, and available water supply sources. Public water supply and domestic self-
 157 supply’s 20-year growth rates are currently being extrapolated to 50 years, through an ongoing contract
 158 with the University of Florida’s Bureau of Economics and Business Research. Respective withdrawal rates
 159 will be calculated using the 20-year per capita use rate. Agriculture, landscape, and recreational withdrawal
 160 rates will include projected temperature, rainfall, and ET rates at 50 years. The surficial aquifer and other
 161 fresh water sources will incorporate SLR in its boundary conditions and all surface water and unconfined
 162 groundwater will incorporate future temperature, rainfall, and ET conditions. The funding request is to
 163 support modeling scenarios formulation and development, followed by the analysis and reporting of results.

Total Amount of Funding Request	Duration
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\$1,200,000

Four Years – One time

164 **WATER AND CLIMATE RESILIENCY METRICS - WEB TOOL**
 165 **IMPLEMENTATION**

166 As part of a series of
 167 resiliency initiatives to address
 168 changing conditions, the District
 169 has established an initial set of
 170 water and climate resiliency
 171 metrics District-wide. These
 172 science-based metrics were
 173 developed with the goal of
 174 tracking and documenting trends
 175 and shifts in water and climate
 176 data. The metrics support the
 177 assessment of current and future
 178 climate condition scenarios and
 179 related operational decisions that
 180 inform vulnerability assessments,
 181 adaptation planning and decision
 182 making in support of the
 183 determination of District resiliency investment priorities. As part of the District’s communication and
 184 public engagement priorities, this effort informs stakeholders, the public, and partner agencies about the
 185 District’s resiliency efforts, while supporting local resiliency strategies.



186 The Water and Climate Resiliency Metrics are an important step towards planning for the future with
 187 consideration of long-term observed trends and their impacts on the District’s mission. The initial set of
 188 selected water and climate resiliency metrics are currently being automated for publication through an
 189 interactive web portal, providing navigation to different locations District-wide and access to real time
 190 data. The portal generates alternative mapping, chart, and graph options to display and
 191 communicate trend results, supported by a story map.

192 This webtool provides real time updates of observed data and automated trend analyses, for eight of the
 193 fifteen prioritized Water and Climate Resiliency Metrics. Real time automation minimize rework and
 194 reprocessing of trend analysis for the selected metrics, based on the best available data and are integrated
 195 into the District’s existing database tools, DBHydro. Currently, DBHYDRO Insights automation is
 196 completed for tidal elevations, groundwater levels and chlorides, and evapotranspiration. Additional story
 197 maps finalized include regional rainfall, salinity in the Everglades, estuarine and mangrove inland migration
 198 and soil subsidence. Water Quality automation and story maps are projected to be completed in FY2023.

199 This funding request will be used to incorporate new metrics, continue automation and finalize
 200 additional story maps. In addition, funding will support continued integration between DBHydro and the
 201 ESRI based Resilience Metrics Hub featuring story maps and web tools for analyzing and sharing data, as
 202 well as the development of the Water and Climate Resiliency Metrics Phase II – Development of Future
 203 Projections.

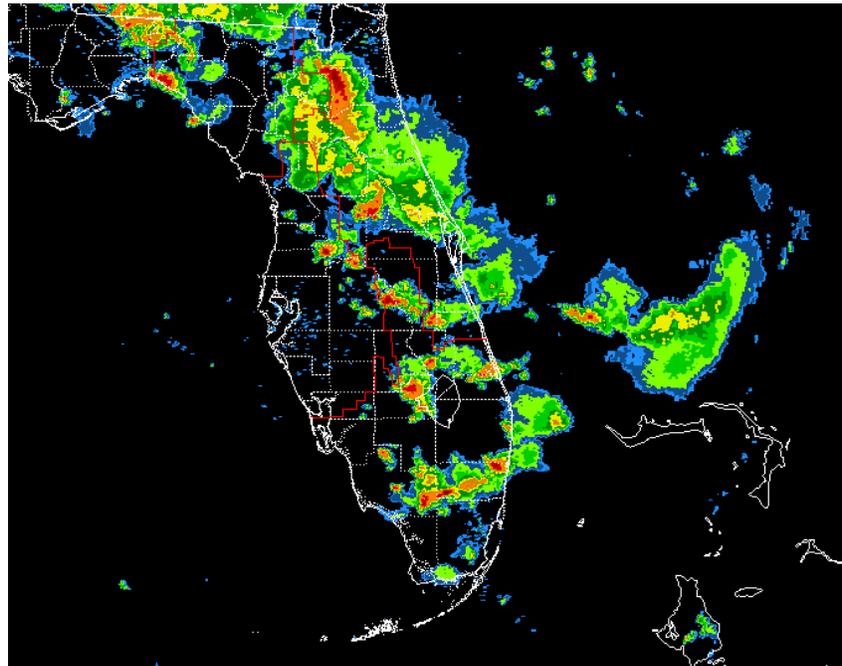
Total Amount of Funding Request	Duration
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\$300,000

Three Years – One Time

204 **HYDROMETEOROLOGICAL DATA MONITORING**

205 This funding request for
 206 hydrometeorological monitoring
 207 will be used for establishing key
 208 baseline monitoring stations, and
 209 evapotranspiration monitoring
 210 for Lake Okeechobee and the
 211 rainfall monitoring network,
 212 focusing on specific resiliency
 213 needs. Future additional data
 214 needs will continue to be
 215 identified and validated through
 216 the Water and Climate
 217 Resiliency Metrics Project.



218 Hydrometeorological
 219 monitoring has played an
 220 important role in managing
 221 water control systems in South
 222 Florida. Stage, flow, and rainfall
 223 data are used daily in SFWMD’s
 224 Operations and Control Center.

225 District weather stations, Florida Agricultural Weather Network’s stations, and National Oceanic and
 226 Atmospheric Administration stations, have been used to calibrate/verify the Geostationary Operational
 227 Environmental Satellite estimate of incoming solar radiation. Incoming solar radiation is the most important
 228 factor that drives evapotranspiration, and therefore is vital for generation of reference evapotranspiration
 229 and potential evapotranspiration estimates for all of Florida at the resolution of 2-km by 2-km grids.

230 With proper support from the Resiliency program, rainfall analyses, such as temporal and spatial
 231 distribution, and trend analysis, can be strengthened and conducted at a more frequent interval, including
 232 sub daily analyses. Rain gauge stations can be added to the network to address the coverage disparity
 233 identified by the Rain Gauge Network Optimization study. A properly distributed rain gauge network will
 234 benefit radar rainfall estimates, and climate change trend analysis. Additionally, the National Hurricane
 235 Center in Miami has been using the meteorological data from the District’s weather stations for hurricane
 236 prediction. More accurate data would benefit these efforts as well.

237 Building resilient water management systems and infrastructure requires science and data. Time series
 238 hydro-meteorological data such as seawater level, air temperature, incoming solar radiation, rainfall, and
 239 evapotranspiration rate can provide input for trend analyses used for the prediction of climate change.

Total Amount of Funding Request	Duration
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\$300,000

Four Years – One Time

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STATEWIDE REGIONAL CLIMATE PROJECTIONS

Statewide Regional Climate Projections are being developed by the Florida Flood Hub and in coordination with Florida Department of Environmental Protection (FDEP), USGS, academia, Water Management Districts, Regional Planning Councils, Florida Department of Transportation and other partner agencies to capture conditions/mechanisms of rainfall, and other related climate variables. Determination of future extreme rainfall conditions (both wet and dry conditions) is key for evaluating potential impacts from climate change to operation of District infrastructure and mission implementation. The District has specific interest in determination of future rainfall scenarios as part of FPLOS Phase I Assessments and the Water Supply Vulnerability Assessment.



The District, the U.S. Geological Survey, Florida International University (FIU) and local governments have been working over the past six plus years at evaluating global and regional climate models to estimate future extreme rainfall conditions. In May 2019, the District and FIU organized a Workshop to define a strategy for the development of uniform rainfall scenarios in Florida. As part of the short-term workshop

264 recommendations, the District, in partnership with USGS and FIU assessed best available downscaled
 265 climate datasets and published the “Extreme Rainfall Change Factors for Flood Resiliency Planning in
 266 South Florida” at the Water and Climate Metrics Hub. The Florida Flood Hub has partnered with the same
 267 team to extend these projections statewide, which recently initiated in FY2023, under the technical
 268 supervision of an established working group with representatives from all the partner agencies listed above.
 269 A parallel long-term effort is being conducted, as recommended in the 2019 Workshop, because the use of
 270 available climate datasets for estimating future rainfall in Florida show biases in extreme rainfall, which
 271 are relatively large when comparing past observation with climate model’s historic data. The Statewide
 272 Regional Climate Projections modeling effort will be better suited to capture conditions/mechanisms of
 273 rainfall occurrences in our State, including contributions from tropical storms and sea breeze, as well as
 274 Florida shelf and ocean dynamics, and other important climatic processes. Advancing a statewide regional
 275 climate projections model will reduce future rainfall uncertainty estimates in Florida. The financial
 276 contribution from SFWMD to this project, in support of the Florida Flood Hub, is summarized below.

277

Total Amount of Funding Request	Duration
\$150,000	Three Years – One Time

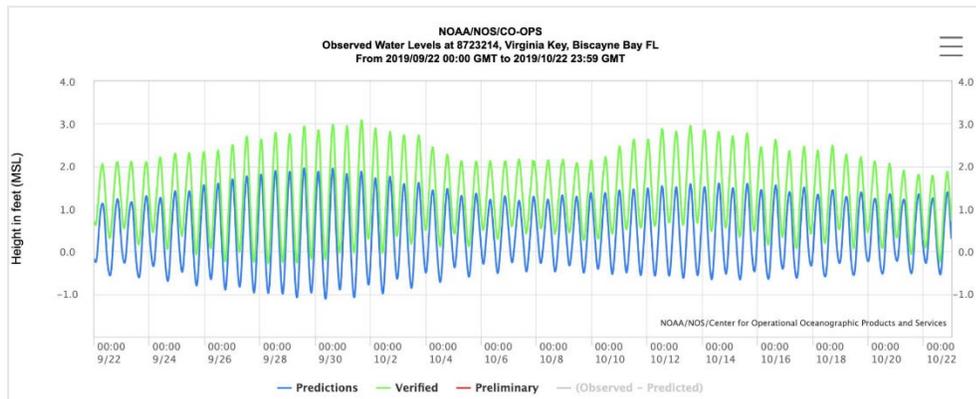
278

279 **ENHANCING TIDAL PREDICTIONS (SFWMD, UNIVERSITY OF MIAMI**
 280 **ROSENSTIEL SCHOOL OF MARINE AND ATMOSPHERIC SCIENCE)**

281 Local near-future tidal predictions are being developed in partnership with the University of Miami
 282 (UM) Rosenstiel School of Marine and Atmospheric Science (RSMAS) to capture tidal conditions
 283 influenced by global and local variables. Establishing accurate near-future tidal conditions is key for
 284 evaluating potential impacts due to SLR to operation of the District’s coastal structures and mission
 285 implementation. Accurate tidal predictions will improve water management response and response timing,
 286 ultimately reducing flood disaster risks and benefiting communities in South Florida.

287 NOAA tidal predictions, which are available for any site well into the future, are limited by current
 288 model inputs. These tidal predictions use sea-level information from 1983-2001, a historical period that
 289 does not account for the roughly six-inch rise in sea level observed in South Florida in the last 20 years.
 290 Furthermore, these tidal predictions are produced using a course seasonal average of tides and lack inputs
 291 representing current weather or oceanic conditions.

292 In 2022, UM completed improvements to current tidal predictions by accounting for more recent
 293 changes in sea-level rise and including adjustments for surface pressure forecasts (weather elements such
 294 temperature, wind velocity and direction, humidity, rainfall, cloud formation, sunshine, thunder and
 295 lightning over a geographic area) to address the limitations of current tidal predictions. Moreover, the
 296 improved prediction model includes a multiple linear regression that accounts for various additional
 297 relevant parameters, such as oceanic waves. The updated model has been run and validated for NOAA’s
 298 Virginia Key Tide Station (and its U.S. global weather model (GFS) output is available for up to 10 days
 299 in the future.



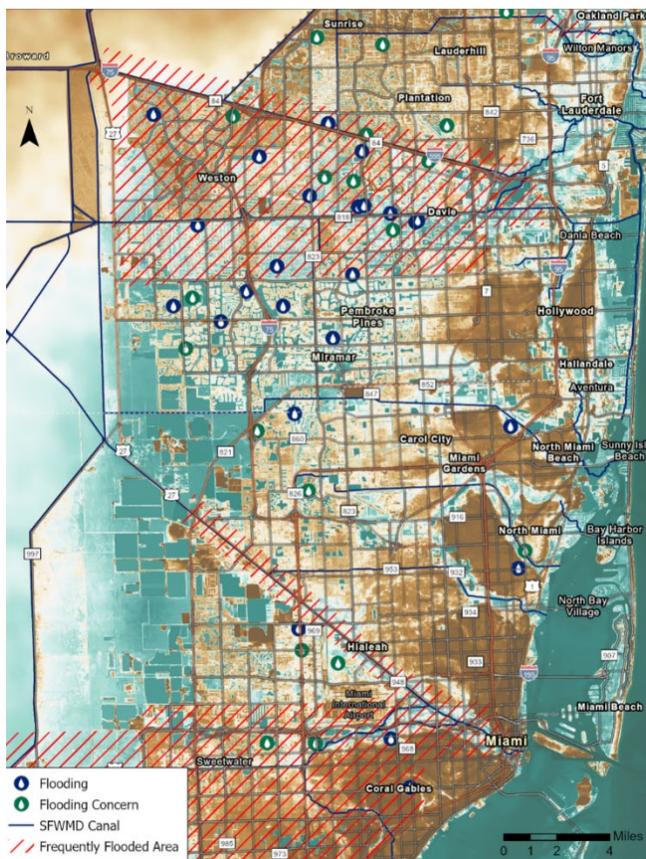
300
 301 The District is partnering with UM RSMAS to build on current efforts and refine the model for use at
 302 additional tide stations along South Florida’s east coast: Port Everglades, Lake Worth, Key West, Vaca Key
 303 and Naples. Near-future tidal predictions based on the latest available data and best available science would
 304 provide water managers at the SFWMD and local agencies more accurate and necessary information to
 305 respond to variable weather conditions now and in the future.

Total Amount of Funding Request	Duration
\$ 65,000	2 Years – One time

307 **FLOODING OBSERVATION SURVEY AND NOTIFICATION SYSTEM**

308 Identification and documentation of high-water marks and other flood observations is critical to
 309 understanding flood depth and extent and provides observations necessary to validate simulation models
 310 attempting to replicate flood occurrence. Identifying where to record and measure high-water marks is a
 311 challenge. Flood observations during events can be used to inform high-water mark collection as well as
 312 provide an early warning of emerging issues that require investigation to mitigate during an event.

313 Compilation of flood distribution, depth, and extent over time will inform understanding of trends in
 314 flood occurrence and effectiveness of mitigation efforts. Although there are local initiatives to collect such
 315 information, there are no regional or statewide tools that can be leveraged at the local level to assist in early
 316 notification or inform high-water mark collection. A regional system of collection and notification would
 317 provide local tools to assist local agencies in responding to and documenting flood occurrence within their
 318 jurisdiction. It would provide a repository for evaluating flood occurrence over time and could be leveraged
 319 to model and develop mitigation measures to address increasing flood occurrence. At a regional level, such
 320 tools can be used to assess regional trends and better inform understanding of the response of regional and
 321 local systems to rainfall and mitigation measures.



Development of a regional flood observation and reporting system is proposed to standardize and centralize flood observation information. Once established, this repository can serve as the basis for development of other regional and statewide tools to assist in the compilation and standardization of flood evaluation and be used to validate local and regional modeling tools for design and implementation and mitigation measures.

Although regional monitoring networks provide critical information for the evaluation of hydrologic trends, a repository of ground observations are needed to understand how these trends impact the effectiveness of local and regional storm water management systems and how mitigation measures are improving those conditions. This proposal is to establish cloud based regional flood data collection tools and a repository for the standardization flood observation and high-water mark data to evaluate flood occurrence over time and mitigation measure effectiveness.

Total Amount of Funding Request	Duration
\$1,000,000	Four Years – One Time

345 **EVALUATING THE PERFORMANCE OF THE SFINCS HAZARD MODEL TO**
 346 **SUPPORT AND ACCELERATE THE FPLOS AND SEFL REGIONAL**
 347 **ADAPTATION PLANNING EFFORTS**

348 Following the recently finalized collaborative development of the SFWMD-FIAT tool and partnership
 349 meetings between the District, Miami-Dade County, Broward County, and Deltares, this project description
 350 summarizes regional modeling challenges and proposes an evaluation of a new tool to address these
 351 challenges. The FPLOS and regional adaptation planning efforts experience various modeling challenges:
 352 First, integration of coastal and inland flood modeling is currently lacking. As a result, the studies do not
 353 consider compound flooding. Second, the comprehensive MIKE flood models used by the District and
 354 Broward County yield reliable and high-resolution results, but this comes at an expense: run times for
 355 individual scenarios amount to nine hours. As a result, detailed probabilistic flood hazard modeling is not
 356 feasible. As an alternative, the District and Broward County work with a representative set of
 357 scenarios/conditions, using a deterministic approach. As an additional consequence, the studies can model
 358 only a relatively small subset of the many identified scenarios, introducing decision-making uncertainties.
 359 Finally, only model experts can use the modeling tools, and the tools miss an adequate translation to support
 360 planning. Herein, Miami-Dade County relies on the modeling work of the District to inform and support its
 361 planning efforts.

362 The USGS and Deltares recently improved and applied the Coastal Storm Modeling System, COSMOS,
 363 to the southeast Atlantic coast, including South Florida, as part of their coop. The improvement included
 364 setting up and validating the compound flood model SFINCS (Super-Fast Inundation of Coastal Systems),
 365 a physics-based, reduced complexity model with typical runtimes of seconds to a couple of minutes for
 366 individual hydro-meteorological events depending on the spatial scales. The SFINCS flood hazard model
 367 is also part of the Community Flood Resilience Support System (CFRSS), recently developed by Deltares
 368 in partnership with the Department of Homeland Security. The CFRSS helps address all the above-listed
 369 challenges and supports the DHS in its mission to accelerate climate adaptation nationwide. The system
 370 application to Charleston, the pilot community, is promising.

371 The SFINCS and the CFRSS tool could, e.g., support the FPLOS program as quick scan tools to
 372 evaluate all scenarios of interest quantitatively. Then, based on the results, scenarios for detailed
 373 assessments using the comprehensive Mike models can be selected and implemented, reducing uncertainty
 374 in decision-making. However, this use requires an additional performance evaluation of the SFINCS model.
 375 For instance, validation of the available SFINCS model in the COSMOS modeling system for South Florida
 376 focused on the near-shore water levels. Therefore, the proposal is to thoroughly assess the performance of
 377 SFINCS in simulating regional flood extents and water depths by comparing the model inputs, outputs, and
 378 computational times with the MIKE models and readily available field observations used to calibrate and
 379 verify the MIKE models. The costs for this in-depth performance evaluation approximate \$75,000 and
 380 includes updating the SFINCS model application as needed and possible within the scope and available
 381 budget. The later will be determined in collaboration with the District. In FY2023, a workgroup was
 382 established with representatives from SFWMD, Deltares, USGS, FIU, University of Miami, and University
 383 of California Irvine to support the development of this project and additional parallel efforts currently in
 384 development for the support of flood adaptation planning.

Total Amount of Funding Request	Duration
\$75,000	1 Year

385 **GREEN INFRASTRUCTURE FLOOD MITIGATION STRATEGIES -**
 386 **ASSOCIATING WATER QUALITY BENEFITS IN THE LITTLE RIVER**
 387 **WATERSHED**

388 In partnership with Miami-Dade County and Florida International University, this project proposed the
 389 integration of scientific research and coastal water management challenges to develop actionable
 390 information for resilience of coastal environments in the face of climate change, SLR, and land-use
 391 development. The overall goal is to identify nature-based features that can be evaluated for flood protection
 392 and water quality benefits in consultation with stakeholders to improve watershed restoration planning.



To enhance regional adaptive capacity for addressing the increasing challenges of flood and water quality protection, a more comprehensive approach to watershed management is needed. This project proposes to address the overarching question: What are the flood mitigation and water quality benefits of cumulative “green elements” of the

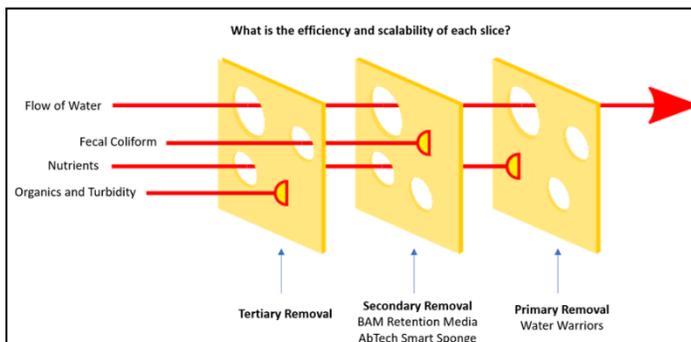
414 Community Rating System (CRS) program and other nature-based features with and without gray flood
 415 mitigation approaches? By planning for restoration and enhancement of natural functions that can improve
 416 flood protection and water quality benefits within the watershed in a coordinated effort across agencies,
 417 supported by expertise of local academic and NGO collaborators, it facilitates enhancing socio-ecological
 418 resilience in the face of SLR and land-use change.

419 Quantifying flood mitigation and water quality benefits through comprehensive watershed restoration
 420 planning is a key outcome of the project. Comparing FPLOS performance metrics, water quality benefits
 421 (specifically, TP, TN, and TSS load reductions), and averted economic damage across the diverse set of
 422 watershed restoration scenarios will support flood protection planning with quantifiable environmental,
 423 societal, and economic benefits assessed by this project. It is expected that future funding opportunities will
 424 result in construction of immediately feasible CRS/Low Impact Development features and zoning/code
 425 changes to enable more transformational CRS/Low Impact Development features to be constructed across
 426 the C-7 and other basins in South Florida.

Total Amount of Funding Request	Duration
\$450,000	Three Years – One Time

427 **WATERWAYS IMPACT PROTECTION EFFORT (PROJECT WIPE-OUT)**

428 The project is to assist the District in finding and piloting innovative technologies that can protect the
 429 health of water systems upstream and downstream of District conveyance structures. Currently, our
 430 waterways and canals act as a channel which collects and moves contamination that flows in from our
 431 basins. This contamination ranges from dissolved nutrients to large debris and
 432 eventually makes its way into our water bodies such as the Biscayne Bay and the
 433 ocean and their natural inhabitants. These water bodies are an essential part of the
 434 South Florida and global ecosystem. Protecting the health of these unique and
 435 fragile ecosystems will require testing different strategies and configurations until a
 436 suite of solutions is identified to be scaled across the region, as the District advances
 437 the implementation of priority resiliency projects.



444 The WIPE-Out project is part of an overall protection strategy that utilizes a Swiss cheese model of
 445 hazard and risk management. This model is used across industries from aviation to healthcare and follows
 446 the principle of layered defenses, where each layer can block risks, ultimately prevents hazards from taking
 447 place. To manage nutrient loads and eutrophication, the proposed multi-layered approach takes the form of
 448 multiple locations and technologies of nutrient removal with the goal of eventually scaling appropriate
 449 solutions until contaminants are contained within the ideal limits. Future iterations may look at the reductive
 450 effects of incorporating nature-based solutions.

451 Project WIPE-Out will be implemented in partnership with Miami Dade County and target nutrient
 452 removal via two strategies: The WIPE-Out Tech Test and the WIPE-Out Incubator. SFWMD and Miami
 453 Dade County received funding for this project in FY23 through FDEP Innovative Tech Grant. The WIPE-
 454 Out Tech Test will identify a selection of promising technologies with scaling potential to pilot in The Little
 455 River (C-7 Canal), a culturally and ecologically important canal that has been called ground zero for the
 456 challenge of removing contaminates. Every year the District removes more than 200 tons of trash from the
 457 Little River which costs the District over \$100,000. The WIPE-
 458 Out Incubator will be multi-year effort that is focused on creating local capacity through developing nutrient
 459 removal ideas in partnerships with various agencies, university, and business
 460 partners. The incubator will assist in launching new startups and
 461 potentially scalable treatment technologies by providing them
 462 with a real-world location to test their technology, free
 463 monitoring, venture building courses and programming, and
 464 access to non-dilutive seed capital, potential investors, and clients.



Trash build-up in the C-7 Canal.

Total Amount of Funding Request	Duration
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\$3M to \$4M

1.5 – 3 years -One Time

466 **FUTURE CONDITIONS DISTRICT INTERNAL RESOURCES FOR**
 467 **REGULATION**

468 The District’s Regulation Division is proposing the development of an internal tool that will give staff
 469 quick access to critical information and resources relevant to both Environmental Resource Permitting
 470 analyses and Water Use Permitting analyses, as a first step in the District’s initiatives for enhancing
 471 regulation standards to account for future climate conditions and for building resiliency into projects.
 472 Criteria currently used by the Regulation Division for evaluating permits, such as rainfall and groundwater
 473 levels, are subject to change because of non-stationary future climate projections and trends that have
 474 already been observed. This information is being incorporated into the Water and Climate Resilience
 475 Metrics Hub (Resiliency Metrics Hub (arcgis.com)) to group key parameters that will serve this purpose.

476

Total Amount of Funding Request	Duration
\$ 150,000	3 Years – One time

477

478 **CARBON STORAGE MONITORING AND REPORTING**

479 To establish routine reporting on carbon uptake and storage totals associated with ecosystem restoration
480 efforts, it is necessary to collect appropriate data for individual restoration projects. This will enable a better
481 representation of their associated mitigation benefits and estimation of resilience benefits. The following
482 data are needed:

- 483 • Soil carbon characteristics: To capture short-term and long-term carbon storage, soil bulk density
484 and carbon concentration should be measured at multiple depth increments.
- 485 • Soil accretion: To capture soil surface changes and vertical accretion, surface elevation tables and
486 feldspar marker horizons should be used to monitor soil building and erosion.
- 487 • CO₂ and CH₄ gas dynamics: To capture the direction (into the ecosystem or out to the
488 atmosphere) of gas movement and determine the net uptake of carbon at the landscape scale, eddy
489 flux towers should be used to measure the uptake and release of carbon gasses (carbon dioxide
490 and methane).

491 The District is actively investigating the potential for using satellite, radar, and lidar imagery to capture
492 changes in plant biomass and land cover, as well as to detect changes in land subsidence and topography at
493 the regional scale. Satellite and radar imagery can help the District to effectively track changes in vegetation
494 over time, differentiate between various land cover types, estimate the amount of green biomass present in
495 an area, and determine the potential for carbon uptake. These technologies would also support the detection
496 of changes in land elevation over time and aid in the mapping of topography in both urban and managed
497 natural areas across the region.

498 In the context of carbon monitoring, exploring the latest scientific publications on the use of satellite
499 and radar imagery can provide a complementary approach to enhance the District's current planning
500 projects for carbon monitoring. Bringing these additional data and analyses would further improve the
501 accuracy and efficiency of carbon monitoring. SFWMD is currently analyzing several relevant scientific
502 publications, listed below, to explore the full potential of these technologies.

- 503 • [NASA Satellites Help Quantify Forests' Impacts on Global Carbon Budget – Climate Change:
504 Vital Signs of the Planet](#): Developing an approach that integrates satellite, laser, and field data
505 can enhance the accuracy of global forest vegetation and carbon stock estimates, thereby
506 facilitating a better understanding of carbon removal rates in forest landscapes moving forward.
- 507 • [The Vegetation of Everglades National Park: Final Report \(Spatial Data\) - data.doi.gov](#): An
508 accurate and comprehensive vegetation map of Everglades National Park created using color-
509 infrared aerial imagery from 2009, providing a valuable baseline to measure the effectiveness
510 of restoration efforts associated with the Comprehensive Everglades Restoration Plan (CERP).
511 The geospatial dataset generated from this imagery will enable the monitoring of changes in
512 vegetation and help gauge the response to hydrologic modifications resulting from the
513 implementation of the CERP.
- 514 • [A Remote Sensing Technique to Upscale Methane Emission Flux in a Subtropical Peatland -
515 Zhang - 2020 - Journal of Geophysical Research: Biogeosciences - Wiley Online Library](#):
516 Developed a remote sensing approach to model CH₄ emission flux in the subtropical
517 Everglades wetland by upscaling using Landsat data and in situ model inputs to account for
518 hydrological seasonality.
- 519 • [Quantifying net loss of global mangrove carbon stocks from 20 years of land cover change |
520 Nature Communications](#): Used Synthetic Aperture Radar (SAR) global mosaic datasets to
521 estimate the net changes in the global mangrove carbon stock resulting from land cover change

522 between 1996 and 2016 to quantify proportional changes in carbon stock during processes of
 523 mangrove loss and gain due to deforestation and forestation.

- 524 • [Global hotspots of salt marsh change and carbon emissions | Nature](#): Conducted a global
 525 analysis using Landsat imagery from 2000 to 2019 to quantify salt marsh ecosystem loss, gain,
 526 and recovery due to landward migration and extreme weather disturbances and estimated the
 527 impact of those changes on blue carbon stocks.

528 By employing these measurements across District restoration projects, accurate assessments of carbon
 529 capture and storage associated with different SFWMD and partner agencies’ ecosystem restoration efforts
 530 can be made. These efforts can be leveraged to demonstrate carbon uptake potential and provide better
 531 estimates of their contribution to climate resiliency.

532 The objective of this proposed project is to establish ongoing monitoring and reporting mechanism for
 533 highlighting the benefits of District’s restoration efforts associated with carbon uptake potential. The project
 534 costs listed below do not account for expenses related to acquiring satellite, radar, or lidar data, as well as
 535 the necessary ground data monitoring required to verify the accuracy of remotely sensed data. The expenses
 536 associated with these supplementary efforts will be included in the budget at a later stage, after an approach
 537 for expanding the project to include the additional work is selected.

538

Total Amount of Funding Request	Duration
\$1,250,000 - \$2,330,000	3 Years – One time

539

540

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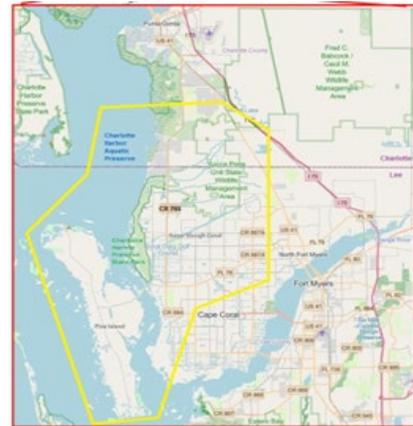
542 **DESIGNING WETLAND HABITAT ENHANCEMENT AND FLOODING**
 543 **IMPROVEMENTS FOR CHARLOTTE HARBOR FLATWOODS PROJECT**

544 This resiliency planning project links to the District’s mission to provide flood control and ecological restoration.
 545 The Designing Wetland Habitat Enhancement and Flooding Improvements for Charlotte Harbor Flatwoods project is
 546 a Florida Fish and Wildlife Conservation Commission proposal supported by the District coordinated Charlotte Harbor
 547 Flatwoods Initiative (CHFI) and part of the South Florida Water Management District’s (District) priority projects
 548 included in this Resiliency Plan. The CHFI is a multi-agency and community partnership which has been planning
 549 and implementing projects for the hydrological restoration of 85,000 acres in the Charlotte Harbor Flatwoods region
 550 since 2010. Partners include FDEP, Southwest and South Florida Water Management Districts, Florida Fish and
 551 Wildlife Conservation Commission (FWC), U.S. Fish and Wildlife Service, Florida Department of Transportation,
 552 Lee and Charlotte counties, City of Cape Coral, Coastal and Heartland National Estuary Partnership, and other
 553 community stakeholders. More on the CHFI is available at [https://chnep.wateratlas.usf.edu/charlotte-harbor-](https://chnep.wateratlas.usf.edu/charlotte-harbor-flatwoods-initiative/)
 554 [flatwoods-initiative/](https://chnep.wateratlas.usf.edu/charlotte-harbor-flatwoods-initiative/).

555 **Benefits:**

- 556 • Reduced erosion and regional flooding,
- 557 • Minimized saltwater intrusion by rehydrating the land to increase groundwater recharge.
- 558 • Increased wetland water storage, depths, and duration for habitat enhancement.
- 559 • Improved flows to Charlotte Harbor’s tidal creeks, mangroves, and seagrass beds.
- 560 • Decreased nutrient runoff pulses to estuary, reducing harmful algal blooms and protecting fisheries.

561 The project area includes Yucca Pens Wildlife Management Area
 562 (WMA), part of the largest remaining hydric pine flatwoods in southwest
 563 Florida and its tidal creeks that flow into Charlotte Harbor. The WMA’s
 564 coastal wetlands are within northern Lee and southern Charlotte Counties.
 565 The proposed project will deliver the final design and permitting for a large-
 566 scale restoration that will improve the hydrology of >8,000 acres of wetlands
 567 increasing the coastal resiliency of Cape Coral and substantially improving
 568 habitat for protected species. The design will build upon a preliminary
 569 conceptual model prioritized by Florida’s Deepwater Horizon Program and
 570 funded in 2019 through Natural Resource Damage Assessment. that
 571 simulates a appropriate timing and quantity of water flows required to improve
 572 wetland habitat conditions, minimize erosion and offsite flooding, improve
 573 groundwater recharge, and reduce the risk of wildfires. Additional modeling
 574 using future land use data, predicted population increase, climate change
 575 impacts, and SLR, as well as confirmed and potential future land acquisition and restoration projects was finalized in
 576 Sep. 2022.



577 Specifically, ditch blocks in smaller ditches would increase storage and surface water hydrology. The
 578 reestablishment of connections to several tidal creeks to the west of Yucca Pens, would be accomplished with low water
 579 fords installed through existing off-highway vehicle ruts and ditches in Yucca Pens. This will restore flows from Yucca
 580 Pens to Charlotte Harbor at several locations rather than as point source from the City of Cape Coral’s man-made Gator
 581 Slough Canal. An approximately 4.5-mile-long groundwater seepage barrier at the southern boundary of Yucca Pens
 582 along Gator Slough Canal will reduce wet season surface water drawdowns and raise groundwater levels in Yucca Pens.
 583 All would protect aquifer recharge and reduce the potential for saltwater intrusion with SLR.

584 The total project costs are around \$650,000 and a full proposal has been submitted to the Coastal & Heartland
 585 National Estuary Partnership in December 2022 and may include matching funds from FDEP and FWC. The project
 586 duration is 3 years.

Total Amount of Funding Request	Duration
\$650,000	3 Year

587 **UPPER KISSIMMEE BASIN FLOOD STUDY, ADAPTATION PLANNING** 588 **AND PROJECT RECOMMENDATIONS**

589 This resiliency planning project links to the District’s mission to provide flood control. This is a long-identified
590 need to address flood risk reduction in the Upper Kissimmee Basin and mitigate the effects of flooding, under
591 conditions that are like what was experienced during Hurricane Ian in the region. First submitted for consideration in
592 2015 under the name Central and Southern Florida Hydrologic Model Updates and Infrastructure Improvement, this
593 multiphase project is currently ranked #12 in the most recent Osceola County Local Mitigation Strategy project list.
594 Led by SFWMD, this project would involve and benefit Osceola County, City of Kissimmee, City of St Cloud, Desert
595 Ranches, Sunbridge, SFWMD and St. Johns River Water Management District. The project will be implemented in
596 3 phases which can be immediately expedited.

597 Phase 1 of this project includes updating the current SFWMD integrated watershed model for the CS&F system
598 to address unaccounted for drainage flows from outside the SFWMD boundaries. Phase 2 includes a level of service
599 impact analysis of adaptation and mitigation measures including operational changes, and nature-based, and structural
600 infrastructure modifications on flood risk. This phase will recommend for implementation, a suite of cost effective
601 and practical adaptation projects. Phase 3 consists of the necessary permitting, design, and construction activities to
602 implement the recommended projects.

603 **Modeling**

604 The Flood Protection Level of Service (FPLOS) Phase I study currently ongoing in the Upper Kissimmee Basin
605 (UKB), SFWMD will complete model update and an assessment of the flood control system, initiate and complete
606 preparation of the tools for evaluation of potential adaptation strategies, using integrated hydrologic and hydraulic
607 modeling and accounting for projections in future growth/land development in the region and climate patterns. The
608 first Phase is a modeling update to allow a robust assessment of the vulnerability of the system to flooding. The model
609 will also help verify and confirm benefits and fine tune operation of identified no-regret strategy projects proposed for
610 immediate implementation.

611 **Development of Mitigation and adaptation Strategies**

612 Working with local government and partner agencies, initiate the UKB FPLOS Phase II study to explore
613 systemwide adaptation and mitigation strategies. Identify components of the regional adaptation that can be fast
614 tracked for implementation immediately, while the project continues to determine longer term strategies and projects
615 to ensure a adequate level of service within the region consistent with the Central and Southern Florida (C&SF) Flood
616 Control project.

617 **Implement Fast-tracked Projects**

618 As soon as they are determined, initiate design, permitting and agency coordination activities to implement the
619 early identified projects.

620 **Implement Long Term Projects**

621 Following the conclusion and approval of the Phase 2, Mitigation and Adaptation Planning Study, initiate design,
622 permitting and agency coordination activities to implement the long-term flood protection strategy for the Upper
623 Kissimmee region. These may include non-SFWMD projects to be funded and executed by local government and
624 other partners.

625 **Implementation**

626 Phase 3 consists of Environmental Impact Studies and Federal approval permitting and implementation of structural
627 and operational modifications.

628

629 **Upper Kissimmee Basin Flood Study Cost Estimate**

Total Amount of Funding Request	Duration
\$3,000,000	

630 **A SURFACE ELEVATION TABLE NETWORK TO MONITOR ACCRETION**
631 **AND ADDRESS IMPACTS FROM CLIMATE CHANGE**632 ***Introduction***

633 Between the 1780s and 1980s, Florida lost 9.3 million acres of wetlands (Caffey and Schenayder 2003).
634 Wetlands are critical components of Florida’s landscape due to the many ecological services they provide.
635 For instance, mangrove and marsh systems sequester nutrients and sediment in runoff, produce and store
636 carbon in above-and below-ground biomass, fuel various food webs, serve as nurseries for many fishery
637 species, and constitute habitat for migratory birds, diamondback terrapins, bald eagles, dolphins, manatees,
638 and many other species (Mitch and Gosselink 2000). Current models suggest that another 20% of coastal
639 wetlands may be lost due to climate change (Webb et al. 2013), through the direct effects of rising sea
640 levels, and increases in flooding depths, hydroperiods, and storm intensity. Over the long term, rising seas
641 threaten to erode or sink large parts of Florida’s coastal zone (Church et al. 2001, Sklar et al. 2021).
642 However, the many projects associated with Everglades restoration (i.e., CERP) have the ability to increase
643 freshwater, brackish and saline wetland resilience by enhancing wetland accretion and carbon capture.

644 In the Everglades, mangroves and marshes have the capacity to maintain elevation via vertical accretion
645 primarily driven by belowground biogenic processes such as root production and decomposition. In some
646 other areas, elevation change may be dependent on inputs of sediment from rivers and storms (Cahoon
647 2006). However, in Florida, there is insufficient data to indicate where wetlands have the capacity to
648 maintain elevation and how much mangroves and marshes have the capacity to store carbon. Therefore, to
649 better understand the hydrological drivers of carbon capture and to better predict the effects of SLR, as part
650 of a general resiliency program, long-term soil elevation change and accretion rates are needed.

651 This accretion monitoring program, like the one built into MEME (see Figure 5-1), will study the
652 processes that effect wetland accretion, determine, and compare the rates at which they accrete, compare
653 rates of accretion in differing habitat types and geographical locations, and increase our knowledge of such
654 functions to a level needed to formulate an accurate representation, via multivariant statistical or
655 deterministic models, of the physical and biotic processes involved in elevation change. This, in turn, will
656 permit us to identify the drivers (i.e., salinity, flow, structure operations, storms, nutrients, etc.) that
657 dominate elevation change, carbon capture and resilience.

658 ***Formulation***

659 This monitoring program constitutes a critical piece of a broader, long-term effort by various state and
660 federal agencies and universities to enhance wetland resilience, sequester carbon, address the potential
661 effect of climate change, and restore the Everglades. Our strategy is to integrate the District, USGS and
662 FIU surface elevation tables (SETs) into this larger effort and insert new SET sites were most appropriate.
663 To accomplish this objective, we suggest a four-phased approach described below.

664 1. First phase is to identify and map all known SET locations in the Greater Everglades, including Big
665 Cypress and the Stormwater Treatment Areas and identify geographical gaps in monitoring coverage.

666 2. The second phase is to install SETs where coverage is poor or absent. These sites will include
667 regions that appear to maintain high accretion rates and sites that can be used as general indicators of large
668 landscapes.

669 3. The third phase is to monitor the SETs and measure changes in elevation, vegetation structure, and
670 soil composition in relation to changes in sea level, hydroperiods, nutrient inputs and water management.

671 4. The fourth phase is to analyze cause-and-effect interactions via multivariate and/or mechanistic
672 models to determine where physical processes dominate elevation change and where biotic process
673 predominate,

674 **Goal and Objectives**

675 The goal of this monitoring is to determine how water management, restoration, climate change and
676 SLR will impact accretion, carbon sequestration and wetland resilience.

677 Objectives:

678 1. Compare rates of elevation change and accretion between inland marsh, STA's, coastal marsh, and
679 mangrove habitats

680 2. Compare rates of elevation change and accretion with local rates of SLR, salinity, hydroperiods,
681 depths, flow, and landscape characteristics.

682 3. Determine primary drivers of the biotic and physical processes that are linked to accretion and
683 elevation change.

684 **Project Design and Methodologies**

685 An array of SETs and marker horizons (MH) will be installed and monitored in wetland habitats across
686 the Greater Everglades. The network of SET-MH will allow researchers the opportunity to study the
687 impacts of water management, restoration, climate change and SLR on a large regional scale. This program
688 will integrate into one database that is already funded and installed by the District, the FCE-LTER program
689 at FIU, Everglades National Park, USGS, and NOAA. Data for the entire network, District and Federally
690 funded sites, will be combined and analyzed by structural, multivariant, or mechanistic equation modeling.

691 Hypotheses:

692 1. Rates of elevation change will differ between marsh and mangrove habitats; and, with differing soil
693 types (e.g., mainly organic vs primarily sand/silt; etc.).

694 2. The biotic and physical processes of elevation change will produce differing rates of accretion and
695 will differ with anthropogenic inputs such as water management and nutrients.

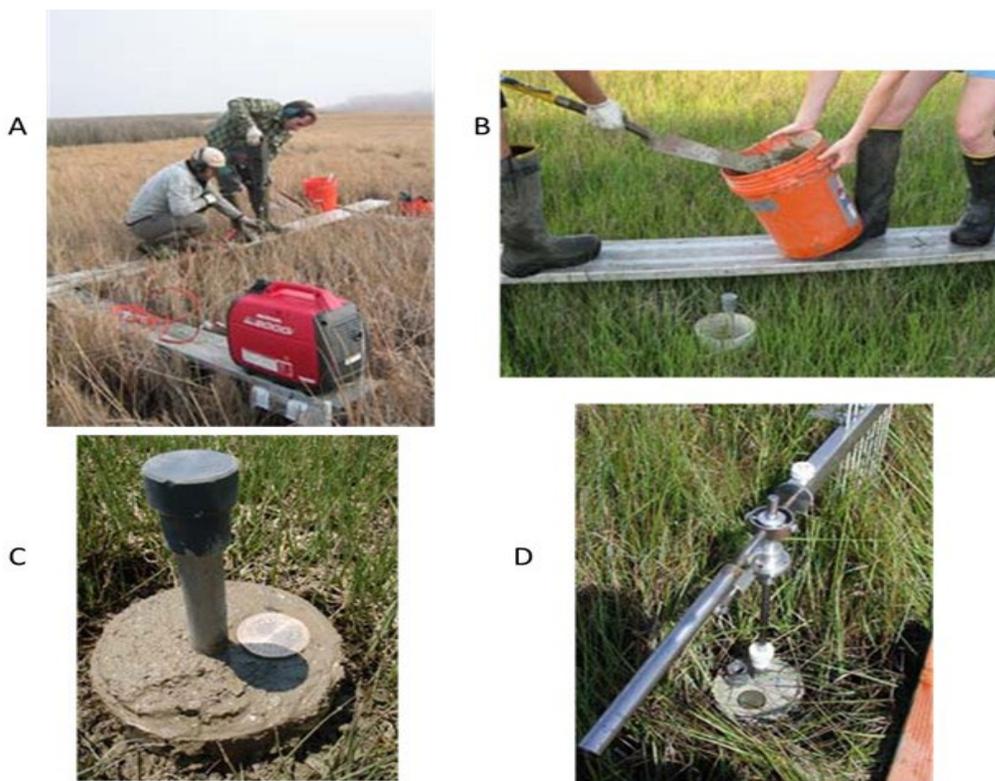
696 3. Rates of elevation change, and accretion can be enhanced to improve carbon storage, accretion, and
697 climate change resilience.

698 Surface Elevation Table technology, coupled with marker horizons of inert material such as feldspar,
699 has been used effectively in numerous wetlands to measure the rates of elevation gain and loss over a fine
700 scale (Cahoon et al. 2002 a,b). In Rookery Bay, southwestern Florida, SLR is approximately 2-4 mm/yr
701 (Cahoon and Lynch 1997). Elevations there, measured by SET, have largely kept pace with SLR, although
702 the mangrove fringe forest dominated by *Rhizophora mangle* has lagged behind the *Avicennia germinans*
703 dominated basin forest (Boumans et al. 2002). One study at Shark River, Everglades National Park, found
704 that despite Hurricane Wilma depositing 3.7 cm of new sediment, 10 mm of elevation was lost a year after
705 the storm (Whelan et al. 2009). Over longer periods of time, the increasing CO₂ concentrations associated
706 with climate change may stimulate plant growth and partially offset losses caused by changes in
707 hydroperiod (Cherry et al. 2009).

708 Due to Florida's variable soil types, tidal ranges, and dominant vegetation, understanding long-term
 709 changes in wetland soil elevation change requires study over many sites and years. Further, the ability of
 710 wetlands to keep pace with SLR that are currently transitioning from marsh to mangrove at the
 711 temperate/subtropical boundary is entirely unknown. To address these data gaps, a more regional scale
 712 approach is needed.

713 The Rod-SET is now the preferred deep SET and will be used here. SET installation and construction
 714 details are given at (Cahoon et al. 2002a,b, <http://www.pwrc.usgs.gov/set/>). Both deep (>2 m) and shallow
 715 RSETs (collectively termed SET hereafter) will be installed at each site to allow investigation on physical
 716 as well as biological (root zone) processes. SET installation and use are illustrated in Fig. 1 from D.
 717 Cahoon's USGS web site listed above.

718



719
 720 **Figure 5-1.** A. Driving rods after constructing platform. B. Cementing collar and receiver. C. View
 721 of completed receiver with brass marker. D. SET arm attached to receiver for first readings. Pictures
 722 from: <http://www.pwrc.usgs.gov/set/>

723

724 ***Expected Results, Applications and Benefits***

725 The sites proposed for SET installation in this program will fill the major geographic gaps in our
 726 understanding of wetland soil accretion and erosion throughout the greater Everglades. These new SETs
 727 will be designed and installed in a way that will tie into the already existing, but currently not centrally
 728 coordinated, SET sites in the state. Ultimately, this system will tie into a large national network such as the
 729 NOAA Sentinel Site program. Currently, there is a coordinated effort establishing a SET monitoring
 730 network in the Gulf of Mexico, Texas through the Panhandle of Florida, and Mid-Atlantic states, Virginia

731 to Georgia. The establishment of the Florida monitoring network could then be added to the existing Gulf
732 Coast and Mid-Atlantic networks to provide a standardized monitoring network from Virginia to Texas.

733

734 **FLUX TOWERS**

735 The Flux tower monitoring plan described below was developed in partnership with the Everglades
736 Foundation and Florida International University. Flux towers are micrometeorological towers that use eddy
737 covariance methods to determine the exchange rates of carbon dioxide, methane, water vapor and energy
738 between the biosphere and the atmosphere. Sensors are placed on the tower above the surrounding
739 vegetation in the mixing zone for wind current eddies between the vegetation and atmosphere. The sensors
740 allow the tower to capture the full profile of atmospheric conditions from the top of the vegetation canopy
741 to the ground. Data collected by these sensors can be used to measure carbon storage (or emission) rates of
742 a particular ecosystem.

743 Although wetland ecosystems are important globally for their capacity to sequester and store carbon
744 (C) (Aselmann and Crutzen, 1989; Whiting and Chanton, 1993), many wetlands are at risk due to
745 anthropogenic pressure, shifts in climate, and SLR (Spencer et al., 2016). In one of the most dynamic
746 wetland complexes in the world, the Florida Everglades, changes in freshwater supply and accelerated rates
747 of SLR are stressing ecosystems. Particularly striking shifts in ecosystem structure and function occurring
748 on the Everglades landscape include peat collapse (Chambers et al., 2014), establishment of non-native
749 species (Doren et al., 2009), inland encroachment of coastal woody species (Davis and Ogden, 1994), and
750 the expansion of a low productivity zone along the coast called the “white zone” (Ross et al., 2000). The
751 severity of these changes is further exacerbated by anthropogenic impacts on the quantity, quality, and
752 timing of freshwater discharge and shifts in disturbance regimes.

753 The subtropical Everglades landscape was created by strong spatial and temporal gradients of water
754 flow that formed a unique network of upland freshwater and coastal wetland ecosystems. The hydrology
755 and disturbance regime in the Everglades region developed a rich diversity of communities that have
756 variable capacities to capture and sequester carbon. Like other coastal wetland ecosystems, primary
757 productivity, respiration, and other processes in the carbon cycle change in response to climate, inundation
758 regime, and salinity.

759 In the greater Everglades region we recommend using the eddy covariance method to measure fluxes
760 of CO₂, CH₄, H₂O and energy. Long-term eddy covariance studies by scientists at FIU, include 15 years
761 of CO₂ and 8 years of CH₄ data in a marl prairie (TS/Ph-1) and freshwater marsh (SRS-2), 6 years of data
762 from a mangrove scrub (TS/Ph-7), and 18 years of CO₂ and 5 years of CH₄ from the tall riverine mangrove
763 forests (SRS-6). The network includes two recently established research sites in the estuary (Bob Allen; 2
764 years of CO₂) and at the ecotone between freshwater marl prairies and the mangrove scrub (SE-1; 3 years
765 of CO₂ and CH₄). Towers operated by the USGS were recently incorporated into the greater Everglades
766 micronet and include a pine upland (PU), cypress swamp (CS), dwarf cypress (DC) to create a transect that
767 extends from upland ecosystems to coastal wetlands and the ocean.

768 Everglades flux towers are currently managed by independent groups of investigators that contribute
769 data to the FCE-LTER and Ameriflux. While funding streams are currently independent, investigators
770 collaborate to coordinate equipment assistance and data processing assistance. Scientists at FIU and at the
771 District are currently looking for funds to organize support efforts to ensure long-term maintenance of
772 towers, equipment updating, and data processing for towers in coastal mangroves and in Shark River
773 Slough, as well as, identifying locations for new towers (e.g., an STA).

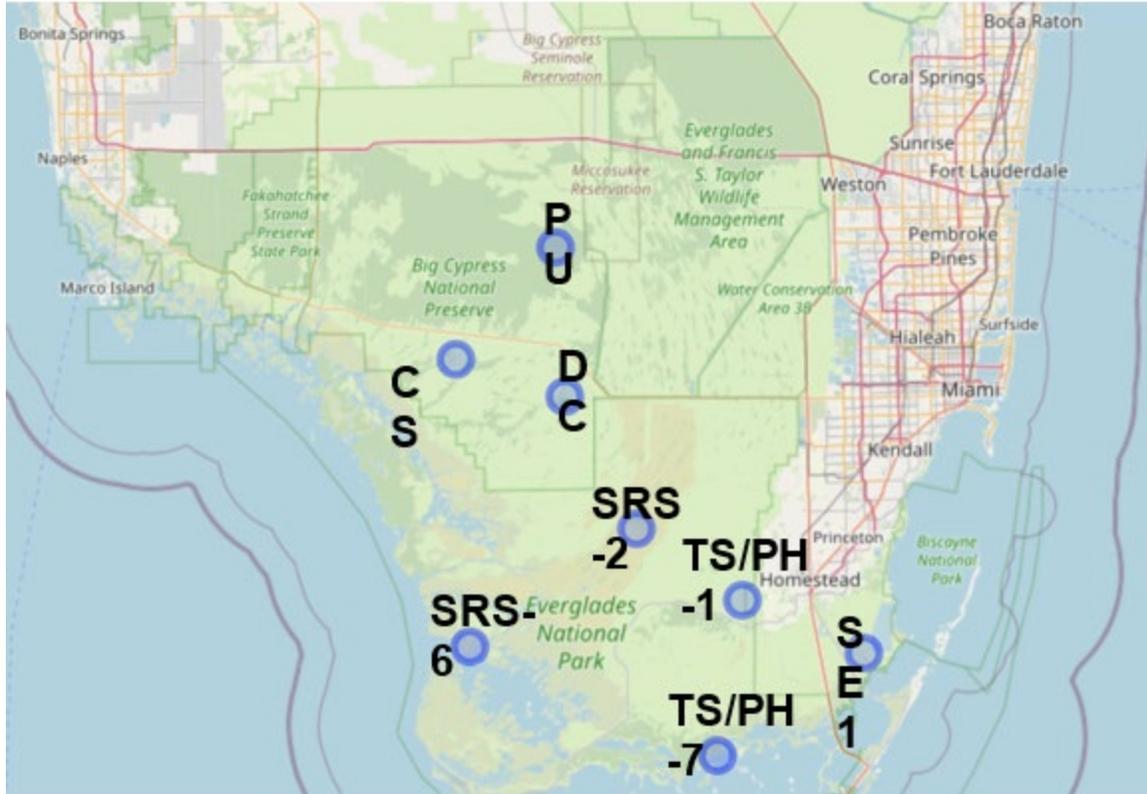


Figure 5-2: Everglades eddy covariance tower sites.

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Table 5-1: The existing towers are managed by various groups of investigators, though they have similar setups and are all associated with the Florida Coastal Everglades Long-term Ecological Research (FCE-LTER).

Tower	Investigators	ENP Permit	Network Association
SRS6	Tiffany Troxler	EVER-2019-SCI-005	FCE-LTER
TS/Ph-7	Edward Castenada Sparkle L. Malone	EVER-2019-SCI-0055	FCE-LTER
TS/Ph-1	Steven F. Oberbauer	EVER-2019-SCI-0055	FCE-LTER/Ameriflux
SRS-2	Gregory Starr	EVER-2021-SCI-0035	FCE-LTER/Ameriflux
SE-1	Christina Staudhammer	NA	FCE-LTER/Ameriflux
DC	Barclay Shoemaker	NA	FCE-LTER/Ameriflux
PU	Andrea Daniels		
CS	Sparkle Malone		

780

781 **Cost estimates**782 **Flux Towers**783 ***Instrumentation***

784 Tower instrumentation requires upgrades and replacement every 5-10 years (Table 5-2). The current
 785 priority for instrumentation is to add methane analyzers to TS-PH-7, PU, and CS. In addition to the \$90K
 786 needed to add methane to towers, an annual instrumentation budget of \$30K is necessary to replace
 787 equipment.

788 **Table 5-2:** Major instrumentation for the eddy covariance method include radiation, gas
 789 analyzers, and sonic anemometers. These costs represent the cost for deploying one flux tower.
 790 Scientists at the District and FIU are in the process of determining how many towers are needed and
 791 where they should be deployed.

Description	Instrument Used	Estimate
Shortwave/Longwave (<i>pyranometer</i>) solar radiation/terrestrial	CNR4-L net radiometer	\$28,000
Wind speed /direction	<u>05103-L Wind Monitor</u>	
Air temp and RH	<u>RAD10E</u>	
Sonic anemometer- 3D wind speed and direction		
Incoming PAR density- LI-250Q	Quantum sensor	\$1,200
LI-7500		\$78,527
LI-7700		
CR1000		\$5,000
CR3000		
	Total per tower	\$112,727

792 ***Personnel Support***

793 To support field work for the maintenance of all tower sites, a full-time technician (\$65K/ per year)
 794 will be available to assist all investigators in data collection and uploading to a general server. Data
 795 processing will be done by the Malone Disturbance Ecology Lab through the partial support of a
 796 postdoctoral scholar who will assist with data processing and research (50K/ year).

797

798 **Table 5-3:** Total annual budget for the Greater Everglades Carbon Project.

Description	Category	Estimate
LI-7700; CH4 analyzer	Equipment	90K * onetime
Repairs and replacements	Equipment	30K
Personnel	Field Technician	65K
Personnel	Data Processing	50K

Description	Category	Estimate
LI-7700; CH4 analyzer	Equipment	90K * onetime
Repairs and replacements	Equipment	30K
Personnel	Field Technician	65K
Total		145,000 /Year + 90K

799 *Overhead is not included in current estimates.

800 **Soil Accretion Monitoring**

801 It is difficult to define a total, comprehensive cost for monitoring accretion because the total number of
 802 new SET-MH sites is not yet known. However, personal experience indicates that an additional 16 sites is
 803 likely the maximum needed to capture the full suite of habitats, hydrological conditions, and water
 804 management options. This would include 2 sites in the ENP, 6 sites in WCA-3, 2 sites in WCA-2A, 3 sites
 805 in an STA and 3 sites in Big Cypress. It may be possible to acquire significant data with only 10 additional
 806 SET-MH sites. These costs below assumes that the District FTE contribution is limited to 0.4 FTE per year.

807 Phase 1: \$75,000

808 Phase 2 and Phase 3:

809 Average Installation Labor and Equipment Cost per station: \$30,000.

810 Average Annual Labor, Lab and Field Monitoring Cost per station: \$20,000

811 Year 1 Total Cost for 16 sites: \$480,000

812 Year 1 Total Cost for 10 sites: \$300,000

813 Year 2 Annual Monitoring Cost for 16 sites: \$320,000

814 Year 2 Annual Monitoring Cost for 10 sites: \$200,000

815 The Total for 5 years of monitoring is between \$1.0 and \$2.0 million.

816 Total Cost for 6 years (5-yrs of monitoring) for 16 sites: \$2,080,000

817 Total Cost for 6 years (5-yrs of monitoring) for 10 sites: \$1,000,000

818 Phase 4: \$175,000

819 Total Cost Range: \$1,250,000 -- \$2,330,000

FINAL COMMENTS AND NEXT STEPS

820

821

822 In coordination with the Florida Department of Environmental Protection, other State and Federal
823 Agencies, and local governments, the District is making infrastructure adaptation investments that are
824 needed to continue to successfully implement its mission. This plan presents a comprehensive list of priority
825 resiliency projects with the goal of reducing the risks of flooding, SLR and other climate impacts on water
826 resources and increasing community and ecosystem resiliency in South Florida. This list of projects was
827 compiled based upon vulnerability assessments that have been ongoing for the past decade. These
828 assessments utilize extensive data observations and robust technical hydrologic and hydraulic model
829 simulations to characterize current and future conditions, and associated risks.

830 The list of priority resiliency projects includes investments needed to increase the resiliency of the
831 District's coastal structures, including structure enhancement recommendations and additional SLR
832 adaptation needs. These projects represent urgent actions to address the vulnerability of the existing flood
833 protection infrastructure. Project recommendations also comprise basin-wide flood adaptation strategies
834 that are based upon other FPLOS recommendations, and water supply and water resources of the State
835 protection efforts. Important planning projects are also presented to continuously advance vulnerability
836 assessments and scientific data and research to ensure the District's resiliency planning and projects are
837 founded on the best available science and advanced technical analyses.

838 Through collaboration with local municipalities, Counties, Regional Climate Compacts, State and Federal
839 Agencies, the projects being proposed in this Plan are discussed and integrated into regional strategies to
840 promote resiliency, which include other structural and non-structural adaptation and mitigation measures,
841 flood proofing, road elevations, relocation, other local drainage improvements, shoreline stabilization, living
842 shorelines, beach restoration, ecosystem restoration, water resources protection and others.

843 Among next steps for the implementation of the project recommendations included in this plan, the
844 District continues to seek funding alternatives at the State and Federal levels. At the State level, in May
845 2021, Governor Ron DeSantis signed Florida Senate Bill 1954 which created the Resilient Florida Program,
846 providing significant funding to support flooding and SLR resiliency projects throughout the State. In May
847 2022, Governor DeSantis approved House Bill 7053 which established further efforts towards Statewide
848 Flooding and Sea Level Rise Resilience. In January 2023, Governor DeSantis signed Executive Order 23-
849 06 to direct funding and strategic action to continue to support the Resilient Florida Program. The District
850 was recently awarded approximately \$19 million from this program to support project implementation, with
851 additional funding also being awarded in partnership with Palm Beach County.

852 At the Federal level, FEMA mitigation and adaptation funding is under consideration and the District
853 is working to finalize a grant agreement with FDEM for the \$50 million award recommendation received
854 from FEMA BRIC Program for the C-8 Basin Resiliency Project. In addition, the District and USACE
855 initiated the C&SF Flood Resiliency Study, to recommend adaptation strategies to build flood resiliency in
856 the Communities served by the C&SF Systems. This Study was initiated in the Fall 2022 under the existing
857 authority of the Flood Control Act of 1970 – Section 216 and is currently leveraging advanced hydrologic,
858 hydraulic and/or hydrodynamic models, representing surface water system and associated operational rules,
859 as well as groundwater and ocean/coastal water interaction developed under the South Florida Water
860 Management District's Flood Protection Level of Service (FPLOS) Program and USACE's South Atlantic
861 Coastal Study (SACS, <https://www.sad.usace.army.mil/SACS/>). The Section 216 Study focus on the highly
862 vulnerable infrastructure that can reduce the most immediate flood risk to changing hydrodynamic and
863 climate conditions, and the resilience aspects of such infrastructure, and is being conducted in coordination
864 with stakeholders, Federal agencies, State, Tribal and local officials. USACE and the SFWMD are 50/50

865 cost-sharing partners. The results of this study will allow the immediate authorization of subsequent design
866 and construction phases and the Final Chief’s Report is estimated to be finalized by May 2026.

867 Finally, the District is committed to continue promoting regional coordination and partnership
868 opportunities by holding proactive discussions, leveraging technical knowledge, and exchanging
869 information. The SFWMD Resiliency Public Forum was kicked off in December 2022 to promote
870 collaboration on water management initiatives related to resiliency, and further engage partners on the
871 impacts of changing climate conditions and water management implications, now and into the future. This
872 forum, which meets quarterly, will continue to foster a constructive environment to discuss tangible asset-
873 level solutions and support decision making on water resource management.

874

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Appendix A.

FPLOS Phase I – Initial Project Recommendations and High Level Estimated Costs

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Appendix A: FPLOS Phase I – Initial Project Recommendations and High-Level Estimated Costs

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Canal Conveyance Improvements	C-8	N/A	N/A	C8_1	\$8,762,351	Conveyance improvements within the eastern segment of C8, downstream of its confluence with Marco Canal could help improve the current conditions FPLOS. As noted in the recent FPLOS report (Taylor, 2020), this canal segment has several bank exceedances, even for the more frequent (e.g., 10-year) design storm events. Dredging the C8 Canal to deepen and/or widen the cross section could reduce flood elevations and thus the frequency of bank exceedances. Although the effectiveness of this strategy would tend to diminish with increasing SLR and higher storm surge elevations, this strategy could be implemented in conjunction with mitigation strategy #2 to improve FPLOS in future SLR scenarios, which would serve to maintain manageable headwater elevations at S28.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Flood Walls and Storm Surge Barrier Downstream of S28	C-8	N/A	N/A	C8_3		<p>Mitigation strategy #3 is somewhat similar to Mitigation strategy #2 but would be more comprehensive and could potentially provide a higher level of flood protection under the more extreme SLR and storm surge scenarios. This strategy would involve construction of a storm surge barrier (i.e., a miter gate or sector gate) downstream of S28 in the vicinity of U.S Highway 1 (Biscayne Blvd), along with a flood wall to tie the surge barrier back into high ground. According to the USACE Back Bay Study (USACE, 2020), the associated flood wall would have to be continuous with a flood wall and storm surge barrier in the C7 Watershed.</p> <p>In order to be effective under the more extreme SLR scenarios, levees and/or flood walls may have to incorporate seepage barriers due to the extremely high permeability of the underlying Biscayne Aquifer. Without such barriers, the porous limestone of the Biscayne could provide a subsurface pathway for tidal waters to flow underground, seeping into the canals upstream of the floodwalls and surge barriers whenever the tides are higher than canal stages.</p> <p>Assessing the feasibility of seepage barriers will require a detailed analysis of the site(s) geology. Seepage barriers are expected to be costly in this environment. Due to the limestone geology, sheet pile walls may not be feasible. Seepage cut-off walls could possibly be constructed using a sequence of drilled shafts or specialized bedrock-cutting equipment similar to that currently employed in the rehabilitation of the Herbert Hoover Dike (Bruce, 2009). Furthermore, this strategy may require additional seepage management infrastructure (seepage collection canals and pumps) on the inland side of the seepage barriers in order to collect and discharge fresh groundwater to tide.</p> <p>Another possible refinement to this strategy would involve co-locating the surge barrier with the gated control structure (S28) and/or a forward pump station. The current plan presented in the USACE Back Bay study calls for a</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>separate surge barrier some distance downstream of S28. If the surge barrier, rebuilt S28, and forward pump station could all be co-located, there may be opportunities to improve the operational flexibility of the system over the current plan, such as having the ability to pump down C-8 when the surge barrier is closed. Thus the structure could serve dual purposes of conveying rainfall-induced runoff while protecting against storm surge.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Raise levees along C-8 canal and add gates / pumps on the secondary branches	C-8	N/A	N/A	C8_4	\$248,791,563	If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canals at acceptable levels, it may be necessary to consider raising the levees along the primary canals and constructing new gated structures and/or pumps on the secondary canals to achieve an acceptable level of flood protection. The FPLOS report shows the flood depth differences for the 25-year event with no mitigation measures (3-foot SLR minus current conditions), along with conceptual locations of potential new gated structures and pump stations on existing secondary canals at their confluence with the primary canals. Also shown on this report are areas that currently drain directly to the primary canals. Because these areas would not be protected by improvements on secondary branches, they would require modifications to the stormwater collection system to either (a) re-route the drainage to a nearby secondary branch, or (b) re-route the drainage to new municipal pump stations (not shown). Although the extensive drainage modifications this would require may render this strategy infeasible basin-wide, this option was included for completeness or as an option to be considered for targeted areas. Initial Cost estimates include adding pump stations for the Miami-Dade Co. tributary canals to the C8 Canal
Connect Western Mine Pits South of C9 Canal to the C9 Canal	C-9	N/A	N/A	C9_1	\$92,401,883	Connect Western Mine Pits South of C9 Canal to the C9 Canal. Construction of a 1000 cfs immediately west of SW 173rd Ave. Construct backup generator power for C9 Lake Belt forward Pump Station
Oleta River Storm Surge Barrier	C-9	N/A	N/A	C9_2	\$14,576,015	This strategy would include a surge barrier on the Oleta River to the north of S29. The Oleta River barrier would cut off a potential pathway for storm surge to bypass the S29 and enter the C9 basin from the north and west through a swath of urbanized lowlands. A more comprehensive (and more costly) version of this strategy that would provide a higher level of flood protection could also be considered for the C9 Basin. This would be similar to the strategy of flood walls and surge barriers discussed as Mitigation Strategy #3 for the C8 Basin.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Raise levees along C-9 Canal and add gates / pumps on the secondary branches	C-9	N/A	N/A	C9_3	\$322,493,438	This strategy is similar to mitigation strategy #4 in the C-8 basin. If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canals at acceptable levels, it may be necessary to consider raising the levees along the primary canals and constructing new gated structures and/or pumps on the secondary canals to achieve an acceptable level of flood protection. Conceptual locations of potential new gated structures and pump stations on existing secondary canals at their confluence with C-9. As in C-8, areas draining directly to C-9 would not be protected by improvements on secondary branches and would require additional modifications to the stormwater collection systems to either (a) re-route the drainage to a nearby secondary branch, or (b) re-route the drainage to new municipal pump stations (not shown). Although the extensive drainage modifications this would require may render this strategy infeasible basin-wide, this option was included for completeness or as an option to be considered for targeted areas. Initial cost Estimates include only new pumps to secondary branches (Station estimate based on \$50k/cfs incl all dewatering, structure const, site work, elec., I&C, and mechanical.) and not raising canal banks.
Increase Connectivity Between C-9 and C-11	C-9	N/A	N/A	C9_4		This strategy was identified by the South Broward Drainage District (SBDD) as a way to increase operational flexibility. In particular, enlarging the Silver Lake Control Structure would facilitate the movement of water into C-11 Basin from SBDD S5 Basin or vice versa depending on relative water levels within the two canals.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Structure S-37B improvements	Broward County	C-14 Basin	The C-14 West Basin has been assigned a 5-year FPLOS rating for SLR1 and less than 5-year FPLOS rating for SLR2 and SLR3. For all return period design storm and sea level rise scenarios simulated, the first FPLOS deficiency that is predicted to occur is flooding of a gravity-drained area that has topographic elevation lower than the peak stage in the C-14 Canal. As return period and sea level rise increases, other deficiencies are predicted to occur such as bank exceedance. Much of the C-14 West Basin is drained by pumps or is	BC_2.1		Although Structure S-37B is not a tidal structure, it is expected to be impacted by sea level rise. As storm surge and sea level rise propagate upstream of Structure S-37A, higher tailwater levels will be seen at Structure S-37B. Higher tailwater levels at Structure S-37B result in decreased discharge and higher stages in the C-14 Canal. One possible improvement to S-37B is the addition of a pump station. However, this addition would only be feasible with major modifications to Structure S-37A also, otherwise it would worsen downstream flooding between S-37B and S-37A. Structural or operational modifications to structure S-37B alone would not be beneficial as Structure S-37B is not predicted to be overtopped and maintains positive head differential during the simulated sea level rise scenarios. Structure improvements at S-37B may be avoidable with a combination of modifications to Structure S-37A, which will be needed anyway, and secondary system improvements, which later studies may determine to be more cost effective as the FPLOS deficiencies are very localized and not widespread.



Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Add gates / pumps on the secondary system	Broward County		protected by the embankments along the C-14 Canal.	BC_2.2	\$129,800,461	As part of the PM #5 analysis presented in Deliverable 4.2A, Taylor Engineering compared peak canal stages with land surface topography elevations. A significant area of the C-14 West Basin has topographic elevations that are lower than the simulated peak canal stages, however, much of it is drained by pumps (areas such as Coral Springs and Tamarac). Areas drained by pumps can continue to discharge when downstream water levels are higher (unless required by permit to stop when the downstream stages exceed a threshold stage), so they are of less significance for the purposes of the PM #5 evaluation. However, areas that are drained by gravity are unable to drain whenever downstream water levels are higher than the land surface elevation. In the C-14 West Basin, one area in particular was identified as being drained by gravity and having land surface elevations lower than the peak stage where it drains to the C-14 Canal. This area, mainly roads in North Lauderdale, between N University Dr and S State Road 7 (Hwy 441), would benefit from the addition of operable structure(s), whether it be to actively drain when downstream water levels are elevated or to prevent the elevated C-14 Canal from backing up into secondary system. The FPLOS report shows conceptual locations of potential new gated structures or pump stations on existing secondary canals at their confluence with the primary canals. Cost estimates include: Replace the existing control structure for flows into the WCA-2 with a 2000 cfs gated spillway and Construction of a 2000 cfs immediately east of the Sawgrass Expy, including backup generator

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Raise levees at selected locations on the C-14 Canal	Broward County			BC_2.3		As part of the PM #1 analysis presented in Deliverable 4.2A, Taylor Engineering compared peak canal stages with canal bank elevations. Although the C-14 Canal is predicted to mostly contain the 100-year return period design storm within its banks for all three sea level rise scenarios simulated, there are a few localized locations of exceedance. Of the three locations with significant bank exceedance levels, only one is predicted to directly result in inundation of developed lands, which was the metric used to identify deficiencies in this study. The FPLOS Report shows the location proposed for canal bank improvements. The proposed bank improvement would involve raising about 1200 linear ft of the 1700 ft section shown on the north side of the canal to form a more elevated continuous embankment.
Canal dredging in areas with significant head loss	Broward County			BC_2.4		One potential way to reduce stages in the C-14 Canal would be to dredge the canal in areas with significant head loss. The canal bottom profile can be compared to the canal design bottom elevation to identify areas with sediment accumulation. Based on the 25-year design storm simulation results, there is a predicted head loss of about 0.60 ft to 0.74 ft (decreasing as SLR increases) over the 9400 ft stretch of canal between the Sunshine WCD PS1 outfall and South State Road 7, and 1.0 ft to 1.23 ft (decreasing as SLR increases) over the 13500 ft stretch of canal between South State Road 7 and Structure S-37B. These areas could benefit from dredging if the existing canal conditions have deteriorated compared to the design conditions. Regardless of whether the existing canal conditions in these areas have deteriorated compared to design, it is possible that deepening the canal to improve conveyance could reduce peak canal stages.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Raise levees on the Cypress Creek Canal	Broward County	C-14 East Basin	The C-14 East Basin has been assigned a 10-year FPLOS rating for SLR1 and less than 5-year FPLOS rating for SLR2 and SLR3. Under SLR1 scenario, the 25-year design storm is predicted to produce peak canal stages that exceed bank elevations and inhibit gravity-driven drainage. Under SLR2 and SLR3 scenarios, the 5-year design storm is predicted to produce peak canal stages that exceed bank elevations and inhibit gravity-driven drainage. As return period and sea level rise increases, so does the predicted occurrences of bank exceedance as well as the area and duration of flooding. The C-14 East Basin is drained by gravity and is therefore sensitive to stage in the Cypress Creek Canal. To reduce flooding and increase the level of service provided for the C-14 East Basin, Taylor Engineering recommends evaluation of the following two potential flood mitigation projects:	BC_3.2		If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canals at acceptable levels, it may be necessary to consider raising the levees along the primary canal to reduce overland flooding as a result of bank exceedance. However, this strategy alone would not reduce flooding as a result of elevated stages in the primary canal inhibiting gravity-driven discharge from the secondary system. Therefore, this mitigation strategy could be implemented as necessary in select locations that would still experience bank exceedance after Structure S-37A Improvements (mitigation strategy 1) have been implemented, which can be determined through future model simulations.
Canal dredging in areas with significant head loss	Broward County			BC_3.3		One potential way to reduce stages in the Cypress Creek Canal would be to dredge the canal in areas with significant head loss. The canal bottom profile can be compared to the canal design bottom elevation to identify areas with sediment accumulation. Based on the 10-year design storm simulation results, there is a predicted head loss of about 0.3 ft over the 1 mile stretch of canal between W Palm Aire Drive and FL-845 (Powerline Road) and 0.2 ft over the 3500 ft stretch of canal between FL-845 and the Train Tracks Bridge.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Culvert Modification	Broward County		The Pompano Basin has been assigned a less than 5-year FPLOS rating for all SLR scenarios simulated. The Pompano Canal is predicted to contain the 100-year SLR3 design storm event within its banks with no instances of bank exceedance. However, the canal stage resulting from even the 5-year SLR1 scenario is predicted to result in water backing up and spilling out of the secondary system, as well as inhibiting gravity-driven drainage of developed areas in some localized areas. The Pompano Basin is drained by gravity and model simulations indicate that it would be sensitive to extremely sensitive to sea level rise. As return period and sea level rise increases, so does the overland flood depth and duration in many areas. To reduce flooding and increase the level of service provided for the Pompano Basin, Taylor Engineering recommends evaluation of the following three potential flood mitigation projects:	BC_4.1		The results of the future conditions FPLOS assessment indicate that the culvert immediately upstream of G-57 is at least partially responsible for the elevated stages in the Pompano Canal. This 10 ft diameter culvert, which is approximately 1450 ft in length, is predicted to have approximately 1.5 to 4.0 ft of head loss depending on the specific return period and sea level rise scenario. Depending on the specific scenario, this head loss is more significant than the effects of sea level rise. Therefore, although Structure G-57 experiences overtopping / bypass, improving the conveyance capacity of this section of the canal may prove to have more impact than G-57 improvements alone. However, to maximize flood protection improvement, modification of this culvert could be done in conjunction with Structure G-57 improvements.
Divert Water Through C-14 West / C-14 East Basin	Broward County	POMPANO BASIN	<ul style="list-style-type: none"> • Culvert modification: Increase the conveyance capacity / decrease the head loss through the culvert immediately upstream of 	BC_4.3		If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canal at acceptable levels, it may be necessary to consider diverting water from the Pompano Basin to the C-14 West Basin, which will ultimately pass through the C-14 East Basin to tide. However, as the C-14 West Basin and the C-14 East Basin are predicted to be affected by sea level rise, diverting water to them would likely only be feasible after structure improvements at S-37B and S-37A are implemented. It may be more effective to divert water through Structure S-37B and Structure S-37A, which will both likely need improvements anyway to protect the large area they serve, than to perform some level of improvement at Structure G-57 and the culvert immediately upstream in addition to the C-14 Basin projects. These potential strategies should be further investigated and analyzed in future studies.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
			Structure G-57 • Structure G-57 improvements • Divert water through C-14 West / C-14 East Basin			
Raise levees along the C-13 Canal and add gates / pumps on secondary branches	Broward County	C-13 WEST BASIN	The C-13 West Basin has been assigned a 25-year FPLOS rating for SLR1, 10-year rating for the SLR2, and less than 5-year rating for SLR3. Under SLR1 scenario, the 100-year design storm is predicted to produce peak canal stages that exceed bank elevations and inhibit gravity-driven drainage. Under SLR2, the 25-year design storm is predicted to produce peak canal stages that exceed bank elevations and inhibit gravity-driven drainage. Under SLR3, the 5-year design storm is predicted to produce peak canal stages near the tidal structure that are higher than larger return periods storms under smaller sea level rise, which highlights the C-13 West Basin’s sensitivity to sea level rise.	BC_5.2		If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canals at acceptable levels, it may be necessary to consider raising the levees along the C-13 Canal and constructing new gated structures and/or pumps on the secondary canals to achieve an acceptable level of flood protection. The FPLOS report presents conceptual locations of potential new gated structures and pump stations on existing secondary canals at their confluence with the primary canals. Gravity structures such as gated culverts, sluice gates, or flap gates are different types of structures that could be considered to prevent flood water from propagating upstream.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
			<p>Per District operational criteria, the S-36 tidal structure closes whenever the tailwater elevation comes within 0.1 ft of the headwater elevation. Due to the increased tailwater elevation associated with sea level rise, the S-36 structure is predicted to close often to prevent storm surge from propagating upstream. Although this prevents storm surge from propagating upstream, it does not completely prevent increased stages upstream, as the C-13 Canal stage will increase due to being unable to discharge to tide when the Structure S-36 is closed.</p>			
Structure Operation Modification	Broward County	NORTH NEW RIVER WEST BASIN	<p>The North New River West Basin has been assigned a 100-year FPLOS rating for SLR1, 25-year for SLR2, and 10-year for SLR3. North New River is predicted to contain the 100-year SLR1, 25-year SLR2, and 10-year SLR3 storm events within its banks with no instances of bank exceedance and little to no overland flooding resulting directly from the elevated canal stages. The 100-year SLR2 and 25-year SLR3 design storms are almost completely contained within bank, however, there is one localized area where</p>	BC_7.1		<p>Based on District-provided structure operations (SFWMD H&H Bureau, 2020), Structure G-54 opens when the headwater elevation exceeds 4.5 ft NGVD29 and does not close until the headwater falls below 3.5 ft NGVD29. As such, once the structure is opened, it remains open when downstream water levels are higher than upstream water levels as long as the upstream water levels have not fallen below 3.5 ft NGVD29, which only occurs for the SLR1 scenarios. It is possible that peak upstream canal stages can be reduced by changing the standard operating criteria. One potential modification that should be further analyzed is closing the gate whenever the downstream elevation is within 0.1 ft of the headwater elevation, as is done with other District tidal outfall structures in Broward County. This operation or a similar set of operating criteria relating to closing the structure if tailwater exceeds headwater would be necessary if a pump station is added, as discussed in Section 8.2. In addition, if structure operations are modified so that the structure closes, the</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
			<p>even the small exceedance would contribute to overland flooding of developed areas. Per District operational criteria listed in the Water Control Operations Atlas for Eastern Broward County (SFWMD H&H Bureau, 2020), the G-54 tidal structure opens whenever the headwater elevation is greater than 4.5 ft NGVD29 and does not close when the downstream water level is elevated. This simulated operation results in elevated upstream water levels and instances of flow reversal. It is possible that closing the structure when downstream levels are within 0.1 ft of the headwater elevation would have similar results to current conclusions as storm surge would overtop Structure G-54, but it should be further analyzed.</p>			<p>gated structure would need modification, which is also discussed in Section 8.2.</p>
<p>Raise Levees at Select Location(s)</p>	<p>Broward County</p>		<p>even the small exceedance would contribute to overland flooding of developed areas. Per District operational criteria listed in the Water Control Operations Atlas for Eastern Broward County (SFWMD H&H Bureau, 2020), the G-54 tidal structure opens whenever the headwater elevation is greater than 4.5 ft NGVD29 and does not close when the downstream water level is elevated. This simulated operation results in elevated upstream water levels and instances of flow reversal. It is possible that closing the structure when downstream levels are within 0.1 ft of the headwater elevation would have similar results to current conclusions as storm surge would overtop Structure G-54, but it should be further analyzed.</p>	<p>BC_7.3</p>		<p>If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canal at acceptable levels, it may be necessary to consider raising the canal levees to reduce overland flooding as a result of bank exceedance. For the North New River Canal, only one instance of bank exceedance was predicted during the future condition simulations (upstream and downstream 124th Ave (N Flamingo Rd)), which was the primary deficiency that impacts the assigned flood protection level of service. Raising the segment of canal embankment identified in Deliverable 4.2B would increase the level of service and is likely a very feasible project to implement. The proposed bank improvement would involve raising about 2800 linear ft of the 3600 ft section shown on the north side of the canal to form a more elevated continuous embankment. It is possible that this strategy would not be required if Structure G-54 follows salinity control operations discussed in Section 8.1, which future modeling simulations can address.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Canal dredging in areas with significant head loss	Broward County			BC_7.4		One potential way to reduce stages in the North New River Canal would be to dredge the canal in areas with significant head loss. The canal bottom profile can be compared to the canal design bottom elevation to identify areas with sediment accumulation. Based on the 25-year design storm simulation results, there is a predicted head loss of about 0.3 ft to 0.83 ft (decreasing as SLR increases) over the 3 mile stretch of canal between Hiatus Rd and N University Dr (FL-817), and 0.14 to 0.46 ft (decreasing as SLR increases) over the 7000 ft stretch of canal between N University Dr and Structure G-54. These areas could benefit from dredging if the existing canal conditions have deteriorated compared to the design conditions. The head loss through the North New River Canal should be analyzed again after the salinity control operations discussed in Section 8.1 have been included in future model simulations. Dredging in areas with significant head loss may eliminate the need to raise the embankment, which could be analyzed in the next phase of this FPLOS study.
Lower water control elevation of primary canal	Broward County	C-11 WEST BASIN	The C-11 West Basin has been assigned a 10-year FPLOS rating for all SLR scenarios. Although the C-11 Canal is expected to contain the 100-year storm event within its banks with no instances of bank exceedance, the elevated canal stage would decrease the gravity drainage ability of the secondary system, contributing to flooding of	BC_8.1		The C-11 West Basin is controlled at a water elevation of 4.0 ft NGVD29. Lowering the control water level in the western segment of the C-11 Canal (upstream / west of Structure S-13AW) may help buffer the peak rainfall and result in overall lower stages in the primary system. As this basin is drained by pumps at the western end of the C-11 Canal, lowering the control elevation would need to be implemented with modification to the standard operating procedure, otherwise the primary canal system would fill back up prior to peak rainfall. However, lowering the control elevation and maintaining the lower stages pre-storm with the pumps may reduce flooding to some extent.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Improve C-11 conveyance capacity / operation modification	Broward County		<p>developed areas. To reduce flooding and increase the level of service provided for the C-11 West Basin, Taylor Engineering recommends evaluation of the following four potential flood mitigation projects:</p> <ul style="list-style-type: none"> • Lower water control elevation of primary canal • Improve C-11 conveyance capacity / operation modification • Add gates / pumps to the secondary system • Use the existing inter-basin connection with C-11 East <p>Although there is a large pump station already draining the C-11 West Basin, it is already at maximum capacity in accordance with the non-Everglades Construction Project permit (SFWMD H&H Bureau, 2020).</p>	BC_8.2		<p>One potential way to reduce the duration of flooding is to increase the conveyance capacity of the C-11 Canal so that the pump has less “down-time”. Based on standard operating criteria, the S-9/S-9A Pump Station reduces discharge when the headwater drops below 1.0 ft NGVD29 and may turn off completely if the water elevation drops below 0.0 ft NGVD29 until the minimum pool elevation is re-established. Increasing channel conveyance capacity could increase the water level upstream of the pumps which would allow them to stay at peak discharge longer, as well as reducing upstream water levels. One potential way of improving canal conveyance is to dredge the primary canal (back to design condition in areas with significant head loss of sediment deposition) or deepen the canal beyond design conditions. Based on the future condition simulations, this strategy would not likely reduce peak flood depths as the pumps are at peak capacity during those times. However, it could reduce the duration that the primary canal is elevated, ultimately reducing the duration of flooding.</p>
Add gates / pumps to the secondary system	Broward County		<p>Therefore, instead of increasing the capacity of the pump station, a potential flood mitigation project would be to provide it more opportunity to discharge at its maximum capacity, either by improving channel conveyance capacity or by modifying the</p>	BC_8.3		<p>If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canals at acceptable levels, it may be necessary to consider constructing new gated structures and/or pumps on the secondary canals to achieve an acceptable level of flood protection. Due to the large number of connection points between the primary and secondary system, it is likely not feasible to add a pump station to each one. However, it is possible that some strategic combination of gates and pumps could be implemented to reduce flooding and increase the level of service. Adding gates to the secondary canals at their confluence with the primary canals would prevent water from backing up into the secondary system during times of peak stage and pump stations placed on secondary canals with the most connectivity could actively drain the secondary system.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Use the existing inter-basin connection with C-11 East	Broward County		standard operation criteria. These are further discussed in Section 9.2.	BC_8.4		Between the C-11 West Basin and the C-11 East Basin exists Structure S-13AW, which is an inter-basin connection. For the purposes of the FPLOS design storms, this structure remained closed. The intended purpose of this structure is to discharge excess water from the C-11 West Basin to tide when capacity is available in the C-11 East Basin. One potential way to reduce flooding in the C-11 West Basin is to divert some flood water to tide through the C-11 East Basin. However, this would only be feasible if structure modifications were implemented to increase the discharge potential of the C-11 East Basin tidal structure. As the maximum discharge capacity of the S-9/S-9A pump station is limited, the most obvious way to remove flood water from the C-11 West Basin is to discharge it to tide by increasing the maximum capacity of the S-13 tidal structure. However, modifications to the S-13 structure alone may not be sufficient enough and the primary canal conveyance may need to be improved through dredging (back to design condition) or deepening in some sections. Improvements to the S-13 structure are further discussed in Section 10.2.



Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Structure S-13 Improvements Option 1	Broward County	C-11 EAST BASIN	The C-11 East Basin has been assigned a 5-year FPLOS rating for all SLR scenarios. Although the C-11 Canal is expected to contain the 100-year storm event within its banks with no instances of bank exceedance, the elevated canal stage would decrease the gravity drainage ability of the secondary system, contributing to flooding of developed areas.	BC_9.1		Structure S-13 is the tidal outfall structure for the C-11 East Basin and is composed of a pump station and an underflow gate. Regardless of gate position, water will bypass this structure at an elevation of 8.0 ft NGVD29 (SFWMD H&H Bureau, 2020), which was not predicted to occur based on District-provided storm surge data. However, the S-13 peak tailwater used for the 100-year SLR3 scenario is within 0.04 ft of bypassing/overtopping the structure. The S-13 underflow gate closes whenever the tailwater elevation gets within 0.1 ft of the headwater elevation. Under future condition sea level rise, the S-13 tailwater stage will often exceed the headwater stage, which forces the underflow gate to remain closed, which significantly reduces the discharge. Structure improvements would involve re-building or modifying the S-13 structure to include more (or larger) forward pumps and increase the heights of the platform to reduce the potential for overtopping/bypass. Due to the low elevation of the C-11 East Basin, sea level rise will likely make a gravity structure such as the S-13 underflow gate impractical. Although the gate is still able to discharge at times during the simulated sea level rise design storms, it does so with upstream water level elevations that cause flooding. Therefore, to reduce flooding and increase FPLOS, increased pump capacity is required.
Structure S-13 Improvements Option 2	Broward County			BC_9.2		Structure S-13 improvement option 1 involves sizing the upgraded/modified pump station to handle the needs of the C-11 East Basin alone. S-13 improvement option 2 involves sizing the upgraded/modified pump station to handle not just the needs of the C-11 East Basin, but also some needs of the C-11 West Basin. The discharge out of the C-11 West Basin through the S-9/S-9A pump station is limited based on the non-Everglades Construction Project permit. However, discharge to tide is only limited to what the infrastructure can handle. As modifying Structure S-13 is likely required to protect the C-11 East Basin from sea level rise, it may be possible to also increase the level of service for the C-11 West Basin at the same time with one project.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Add Gates / Pumps to the Secondary System	Broward County			BC_9.3		<p>If, in the future SLR scenarios, it is no longer feasible or cost effective to maintain stages in the primary canals at acceptable levels, it may be necessary to consider constructing new gated structures and/or pumps on the secondary canals to achieve an acceptable level of flood protection. Due to the large number of connection points between the primary and secondary system, it is likely not feasible to add a pump station to each one. However, it is possible that some strategic combination of gates and pumps could be implemented to reduce flooding and increase the level of service. Adding gates to the secondary canals at their confluence with the primary canals would prevent water from backing up into the secondary system during times of peak stage and pump stations placed on secondary canals with the most connectivity could actively drain the secondary system. In the C-11 East Basin, the secondary system is mostly composed of north/south drainage canals and does not have many east/west canals connecting them. Therefore, increased connectivity and conveyance between the secondary system would be needed to minimize the number of secondary system pump stations.</p>



Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Improvements in Primary Canals C-1W and C-1	South Miami-Dade	Watershed C-1	<p>The C-1 Watershed has been assigned a 10-year FPLOS rating for SLR0 and SLR1 and 5-year FPLOS rating for SLR2 and SLR3. The primary reason for rating the watershed as a 10-yr and 5-yr LOS is due to canal bank exceedance. The following infrastructure projects are suggested to maintain and improve the LOS of watershed C-1:</p> <ol style="list-style-type: none"> 1. Improvements in Primary Canals C-1W and C-1. 2. Upgrades of coastal structure S21 and potential new tidal structure at the Goulds Canal outfall to Biscayne Bay. 3. Upgrades of inland structures S148 and S149. 4. Installation of backflow prevention measures and devices. 5. Installation of control structure at the crossing of Cutler Wetland C-1 Flow Way and the eastern levee. 6. Improvements to elevation requirements of levees at the eastern boundary of the C-1 watershed. 7. Development of local flood mitigation projects in collaboration with Miami-Dade County. <p>The numerical model can be</p>	SMD_2.1		<p>The improvements in Primary Canals C-1W and C-1 may include maintenance and dredging to provide an even bottom gradient from the west to the east and an upgrade of canal bank top elevations to eliminate overtopping. An example of the canal profiles and the deficiencies along the canals for 25-yr design event and SLR 0, 1, 2 and 3 is provided in the Report.</p> <p>The canal profiles show exceedance of canal banks on multiple locations for design events with a return period greater than 5-yr and 10-yr and an increase of SLR. In addition, the report shows that there is a water divide in canal C-1W at approximate chainage 5.5 which suggests that the cross sections of the C-1W may require widening to allow flow to the west (to canal L-31N). Structure S-338 closes depending on the flooding conditions downstream in the C-1 basin. Opening of the structure may cause additional flooding. Any changes for flood operations to this structure will be dependent on downstream flood conditions, therefore additional analysis is recommended to provide a better understanding of effects of redirecting flow to the west.</p> <p>Improvements in Canals C-1W and C-1 will involve:</p> <ul style="list-style-type: none"> • Increase of canal bank elevation above the stage of the 25-yr 3-day design event within the Urban Development Boundary and at locations where flooding damages may occur as result of overtopping of the canal banks. • Maintenance of canals C-1W and C-1, and potential dredging to improve the canal bottom gradient and minimize hydraulic losses <p>Considering that dredging and changing the elevations of the original canal bottom profiles could be prohibitively expensive for the entire canal, additional hydrographic surveys of the C-1N and C-1 canals and cross sections are recommended (C-1W canal already has a detailed cross section survey which has been implemented in the model). The new hydrographic surveys will be used to update the model cross sections, and additional simulation are suggested to determine locations where the canal bottom profile or cross section configurations may cause head</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
			extended to provide analysis of the suggested projects and evaluate the effect of each project on the LOS for current and future conditions.			losses due to constriction or sedimentation and determine canal sections that may require deepening or widening.
New tidal structure at the Goulds Canal outfall to Biscayne Bay	South Miami-Dade	Watershed C-1		SMD_2.3	\$14,140,467	Additional consideration should be given to future urbanization of the agricultural areas which are in the vicinity of Goulds Canal. Future land use which is marked as Agriculture. If the agricultural areas become developed, significant runoff contribution will be expected into Goulds Canal, which may additionally require a tidal structure to accommodate discharges from urbanized areas.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Upgrades of inland structures S148 and S149	South Miami-Dade	Watershed C-1		SMD_2.4		<p>The inland structures will require:</p> <ul style="list-style-type: none"> • Increase of conveyance capacity of Canal C-1N by increasing the capacity of Structure S149 (currently 400 cfs), considering that flooding and canal overtopping has been observed upstream of S149 in canal C-1N. • Upgrade heights of the S149 platform and gates. Currently stages of 7.5 NGVD 29 (6.0 ft NAVD) can by-pass the structure. • Upgrade heights of the S148 platform and gates. Currently stages of 9.0 NGVD 29 (7.5 ft NAVD) can by-pass the structure.
Installation of backflow prevention measures and devices		Watershed C-1		SMD_2.5		Installation of backflow prevention devices to protect the secondary and tertiary system from backflow from the primary canal system particularly for increased SLR and storm surge conditions which can create high stages in the primary canals.
Installation of control structure at the crossing of Cutler Wetland C-1 Flow Way and the eastern levee.	South Miami-Dade	Watershed C-1		SMD_2.6		The planned Cutler Wetland C-1 Flow Way will require a control structure to avoid backflow during storm surge as discussed in the analysis of Future Conditions (Task 5.2, Section 3.1.4). Proposed structures may include a set of gated box culverts with parameters which will be based on additional analysis of flow rates and stages determined from selected design events and SLR scenario.
Improvements to elevation requirements of levees at the eastern boundary of the C-1 watershed.		Watershed C-1		SMD_2.7		<p>Levee overtopping caused by storm surge can result in significant backflow in the C-1 watershed and increased upstream flood potential. Therefore, raising the top of the levees up to the 25-yr 3-day design event storm elevation at locations on the C-1 Watershed Canal within the Urban Development Boundary would be necessary.</p> <p>Elevation improvements of all levees at the eastern boundary of the C-1 watershed to 7.5 ft (NAVD 88) plus the necessary freeboard would be required. For example, near Goulds Canal, the levee will require an upgrade with a recommended top of the levee of 7.5 ft. (NAVD 88) plus required freeboard (based on the peak stages for the 100-yr event and +3 ft SLR).</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Development of local flood mitigation projects in collaboration with Miami-Dade County.	South Miami-Dade	Watershed C-1		SMD_2.8		<p>The proposed mitigation areas are based on the flood depth greater than 1.0 ft for the 25-yr 3-day design event and flood depth greater than 2.5 ft for the 25-yr 3-day design event.</p> <p>Based on the Flood Extent and Duration Maps (PM5 and PM6) for the 25-yr 3-day storm event and +3 ft SLR, the C-1 Watershed areas within the Urban Boundary Line will require flood mitigation.</p> <p>To analyze the impacts of SLR on the urban drainage, the difference of the flood rasters for SLR 3 and SLR 0 were used to determine the greatest impact of SLR within the watershed. The SLR 0 depth raster depth was subtracted from the SLR 3 depth raster and differences were classified into 3 categories: i) less than 1 ft SLR impact, ii) SLR impact between 1 and 2 feet and SLR impact greater than 2 feet. The FPLOS report shows the areas impacted by SLR change from +0 to +3 ft. The major impacts are within the wetland areas which are interconnected within the drainage system and more specifically the primary canals. The figure shows that the SLR impacts for most of the urban areas (except for the areas highlighted with yellow and red colors) is not expected to be significant for a SLR change from 0 to 3. The FPLOS Report additionally shows the locations within watershed C-1 which will experience increased flooding with SLR and will require drainage improvements.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Improvements in Primary Canals C-100, C-100A, C-100B.		Watershed C-100	The C-100 Watershed has been assigned a 5-year FPLOS rating for SLR0 and SLR1 and less than 5-year FPLOS rating for SLR2 and SLR3. The primary reason for these ratings is due to canal bank exceedance along several locations along the C-100 Canal. The following projects are recommended for evaluation as potential flood mitigation projects: 1. Improvements in Primary Canals C-100, C-100A, C-100B. 2. Upgrades of coastal Structure S123. 3. Backflow prevention. 4. Increase in elevation of all levees at the eastern boundary of the C-100 watershed. 5. Development of local	SMD_3.1		Considering that changing the original canal bottom profile design could be prohibitively expensive for the entire canal, additional hydrographic surveys of the cross sections are recommended. The hydrographic surveys can be used to update the model cross sections, and additional simulation are suggested to determine locations where the canal bottom profile may cause head losses due to constriction or sedimentation. Improvements in Canals C-100, C-100A and C-100B involve: <ul style="list-style-type: none"> • Increase of C-100B canal bank elevation above the peak stage of the 25-yr 3-day design event within the Urban Development Boundary and at locations where flooding damages may occur as result of overtopping of the canal banks. • Maintenance and dredging of canals C-100A and C-100B for selected locations to improve the canal bottom gradient at locations which potentially have negative bottom gradient or higher hydraulic losses than average • An example of the canal profiles is provided in the report. The canal profiles show exceedance of canal banks on multiple locations of canal banks of C-100A and C-100B within the Urban Development Boundary of Miami-Dade County.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Upgrades of coastal Structure S123.	South Miami-Dade	Watershed C-100	flood mitigation projects in collaboration with Miami-Dade County. The numerical model can be extended to provide an analysis of the suggested projects and evaluate the effects of each project on the LOS for the current and future conditions. The improvements in Primary Canals C-100, C-100A, C-100B may include maintenance and dredging to provide an even bottom gradient from west to east and an increase of the canal bank elevations to eliminate overtopping.	SMD_3.2		Structure S123 is a two-gate spillway structure with a design flow of 2,300 cfs at 40% SPF, for a 0.5 ft head differential and a tailwater at 1.5 ft (0.0 ft NAVD 88). The major deficiency of this structure for SLR and storm surge conditions is the low by-pass level which is listed as 8.0 ft NGVD 29 (approximately 6.5 NAVD 88). For example, the structure will be by-passed for the 25-yr and 100-yr Storm events for SLR 2 and 3. Figure 17 shows the computed headwater elevations at Structure S123 for the 25-yr and 100-yr events and SLR 0, 1, 2 and 3 ft. Figure 18 illustrates the locations of the C-100 canal banks which have an elevation deficiency and will allow overtopping of the canal. The structure is rated at 5,000 cfs at 100% SPF with head differential of 0.8 ft at tailwater of 2.0 ft NGVD 29 (0.5 NAVD 88) and may require increased peak flow capacity for future SLR and storm surge conditions, and to maintain the peak headwater to design conditions (1.3 ft NAVD). The upgrades of structure S123 include: <ul style="list-style-type: none"> • Installation of a new pump facility which will require additional analysis to optimize flow rates, pump location, downstream effects, funding, local conditions, selected return period of design events, criteria for SLR, freeboard and storm surge elevations. • Increase the heights of the platform and gates above 7.5 ft NAVD plus freeboard. • Improvements to the levees north and south of the structure to be above 7.5 ft (currently the lowest points are 6.03 ft. (NAVD) and potential overtopping can occur).
Backflow prevention.		Watershed C-100		SMD_3.3		Installation of backflow prevention devices are necessary to protect the secondary and tertiary system from backflow from the primary canal system, particularly for increased SLR and storm surge conditions, which can create high stages in the primary canals.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Development of local flood mitigation projects in collaboration with Miami-Dade County.	South Miami-Dade	Watershed C-100		SMD_3.4		Based on the Flood Extent and Duration Maps, the C-100 Watershed areas within the Urban Boundary Line which will require flood mitigation, based on the flood depth greater than 1.0 ft and 2.5 ft for the 25-yr 3-day design event, are depicted in the yellow colored areas. Additionally, the difference of the flood rasters for SLR 3 and SLR 0 were used to determine the greatest impact of SLR within the watershed. The SLR 0 depth raster depth was subtracted from the SLR 3 depth raster. The differences were classified into 3 categories: i) less than 1 ft impact, ii) impact between 1 and 2 feet and iii) impact greater than 2 feet. The FPLOS report also shows that the SLR impacts for most of the urban areas (except for the areas highlighted with yellow and red colors) is not expected to be significant for SLR change from 0 to 3. The locations within watershed C-100 which will experience increased flooding with increasing SLR and will require drainage improvements are detailed in the report.
Improvements in Primary Canals C-102 and C-102N		Watershed C-102	The C-102 Watershed has been assigned a 5-year FPLOS rating for SLR0 and SLR1 and less than 5-year FPLOS rating for SLR2 and SLR3. The primary reason for rating the watershed as 5-yr and less than 5-yr is due to canal bank exceedance. The following projects are recommended for evaluation as potential flood mitigation projects: 1. Improvements in Primary Canals C-102 and C-102N. 2. Upgrades of coastal structure S21A. 3. Backflow prevention devices. 4. Installation of a control	SMD_4.1		Improvements in Primary Canals C-102 and C-102N may require maintenance and dredging to provide an even bottom gradient from west to east and an increase of canal bank elevations to eliminate overtopping. Considering that changing the original canal bottom profile design could be prohibitively expensive for the entire canal, additional hydrographic surveys of the cross sections are recommended. The hydrographic surveys can be used to update the model cross sections, and additional simulations are suggested to determine locations where canal bottom profile may cause head losses due to constriction or sedimentation. Improvements in Canals C-102 and C-102N involve: <ul style="list-style-type: none"> • Increase of canal bank elevation above the stage of the 25-yr 3-day design event within the Urban Development Boundary and at locations where flooding damages may occur as a result of overtopping of the canal banks. • Maintenance of Canals C-102 and C-102N to ensure a consistent canal bottom gradient which will minimize the hydraulic losses.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
			<p>structure at the eastern levee crossing of conveyances.</p> <p>5. Improved elevation of all levees at the eastern boundary of the C-102 watershed.</p> <p>6. Development of local flood mitigation projects in collaboration with Miami-Dade County.</p> <p>The numerical model can be extended to provide an analysis of the suggested projects and evaluate the effects of each project on the LOS for current and future conditions.</p>			An example of the canal profiles and the deficiencies along the canals C-102 and C-102N is provided in the report.
Backflow Prevention	South Miami-Dade	Watershed C-102		SMD_4.3		Installation of backflow prevention devices will be necessary to protect the secondary and tertiary system from backflow from the primary canal system particularly for increased SLR and storm surge conditions which can create high stages in the primary canals.
Installation of control structures at Levee L31E	South Miami-Dade	Watershed C-102		SMD_4.4		Information from SFWMD suggests that 10 culverts and 5 pump stations will be constructed on Levee L-31E for future planned water deliveries to the wetlands east of the levee. All culverts will require controlled gates to prevent backflow from Biscayne Bay during tidal and storm surge events.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Retrofitting Levees		Watershed C-102		SMD_4.5		The top elevation of the L-31E levee between Structures S20G and S21A. The profile shows that the levee elevation can be overtopped at multiple locations for peak stages greater than 5.5-6.0 ft. Overtopping of Levee L-31E can result in significant backflow in the C-102 watershed, increased flooding potential upstream and considerably slower drainage of the flooded areas. Therefore, upgrading the levee to 7.5 ft NAVD plus required freeboard is recommended (7.5 ft NAVD is based on the headwater peak stages for the 100-yr design event and SLR +3.0 ft).
Local Mitigation projects	South Miami-Dade	Watershed C-102		SMD_4.6		Based on the Flood Extent and Duration Maps (reported in PM5 and PM6), the C-102 Watershed areas within the Urban Boundary Line which will require flood mitigation, based on the flood depth greater than 1.0 ft for the 25-yr 3-day design event and flood depth greater than 2.5 ft for the 25-yr 3-day design event. Additionally, the difference of the flood depth rasters for SLR +3 and SLR +0 were used to determine the greatest impact of SLR within the watershed. The SLR 0 depth raster depth was subtracted from the SLR 3 depth raster and differences were classified into 3 categories: i) less than 1 ft SLR impact, ii) SLR impact between 1 and 2 feet and SLR impact greater than 2 feet. The report shows the areas impacted by SLR from 0 to 3 ft. The major impacts are within the wetland areas which are interconnected with the drainage system. The FPLOS report shows that the SLR impacts on the urban areas is not expected to be significant for SLR from 0 to 3, however there are multiple locations within the watershed which experience flooding, and which will require mitigation such as conveyance improvements, coastal structure upgrades, and backflow prevention. FPLOS report shows the locations within watershed C-102 which will experience increased flooding with increasing SLR and will require drainage improvements.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Improvements in Primary Canals C-103 and C-103N	South Miami-Dade	Watershed C-103	The C-103 Watershed has been assigned a 5-year FPLOS rating for SLR0 and SLR1 and less than 5-year FPLOS rating for SLR2 and SLR3. The primary reason for rating the watershed as 5-yr and less than 5-yr is due to canal bank exceedance. The following projects are recommended for evaluation as potential flood mitigation projects: 1. Improvements in Primary Canals C-103 and C103N. 2. Upgrades of coastal structures S20F and S20G. 3. Backflow prevention devices. 4. Installation of a control structure at levee L-31E. 5. Improved elevation of all levees at the eastern boundary of the C-103 watershed.	SMD_5.1		The improvements in Primary Canals C-103 and C-103N considers improved maintenance and dredging at locations with high head losses to provide an even bottom gradient from west to east, and upgrades of the canal banks to eliminate overtopping. <ul style="list-style-type: none"> An increase of C-103 canal bank elevation above the stage of the 25-yr 3-day design event, within the Urban Development Boundary and at locations where flooding damages may occur as a result of overtopping of the canal banks. Maintenance of canals C-103 and C-103N to ensure consistent canal bottom gradient which will minimize the hydraulic losses. An example of the canal profiles is provided in the FPLOS report Considering that dredging of the original canal bottom profile design could be prohibitively expensive for the entire canal, additional hydrographic surveys of the cross sections are recommended. The hydrographic surveys can be used to update the model cross sections, and additional simulation are suggested to determine locations where the canal bottom profile may cause head losses due to constriction or sedimentation
Backflow Prevention		Watershed C-103	6. Development of local flood mitigation projects in collaboration with Miami-Dade County.	SMD_5.3		Installation of backflow prevention devices are necessary to protect the secondary and tertiary system from backflow from the primary canal system particularly for increased SLR and storm surge conditions which can create high stages in the primary canals.
Installation of Control Structures at Levee L31E		Watershed C-103	The numerical model can be extended to provide an analysis of the suggested projects and evaluate the effect of each project on the	SMD_5.4		Information from SFWMD suggests that 10 culverts and 5 pump stations will be constructed on Levee L-31E for future planned water deliveries to the wetlands east of the levee. All culverts will require controlled gates to prevent backflow from Biscayne Bay during tidal and storm surge events.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Retrofitting Levees	South Miami-Dade	Watershed C-103	LOS for current and future conditions.	SMD_5.5		Overtopping of the levee can result in significant backflow in the C-103 watershed which will also result in considerably slower drainage and increased upstream flood potential. Therefore, upgrading the levee to 7.5 ft NAVD plus required freeboard are recommended. The top elevation of the L-31E levee between structure S20G and Florida City Canal. The profile shows that the levee elevation can be overtopped at multiple locations for peak stages greater than 5.0-6.0 ft.
Local Mitigation projects		Watershed C-103		SMD_5.6		Based on the Flood Extent and Duration Maps (reported in PM5 and PM6), the C-103 Watershed areas within the Urban Boundary Line which will require flood mitigation based on the flood depth greater than 1.0 ft for the 25-yr 3-day design event and flood depth greater than 2.5 ft for the 25-yr 3-day design event. There are multiple locations within the watershed which experience flooding, and which will require mitigation such as conveyance improvements, coastal structure upgrades and backflow prevention. Additionally, the difference of the flood depth rasters for SLR +3 and SLR +0 were used to determine the greatest impact of SLR within the watershed. The SLR 0 depth raster depth was subtracted from the SLR 3 depth raster and differences were classified into 3 categories: i) less than 1 ft SLR impact, ii) SLR impact between 1 and 2 feet and iii) SLR impact greater than 2 feet. FPLOS Report shows the areas impacted by SLR from 0 to 3 ft and the locations within watershed C-103 which will experience increased flooding with increasing SLR and will require drainage improvements.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Downstream C-7 Basin OBS: These projects were detailed back in 2018 and associated cost estimates are now outdated.	C-7	N/A	N/A	C7_1		<p>Measures include the following: ID; Measure; Unit Cost; Dimensions M1; Total Costs; Remarks A- Flood walls; \$1500 per linear foot; 36568 feet; \$54,852,000; Assuming 30 feet depth B- Exfiltration trenches; \$1500 per linear foot; 170,293 feet; \$25,543,950 C- Backflow preventers; \$70,000 per piece; 16 pieces; \$1,120,000; Range of \$10,000 to \$100,000 D- Pumps; \$30,000 per cfs; 3,300 cfs; \$99,000,000; Range of 3>0 to 30,000 per CFS</p> <p>Total: \$180,515,950</p> <p>Note: For the M1 scenario, it was assumed that 3,300 cfs pump capacity would be needed. In practice this was less, as about 3,137 cfs maximum capacity was simulated. However, the 3,300 cfs was used for the cost calculation. Only construction costs are considered; operation and maintenance costs for the pumps are not included.</p>
Elevation to 6 feet (NGDV29) for all buildings and roads OBS: These projects were detailed back in 2018 and associated cost estimates are now outdated.	C-7	N/A	N/A	C7_3.1		<p>ID; Unit Costs of Elevation; Dimensions; Total Costs A- Buildings; \$50,000 per building; 736; \$36,800,000 B- Roads; \$500 per linear foot elevation; 240,156; \$120,078,206</p> <p>Total: \$156,878,206</p>
Elevation to 7 feet for all buildings and roads OBS: These projects were detailed back in 2018 and associated cost	C-7	N/A	N/A	C7_3.2		<p>ID; Unit Costs of Elevation; Dimensions; Total Costs A- Buildings; \$50,000 per building; 1,730; \$86,500,000 B- Roads; \$500 per linear foot elevation; 367,964; \$183,982,245</p> <p>Total: \$270,482,245</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
estimates are now outdated.						
Elevation to 8 feet for all buildings and roads OBS: These projects were detailed back in 2018 and associated cost estimates are now outdated.	C-7	N/A	N/A	C7_3.3		ID; Unit Costs of Elevation; Dimensions; Total Costs A- Buildings; \$50,000 per building; 3,432; \$171,600,000 B- Roads; \$500 per linear foot elevation; 474,458; \$237,229,000 Total: \$408,829,000
All buildings elevated to the maximum 100-year flood levels under scenario SLR3, and all roads to the 10-year flood level under scenario SLR3 (scenario M3(x)). OBS: These projects were detailed back in 2018 and associated cost estimates are now outdated.	C-7	N/A	N/A	C7_3.4		ID; Unit Costs of Elevation; Dimensions; Total Costs A- Buildings; \$50,000 per building; 2,932; \$146,600,000 B- Roads; \$500 per linear foot elevation; 284,197; \$142,098,530 Total: \$288,698,530

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Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Canal Improvements L-31NS	C-111	L-31NS	<p>The L-31NS Watershed has been assigned a 5-yr FPLOS rating for the future hydrologic conditions. For this overall rating, weight was placed on PM1, as the primary canals in this watershed collectively are expected to contain the 5-yr storm event within its MIKE 1D right and left banks as modeled.</p> <p>The results of this analysis showed that most of the canals in L-31NS Watershed can convey the 5-yr event without overflowing for CSL. Multiple short sections of which canals were identified that overflow during the 10-yr and 25-yr flood events for a short period of time. For the 100-yr event all L-31NS watershed canals have cross sections which allow bank overflows. L-31N canal, which is the upstream portion of the watershed L-31NS canal system has a higher flood protection level of service than the remaining canal system. Overall, the L-31NS Watershed canals provide 5-yr LOS based on the most limiting factor which is 5-yr for canal L-31N, which may cause overbanking over the east bank of the canal. Within increasing SLR, the LOS of the canals is nearly constant.</p>	C111_1.1		<p>Retrofitting and increasing the eastern canal bank elevation of L-31NS can provide significant reduction of flood extent and duration within the agricultural areas of the watershed and increase of the FPLOS rating to greater than the watershed 5-yr rating. While the SLR does not significantly increase the flood extent, the flood duration increased with SLR and rainfall return period.</p> <p>Installation of forward pump at structure S176 is recommended for additional analysis to increase the drainage capacity of this section of canal L-31N to compensate for the reduced hydraulic gradient between S176 and the outfall of canal C-111 for the conditions of SLR3.</p> <p>Development of local flood mitigation projects and addition of secondary canals at the locations with highest flood duration parameters is recommended. Additional local drainage improvements such as the addition of ditches and local pumps to improve the drainage rate to the L-31N Canal are recommended.</p>
Forward Pump S176				C111_1.2		
<p>Local Mitigation projects:</p> <ul style="list-style-type: none"> -Upgrades of canal banks top elevations - Interconnectivity improvements -Backflow control for high stages in outfalls -Green infrastructure projects -Exfiltration trenches and drainage wells -Upgrades in capacity of secondary canal system -Additional pumping -Additional storage and retention reservoirs 				C111_1.3		

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Addition of Secondary Canals				C111_1.4		
Local Drainage Improvements (Ditches and local pumps)				C111_1.5		
Improvements in Primary Canals	C-111	C-111 AG	The C-111 AG Watershed has been assigned a 5-yr FPLOS rating for the current hydrologic conditions. For this overall rating, weight was placed on PM1, as the primary canals in this watershed collectively are expected to contain the 5-yr storm event within its MIKE 1D right and left banks as modeled.	C111_2.1		<p>Retrofitting and increasing the low elevations of the eastern canal bank elevation of C-111 Ag can provide significant reduction of flood extent and duration within the agricultural areas of the watershed and increase of the FPLOS rating to greater than the current watershed 5-yr rating.</p> <p>Installation of forward pump at structure S177 is recommended for additional analysis to increase the drainage capacity of this section of canal C-111 in order to compensate for the reduced hydraulic gradient between S177 and the outfall of canal C-111 for the conditions of SLR3. Analysis will be provided for simultaneous pump operation at structures S176 and S177.</p> <p>Development of local flood mitigation projects and installation of secondary canals is recommended as well. Local drainage improvements to reduce flood duration, addition of ditches and local pumps to C-111 Canal are recommended.</p>
Forward Pump S177				C111_2.2		
Local Mitigation projects: -Upgrades of canal banks top elevations - Interconnectivity improvements -Backflow control for high stages in outfalls -Green infrastructure projects -Exfiltration trenches and drainage wells -Upgrades in capacity of secondary canal system				C111_2.3		

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
-Additional pumping -Additional storage and retention reservoirs						
Addition of Secondary Canals				C111_2.4		
Local Drainage Improvements C111 Canal (Ditches and pumps)				C111_2.5		
Extension of Levee L-31E Southwest	C-111	US1 Watershed	The US1 Watershed has been assigned a no FPLOS rating considering that the watershed is unprotected from the south and there are no agricultural areas, and the urban areas small fraction (35 acres from total of 16,803 acres, mostly located on high ground).	C111_3.1		The US1 Watershed has been assigned a no FPLOS rating considering that the watershed is unprotected from the south and there are no agricultural areas, and the urban areas small fraction (35 acres from total of 16,803 acres, mostly located on high ground). However, during storm surge, watershed US 1 is unprotected from the coast and the storm surge propagates considerably north thus creating potential flooding of Card Sound Road. Therefore, a potential extension of Levee L-31E from the junction with Card Sound Road to the boundary between watershed US 1 and C-111 South is recommended for analysis to determine protection from storm surge events and overtopping during high tide for future conditions of SLR

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Upgrades and retrofitting of Levee L-31E	C-111	MODEL LAND Watershed	Watershed MODEL LAND has been assigned less than 5-yr FPLOS Rating for current and future hydrologic conditions because of extensive flooding which occurs for events with return frequency greater than 5-yr. The watershed is surrounded by levees, a small fraction is agriculture (205 out of 18,390 acres), and the urban areas small fraction (52 acres from total of 18,390 acres, mostly located on higher ground). The watershed is entirely outside of the Urban Development Boundary and no future development is expected. Furthermore, overtopping of Levee L31E and Card Sound Rd is not observed for current conditions as shown in Figure 542 through Figure 549 which show the profile of the peak stages along L-31E canal and Card Sound Road Canal for all SLR and Design Event Scenarios.	C111_4.1		The watershed is surrounded by levees, with a small fraction of agriculture (205 out of 18,390 acres), and urban areas (52 acres from total of 18,390 acres, mostly located on higher ground). Upgrades and retrofitting of Levee L-31E are recommended to prevent overtopping of the levee and long retention times of flooded areas. Additionally, installation of forward pump at structure S20 can reduce the flood duration in the watershed.
Installation of forward pump at Structure S20	C-111			C111_4.2		



Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
S22 hardening (Raise the overtopping and bypass elevations, add tie-back levees/floodwalls)	C-2	Eastern (Tidal)	Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the C2 watershed can handle up to the 10-year storm event, which was primarily due to road exceedance at culvert locations and canal embankment overtopping along the canals, as explained in PM#1. For the SLR1 condition, similar results to the current conditions 10-year storm were found for not only culverts and canal embankments, but also overland flooding depth and duration. All greater SLR conditions and storm events showed significant increases in canal flooding, as discussed in PM#1, and direct flooding from the canals to the overland, as discussed in PM#5 and PM#6. Therefore, it is determined that the overall level of service provided by this watershed for future SLR conditions is the SLR1 5-year storm. No other SLR conditions have passing storms.	C2_1.1		Structure S22 is a two-bay, reinforced concrete gated spillway located about 7,000 ft from the mouth of Biscayne Bay, in the Snapper Creek Canal (C2 Canal). The discharge from the structure is controlled by two electric driven cable drum operated vertical lift gates. The S22 tidal structure operates with the intention to maintain optimum water levels in the C2 Watershed and pass 100% of the Standard Project Flood (SPF) without exceeding upstream flood design stage. The structure is also used to restrict downstream flood stages and discharge velocities to protect downstream areas, as well as prevent saline intrusion during periods of high tides. Figure 2-1 shows a picture of the structure. Table 2-1 shows the design parameters for S22 as provided in the Water Control Operations Atlas. Suggested upgrades to mitigate the effects of SLR are as follows: 1) Increase the existing structure elevation (including gates and platform) to prevent overtopping 2) Install a forward pump station to help reach the design discharge capacity of 1905 cfs while gravity discharge capacity is limited under storm surge and SLR conditions 3) Add tieback levees and floodwalls to prevent flooding of the area and short-circuiting of the water around the structure, also known as structure flanking
Forward pump station				C2_1.2		

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Canal re-alignment				C2_1.3		<p>The tidal section of the Snapper Creek Canal from the S22 structure to the Biscayne Bay is primarily within the R Hardy Matheson County Preserve, and is currently a straight line from the structure to the Bay; however, the historical channel followed a more natural path, winding northeast, splitting and rejoining along the way to the coast, as shown in Figure 2-3 (Miami-Dade County, 2012). This natural pathway may have reduced the wave energy coming from storm surge and tidal surge.</p> <p>By increasing the number of bends in the existing canal and/or re-aligning the canal to follow a more natural pathway, the wave energy should be reduced, and storm related surge may be less intense at the S22 structure. Some examples of these canal re-alignments are shown in Figure 2-4 A and B. Any changes to the mangrove and coastal vegetation communities may require habitat restoration and/or wetland mitigation.</p> <p>Canal conveyence capacity for the section of the Snapper Creek Canal downstream of the S22 structure will require further evaluation and modeling to determine the effects on downstream stages.</p> <p>In addition, canal and shoreline stablization can be implemented using living shoreline techniques along the areas highlighted in purple in panel C of Figure 2-4. Living shorelines utilize natural edging to increase stability along coastlines (NOAA, 2015). Since this area is already a mangrove habitat, stabilization here may mean adding oyster beds and breakwater habitats to reduce erosion and impact to these mangrove habitats.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Raising canal embankments in problem areas		Central (Upland)	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the C2 watershed can handle up to the 10-year storm event, which was primarily due to road exceedance at culvert locations and canal embankment overtopping along the canals, as explained in PM#1. For the SLR1 condition, similar results to the current conditions 10-year storm were found for not only culverts and canal embankments, but also overland flooding depth and duration. All greater SLR conditions and storm events showed significant increases in canal flooding, as discussed in PM#1, and direct flooding from the canals to the overland, as discussed in PM#5 and PM#6. Therefore, it is determined that the overall level of service provided by this watershed for future SLR conditions is the SLR1 5-year storm. No other SLR conditions have passing storms.</p>	C2_2.1		<p>Raising the elevation of the canal banks will help reduce overtopping of embankments from the canals to the overland elevations during the peak of the storm events. For the C2 Watershed there are several locations where raising the embankments can provide immediate relief during extreme rainfall and surge events with high canal stages. To review the deficiency of these embankment heights, a comparison was made with the 2022 Miami-Dade County Flood Criteria map, which is based on a 10-year, 24-hour storm event, 2060 scenario with SLR. Figure 2-5 shows the difference of the modeled embankment elevations minus the Miami-Dade Flood Criteria (MDFC) map elevations. In the figure, embankment elevations that are less than a foot above the MDFC are colored with greens and blues, and therefore less urgent in their potential upgrades. Reds and oranges are more urgent, as these embankment locations are much lower than the MDFC. The following areas (also indicated in the figure with yellow dashed lines) may benefit from embankment improvements:</p> <ol style="list-style-type: none"> 1. Snapper Creek Canal <ol style="list-style-type: none"> a) Low sections along SW 117th Ave on the eastern embankment from Coral Way to N Snapper Creek Dr b) Low Sections along N Snapper Creek Dr on the north embankment and along the south embankment c) Low portion from S.R. 826 to Ludlam Glade Canal d) Low section upstream of SW 57th Ave Bridge near SW 88th Ste) Low section upstream of S22 structure 2. SW 60th St Canal – southern embankment from SW 127th Ave to the Turnpike 3. SW 144th Ave Canal – full canal 4. Westwood Lakes Canal – full canal

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Temporary storage in parks/golf courses				C2_2.2		<p>To provide additional storage within the watersheds, Miami-Dade County parks or golf courses can potentially be used as emergency temporary storage. A majority of these parks are at lower elevations than average grade. Green infrastructure can be implemented at these parks to allow for recreational use during dry periods while also being able to provide storage during storm events. The C2 Watershed has few non-urban areas and recreational areas that may be considered for use as temporary storage areas during extreme rainfall events. As previously mentioned, the Miccosukee Country Club along SW 60th St Canal is in-line with the secondary canal and may already have naturally lower embankments that likely provide some floodplain storage. However, this golf course could be enhanced to provide additional dry detention, and/or regraded to allow the canal to overflow onto the natural areas. A map of the Miami-Dade County Parks, municipal parks, and golf courses are provided for the C2 and C3W watersheds in Figure 2-6. Some parks have also been identified in the C2 Watershed that can provide a similar service. These include:</p> <ol style="list-style-type: none"> 1. Tamiami Park – although this park is in the C4 Watershed, this location could take overflow from Snapper Creek on the west side across NW 117th Ave 2. Kendall Indian Hammocks Park – this large park is not adjacent to any canal, but additional connections could be considered and/or storm drain pipes can provide canal connections 3. Boys and Girls Club of Miami fields – these fields are located at the Snapper Creek Canal and the Don Shula Expressway 4. West Matheson Hammock Park and others – several natural areas in the South Miami/Pinecrest area are adjacent to the Snapper Creek Canal and may provide additional storage due to their naturally low topography (includes Dante Fascell Park, Banyan Drive Park, Red Road Linear Park, etc.)

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Municipal pump station (including pumping from Ludlam Glade contributing basin up to Coral Gables Canal)				C2_2.3		<p>Most of Miami-Dade drains via gravity drainage from the neighborhood and street level culverts out to a secondary or primary canal. However, when stages in these canals increase due to sea level rise and storm events, there is less opportunity for water to drain out via gravity and the duration of storm events can increase significantly. To counter these effects, subbasins where gravity drainage will be less possible can implement a municipal pump to pull the water out of existing stormwater drainage infrastructure and pump into the canals. Similar municipal pumps have been implemented in such municipalities as Sweetwater, the City of Miami, and unincorporated Miami-Dade County in the C4 Watershed, as well as in the City of West Miami in the C3W Watershed, and can be repeated for other low-lying subbasins in the C2 watershed. Physical requirements of the pump station must be achievable for the sub-basin, this includes the retrofitting or construction of an adequate collection system and the available space required for a wet well with pump station housing located near the primary canal. In addition, the implementation of any municipal pump discharging to the primary canal would require that a) the canal levees are raised to meet the minimum appropriate elevations, and b) that there are future connections to planned storage areas or the C4 Impoundment. These requirements will be addressed in subsequent studies if municipal pumps are selected as an alternative for flood mitigation.</p> <p>Several locations in the C2 Watershed may benefit from municipal pump stations, including: A- South of FIU Campus and north of SW 49th B- West of the Southern Estates community, east of SW 132nd Ave and north of Bird Drive C- Kendal Lakes east of SW127th Ave and west of the Turnpike D- Near Kendall Rd (SW 88th St) and the Don Shula</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						Expressway, north of Baptist Hospital. This can also utilize the Snapper Creek Lake and CS-1, which controls water levels in the lake. E- South Miami/Pinecrest near the Hammocks F- Ludlam Glades Canal contributing areas

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Evaluating undersized culverts				C2_2.4		<p>Some culverts within secondary canals may not be sufficiently sized for conveying flows during extreme rainfall events and may need to be upsized. At an initial review, culverts that impacted upstream stages may include those located at:</p> <ul style="list-style-type: none"> • Bird Drive Canal (SW 144th Ave, SW 132nd Ave) • SW 60th St Canal (SW 163rd Ct, SW 162nd Ave, SW 132nd Ave, SW 146th Ave, SW 137th Ave, SW 132nd Ave)
Extend SW 157th Avenue Canal to the C4 Canal				C2_2.5		<p>During the future conditions analysis, the planned canals from Miami-Dade County (Miami-Dade County, 2021) were implemented into the model network to anticipate development of future drainage infrastructure. The planned canal along SW 157th Avenue was added to the network (this canal can be found in Figure 2-12), connecting the Bird Drive Extension Canal to the C4 Canal just upstream of District structure S380. This connection, along with other inter-basin connections to the C4 Canal, showed a reversal of flows when the C4 Impoundment pumps turn on. This new connection caused a reduction in stages west of SW 144th Ave, as shown in the peak stage profile in Figure 2-11 for the existing (blue) and future SLR conditions for the 25-year storm event.</p> <p>Since this planned canal already showed an improvement in stages to the west, it is recommended that this remain as a flood mitigation strategy.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>In addition, the amount of water that is being pulled from the planned canal into the C4 Impoundment can be regulated with additional controls at the S380 structure. If gate operational strategies can't provide the level of control that is needed for this new connection, potential upgrades to the S380 structure should be considered (see Section 5.3.1).</p>
<p>Sub-dividing the C2 Watershed to increase discharge potential</p>				<p>C2_2.6</p>		<p>One approach to increasing operational flexibility and attenuating peak flows is subdividing the existing basin into subbasins along tributary reaches. This basin staging or step-down approach is commonly used on the west coast of Florida in areas such as Lehigh Acres Municipal Services Improvement District (LA-MSID) and the City of Cape Coral, where major structures are in multiple places along the primary and secondary canals, providing a step-down of basin control elevations. This strategy adds more control during the dry season, allowing for inland basins to help maintain water tables at a higher elevation for wetland hydration and water supply purposes, and allows tidal structures to keep minimum flows and levels. In addition, by adding more structures along major canals, this can provide relief to the areas draining to the canal downstream of these structures, as the tailwater conditions would be lowered.</p> <p>The C2 watershed has some higher regions that act separately from the primary system east of the Turnpike. Water control structures, such as sluice gates, can be implemented along the Bird Drive</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>Extension Canal and SW 60th St Canal at SW 127th Ave to divide up the C2 Watershed into C2 West, see Figure 2-12. This could step up stages west of the structures during the dry season, providing additional groundwater recharge. Perhaps more critically, this strategy could provide relief to downstream canal stages, allowing for lower tailwater conditions and better drainage to Snapper Creek in critical areas. Additionally, a gated culvert can be implemented at SW 132nd Ave Canal to provide additional control. This strategy would likely function optimally if implemented in coordination with the storage options to the west, as discussed in the following section.</p>
<p>Acquire storage in western mining lakes with water control structures in Bird Drive Extension Canal to convey water to storage facilities</p>		<p>Western (Rock Mines)</p>	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the C2 watershed can handle up to the 10-year storm event, which was primarily due to road exceedance at culvert locations and canal embankment overtopping along the canals, as explained in PM#1. For the SLR1 condition, similar results to the current conditions 10-year storm were found for not only culverts and canal embankments, but also overland flooding depth and duration. All greater SLR conditions and storm events showed significant increases in canal flooding, as discussed in PM#1, and direct flooding from the canals to the overland, as discussed in PM#5 and PM#6. Therefore, it is determined that the overall level of service provided by this watershed for future SLR conditions</p>	<p>C2_3.1</p>		<p>As part of the Central Everglades Restoration Plan (CERP), the area shown in Figure 2-13 was proposed to have an above-ground impounded recharge area of 2,877 acres, providing 11,500 ac-ft of storage. The goals were to 1) reduce seepage from Everglades National Park, 2) recharge groundwater east of Krome Avenue, 3) increase C4 peak flood attenuation, 4) allow water supply deliveries to the South Dade Conveyance System, and 5) increase spatial extent of wetlands. This project, known as the Bird Drive Recharge Area, was screened out as the concept as envisioned in the Yellow Book was "not feasible" due to the high cost/low benefit ratio (SFWMD, 2011). In terms of flood control, it was stated that the flood attenuation benefits were diminished due to the C4 Emergency Detention Basin. As shown in the FPLOS scenario analysis, during the 100-year/72-hour current condition simulation the C4 detention basin reaches capacity (i.e. max water level of 8.44 ft-NAVD</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
			is the SLR1 5-year storm. No other SLR conditions have passing storms.			or 10 ft-NGVD), and during the 25-year/72-hour the detention basin reaches capacity for the future SLR conditions, as further discussed in Section 7.1. In addition, the Bird Drive Recharge Area could provide flood relief for multiple basins such as the C2, C3W, C4, and C5 basins. This area should be reevaluated as a flood control option, similar to the C4 Detention Basin. This area is directly adjacent to the Bird Drive Extension Canal. Additional structures can be added to the Bird Drive Extension Canal to provide operational flexibility.

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Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
G93 hardening (Raise the overtopping elevation)	C-3	Eastern (Tidal)	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the drainage provided by the primary system in the C3W basin can handle up to the 25-yr event.</p> <p>There is a substantial number of flooded areas likely from tertiary drainage issues due to distance from the canal system, these issues are exacerbated with increasing canal stages, which reduces the ability of the region to drain. Additionally, overtopping of the canal just upstream of the G93 structure increases with SLR, as discussed in PM#1, which then spills into the overland to increase flooding depths and extents, as shown in PM#5. This indicates some amount of primary drainage issues at higher SLR conditions. To account for this, an emphasis on the overall rating was placed on the PM#1 LOS rating, which gives the SLR1 a 10-year, SLR2 a 5-year, and SLR3 does not pass any storms.</p>	C3_1.1		<p>Structure G93 is a two-bay, reinforced concrete gated spillway on the Coral Gables Canal (C3 Canal), located west of Red Road (SW 57th Ave), in the City of Coral Gables. The original structure, G97, was replaced in January 1990 by G93. The discharge from the structure is controlled by two stem operated vertical lift roller gates. The G93 tidal structure operates with the intention to maintain water levels in the C3W Watershed and pass the design flood (from a one in ten-year flood), plus a small discharge from the C4 Watershed, without impacting upstream flooding. In addition, the structure is used to restrict flows to decrease stages and velocities that may cause damage to downstream areas, while preventing saline intrusion during high tides. Figure 3-1 shows a picture of the structure. Table 3-1 provides the design parameters for structure G93 as provided in the Water Control Operations Atlas.</p> <p>The peak discharge at G93 falls below the design value for all design storms during current and future SLR scenarios, while the maximum HW and TW exceed the design HW and TW for all scenarios. Maximum HW elevations exceed the water level that will bypass G93 for all future SLR scenarios except for the 5-year SLR +1 scenario. Maximum TW elevations exceed this bypass elevation during all future SLR scenarios except for the 5-year and 10-year SLR +1 scenarios.</p> <p>Suggested upgrades to mitigate the effects of SLR are as follows:</p> <ol style="list-style-type: none"> 1. Increase the existing structure elevation (including gates and platform) to prevent overtopping 2. Install a forward pump station to help reach the design discharge capacity of 640 cfs while gravity discharge capacity is limited under storm surge and SLR conditions

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>3. Add tieback levees and floodwalls to prevent flooding of the area and short-circuiting of the water around the structure.</p> <p>Forward pumps at this location should be limited in capacity and usage, as there is over 6 miles of canal downstream of the pump station before the Bay that may be impacted by additional downstream discharges on top of tidal surge.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Additional salinity structure or storm surge/tidal barrier at the end of the C3 Canal (potentially with navigational accessibility)				C3_1.2		<p>G93, the salinity structure for the C3 Canal, is over 4.1 miles from the outlet at Biscayne Bay. The downstream area of G93 passes through the Biltmore Golf Course and through highly urbanized South Miami and Coral Gables. An additional salinity structure could be added closer to Biscayne Bay to limit the effect of storm surge and/or SLR on the C3 and C3W Basins, while also providing more discharge capacity for the G93 structure. A potential location for this structure is the area around Cocoplum Circle, near Ingraham Park, as shown in Figure 3-3. There is an existing Cocoplum Road Pedestrian Bridge that could tie-in with the design and capabilities of a new salinity structure.</p> <p>While this structure could significantly reduce impacts from SLR and storm surge in Coral Gables all the way to Red Road, a standard sluice gate implemented at this location would eliminate recreational and commercial navigation upstream. However, implementation of a miter gate would maintain the canal as a navigable until the gates are closed during high tide events. Miter gates consist of a pair of gates, anchored to reinforced concrete abutments at either riverbank, that swing out and meet at an angle pointing toward the upstream direction. Because of this design, the gate would only be operable when the tides are higher than the canal levels (as indicated at G93_T) and could not be used to control flows out of the system. A miter gate would also limit the impacts to wildlife that currently uses the channel, i.e. manatees and fish.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Raising canal embankments in problem areas		Central (Upland)	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the drainage provided by the primary system in the C3W basin can handle up to the 25-yr event.</p> <p>There is a substantial number of flooded areas likely from tertiary drainage issues due to distance from the canal system, these issues are exacerbated with increasing canal stages, which reduces the ability of the region to drain. Additionally, overtopping of the canal just upstream of the G93 structure increases with SLR, as discussed in PM#1, which then spills into the overland to increase flooding depths and extents, as shown in PM#5. This indicates some amount of primary drainage issues at higher SLR conditions. To account for this, an emphasis on the overall rating was placed on the PM#1 LOS rating, which gives the SLR1 a 10-year, SLR2 a 5-year, and SLR3 does not pass any storms.</p>	C3_2.1		<p>Raising canal levees will help reduce overtopping of embankments from the canals to the overland elevations during the peak of the storm events. For the C3W and C3 Watersheds areas primarily near and just downstream of the G93 structure would benefit from higher bank elevations. To review the deficiency of these embankment heights, a comparison was made with the 2022 Miami-Dade County Flood Criteria map, which is based on a 10-year, 24-hour storm event, 2060 scenario with SLR. Figure 3-4 shows the difference of the modeled embankment elevations minus the Miami-Dade Flood Criteria (MDFC) map elevations. In the figure, embankment elevations that are less than a foot above the MDFC are colored with greens and blues, and therefore less urgent in their potential upgrades. Reds and oranges are more urgent, as these embankment locations are much lower than the MDFC. The following areas may benefit from embankment improvements:</p> <ol style="list-style-type: none"> 1. Coral Gables Canal <ol style="list-style-type: none"> a. Low section at intersection with the C4 Canal b. Low section upstream of G93 structure c. Low sections downstream of where the canal diverges to US1 (this does not include the Biltmore golf course, which can be used for emergency storage during high storm events)

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Temporary storage parks/golf courses in				C3_2.2		<p>Because the C3W basin is entirely within the eastern and highly urbanized portion of Miami-Dade County, there is no land readily available for regional storage. To provide additional storage within the C3W Watershed, Miami-Dade County parks or golf courses can potentially be used as emergency temporary storage. A majority of these parks are at lower elevations. Green infrastructure can be implemented at these parks to allow for recreational use during dry periods while also being able to provide storage during storm events. A map of the Miami-Dade County Parks, municipal parks, and golf courses are provided for the C2 and C3W watersheds in Figure 2-6. For example, A.D. Barnes Park is located upstream of G93 and could potentially be used for temporary storage to limit the amount of water coming out of the basin during a storm event. This is critical for the C3W Basin as there is a significant amount of urbanized area downstream of G93 and discharging too much water from the watershed in a short amount of time can contribute to flooding in the C3 Watershed. Downstream of the G93 structure, the Coral Gables Canal can utilize the low embankments of the Biltmore Golf Course to provide additional floodplain storage during high intensity rainfall events. Topography in these golf courses or parks must be reviewed to ensure that new connections to the canal floodplain do not create new paths to structures or residences nearby. Some park facilities may need to be elevated and berms may be required to control the flooding extent.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
<p>S25B Structure Upgrades – raising the overtopping elevation, adding tie-back levees</p>	<p>C-4</p>	<p>Eastern (Tidal)</p>	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the C4 watershed can handle up to the 10-year storm event. The C4 Canal embankments (PM#1) were overtopped for less than a mile for the current conditions 25-year storm and very few culverts were overtopped; however, the overland flooding (PM#5) suggests that more than 0.75 ft (or 9 inches) of flooding may occur in neighborhoods adjacent to the canal, and overland flooding duration is longer than 48 hours for some neighborhoods farther away from the canals, such as the region between SW 92nd Ave and SW 82nd Ave north of Bird Road.</p> <p>For the SLR1 condition, similar results to the current conditions 10-year storm were found for not only culverts and canal embankments, but also overland flooding depth and duration. The number of culverts overtopped doubles from SLR1 to SLR2. For SLR2 the length of canal embankment overtopped (PM#1) is similar to the SLR1 condition. In addition, the flooding depth and duration (PM#5 and PM#6) of the SLR2 5-year storm are similar to the SLR1 10-year storm.</p> <p>SLR3 conditions and storm events showed significant increases in canal flooding, as discussed in PM#1, and direct flooding from the canals to the overland, as discussed in PM#5 and PM#6. Therefore, the SLR3 condition does not pass any of the simulated storm events.</p>	<p>C4_1.1</p>		<p>As per the structure data sheet, the S25B tidal gravity structure (S25B_S) controls flow from the C4 Canal to the C6 Canal downstream of S26. S25B_S is operated with the intention to maintain water levels in the C4 Canal and pass the standard project flood without impacting upstream flooding. In addition, the structure is used to restrict flows to decrease stages and velocities that may cause damage to downstream areas, while preventing saline intrusion during high tides. Figure 4-1 provides a photograph of the S25B structure from the upstream side (west). Table 4-1 provides the design parameters for S25B_S as provided in the Water Control Operations Atlas.</p> <p>The peak discharge at S25B exceeds that design discharge of 2,000 cfs for the 25-year and 100-year design storms under current and all future SLR conditions and falls slightly short of the design discharge for the 5-year and 10-year design storms under current and all future SLR conditions. S25B is the only tidal structure explored in this study whose maximum discharge does not seem to be affected by SLR.</p> <p>Maximum HW elevations exceed the water level that will bypass S25B for the 100-year and 25-year current conditions scenarios and all future SLR scenarios (SLR1, SLR2, SLR3) except for the 5-year SLR1 scenario. Maximum TW elevations exceed this bypass elevation during the 100-year current conditions scenario and all future SLR scenarios (SLR1, SLR2, SLR3) except for the 5-year SLR1 scenario. Figure 4-2 shows the land elevations around S25B compared to the 25-year event for existing conditions and future SLR conditions.</p> <p>Suggested upgrades to mitigate the effects of SLR are as follows:</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						1) Increase the existing structure elevation (including gates and platform) to prevent overtopping 2) Add tieback levees and floodwalls to prevent flooding of the area and short-circuiting of the water around the structure, also known as structure flanking

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Adjust forward pump operations to allow for discharge under higher downstream conditions				C4_1.2		<p>To maintain discharges from the land side to the seaside of S25B_S when gravity capacity is limited, or the gates need to be closed due to the threat of saltwater intrusion, a 600cfs pump station (S25B_P) was added to the S25B spillway (S25B_S) as part of the Miami Dade County Flood Mitigation Program in 2002. As per the structure sheet, S25B_P allows additional discharge capacity during high tide or storm surge events when downstream water levels are elevated. Table 4-2 provides the design parameters for S25B_P as provided in the Water Control Operations Atlas.</p> <p>As discussed in the FPLOS scenario analysis, S25B_P remained off during future SLR conditions because of high downstream water surface elevations at MRMS4, which also forced S26_P to remain off, as this pump protocol requires that the S25B_P is running to turn on.</p> <p>As an immediate response to flooding and as sea level rises, the protocols for operations of the S25B_P forward pumps should be re-evaluated, and higher downstream stages should be used as the cut-off for pumping. If this recommendation is to be implemented, it would require additional hardening and canal embankment increases downstream of S25B to prevent flooding.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Raising canal embankments in problem areas		Central (Upland)	<p>Under critical consideration for this watershed is PM #1, PM#5 and PM#6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the C4 watershed can handle up to the 10-year storm event. The C4 Canal embankments (PM#1) were overtopped for less than a mile for the current conditions 25-year storm and very few culverts were overtopped; however, the overland flooding (PM#5) suggests that more than 0.75 ft (or 9 inches) of flooding may occur in neighborhoods adjacent to the canal, and overland flooding duration is longer than 48 hours for some neighborhoods farther away from the canals, such as the region between SW 92nd Ave and SW 82nd Ave north of Bird Road.</p> <p>For the SLR1 condition, similar results to the current conditions 10-year storm were found for not only culverts and canal embankments, but also overland flooding depth and duration. The number of culverts overtopped doubles from SLR1 to SLR2. For SLR2 the length of canal embankment overtopped (PM#1) is similar to the SLR1 condition. In addition, the flooding depth and duration (PM#5 and PM#6) of the SLR2 5-year storm are similar to the SLR1 10-year storm.</p> <p>SLR3 conditions and storm events showed significant increases in canal flooding, as discussed in PM#1, and direct flooding from the canals to the overland, as discussed in PM#5 and PM#6. Therefore, the SLR3 condition does not pass any of the simulated storm events.</p>	C4_2.1		<p>Raising canal levees will help reduce overtopping of embankments from the canals to the overland elevations during the peak of the storm events. For the C4 Watershed there are several locations where raising the embankments can provide immediate relief during extreme rainfall and surge events with high canal stages. To review the deficiency of these embankment heights, a comparison was made with the 2022 Miami-Dade County Flood Criteria map, which is based on a 10-year, 24-hour storm event, 2060 scenario with SLR. Figure 4-3 shows the difference of the modeled embankment elevations minus the Miami-Dade Flood Criteria (MDFC) map elevations. In the figure, embankment elevations that are less than a foot above the MDFC are colored with greens and blues, and therefore less urgent in their potential upgrades. Reds and oranges are more urgent, as these embankment locations are much lower than the MDFC. The following areas may benefit from embankment improvements:</p> <ol style="list-style-type: none"> 1. Snapper Creek Canal Extension between NW 25th St and NW 74th St 2. Northline Canal – between Snapper Creek Canal Extension and the Palmetto Expy 3. NorthlineNS_C4 – along the Palmetto Expy from the Northline Canal to the Dolphin Expy 4. SW97Ave_North_Canal – near Fontainebleau community 5. Coral Way Canal – along SW 24th St 6. C4 Canal – between SW142nd Ave and SW 122nd Ave 7. S4 Canal – near S25B structure and the International Links golf course

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Temporary storage in parks/golf courses				C4_2.2		<p>To provide additional storage within the watersheds, Miami-Dade County parks or golf courses can potentially be used as emergency temporary storage. A majority of these parks are at lower elevations. Green infrastructure can be implemented at these parks to allow for recreational use during dry periods while also being able to provide storage during storm events. The C4 Watershed has many non-urban areas and recreational areas that may be considered for use as temporary storage areas during extreme rainfall events. A map of the Miami-Dade County Parks, municipal parks, and golf courses are provided for the C4 watershed in Figure 4-4.</p> <p>Golf courses that are in-line with the secondary canals may already have naturally lower embankments or may require embankment degradation to promote overbank spilling in controlled areas. There are no golf courses within the C4 Watershed, however, immediately downstream and south of the S25B structure is the International Links golf course, which may already be providing some floodplain storage during extreme events, and may be potentially improved to increase this floodplain storage in conjunction with improvements to the S25B structure such as tie-back levees.</p> <p>Parks can also be used for temporary floodplain storage during large storm events by degrading the canal embankments and creating what is essentially a dry detention area connected to the canal. There are very few large parks within the watershed, however, the following may be utilized for temporary storage:</p> <ol style="list-style-type: none"> 1. FPL Linear Park – a utility easement that runs parallel to Mud Creek Canal 2. Tamiami Park – adjacent to the Coral Way Canal 3. Carlos Arboleya Camping and Picnic Ground – adjacent to the C4 Canal and Lake Mahar <p>In either strategy, topography in these golf courses or</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>parks must be reviewed to ensure that new connections to the canal floodplain do not create new paths to structures or residences nearby. While not listed as a park, an additional utility easement is located just west of the connection between the C4 Canal and Coral Way Canal, shown in Figure 4-5. Low embankments at this location along the C4 Canal have been identified in the modeling and already experiences overtopping during the current conditions 100-year/3-day storm event. However, additional storage may be possible farther away from the canal within this easement.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Municipal pump station improvements				C4_2.3		<p>Most of Miami-Dade drains via gravity drainage from the neighborhood and street level culverts out to a secondary or primary canal. However, when stages in these canals increase due to sea level rise and storm events, there is less opportunity for water to drain out via gravity and the duration of storm events can increase significantly. To counter these effects, subbasins where gravity drainage will be less possible can implement a municipal pump to pull the water out of the stormwater drainage infrastructure and pump into the canals. Similar municipal pumps have been implemented in such municipalities as Sweetwater, the City of Miami, and unincorporated Miami-Dade County in the C4 Watershed, as well as in the City of West Miami in the C3W Watershed. These municipal pump stations are required to shut off if the elevation in the C4 Canal is above 3.43 ft-NAVD88 (5.0 ft-NGVD29). Table 4-3 shows the percentage of time that the municipal pumps are shut off within the entire simulation period for the 100-year/3-day storm event simulation. In general, the amount of time that the pumps will operate during extreme events, or their efficiency at providing flooding relief will decrease as the stages within the C4 Canal increase, to the point where they will not function at all during a 100-year storm event with +3ft of SLR. While keeping the stages within the C4 Canal low will help to reduce the times that the pumps are off, this strategy may not always be possible or feasible when the groundwater and tides are increasing beyond the control of infrastructure. Instead, the pump-off trigger of 3.43 ft-NAVD88 should be re-evaluated in conjunction with raising the canal embankments and increasing the pump capacity of S25B_P.</p> <p>Several locations in the C4 Watershed may benefit from municipal pump stations, including: A- Northwest corner of the intersection with SW 8th</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						St and the Palmetto Expy B- Southwest corner of the intersection with the Dolphin and Palmetto Expys C-Neighborhood south of SW 24th St between SW 92nd Ave and SW 82nd Ave
Evaluating undersized culverts				C4_2.4		Some culverts within secondary canals may not be sufficiently sized for conveying flows during extreme rainfall events and may need to be upsized. At an initial review, culverts that impacted upstream stages may include those located at: <ul style="list-style-type: none"> • SW97Ave_Canal_North o All culverts: Increasing conveyance in this canal may also help alleviate flooding for the communities just south of the Dolphin Expy, such as Fontainebleau.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Control structures at C2 and C3W watersheds				C4_2.5		Currently, the C4 Canal connects directly with the C2 Watershed via Snapper Creek Canal, SW 132nd Ave Canal, and Coral Way Canal. The C4 Canal connects directly with the C3W watershed at the Coral Gables Canal, as shown in Figure 4-7. These direct connections have shown that the C2 and C3W watersheds are impacted from pumping in the C4 watershed. Adding control structures at the outfalls at Snapper Creek and Coral Gables would provide 1) more control on the flows going to S25B, G93 and S22, 2) backflow prevention from the C2 and C3W watersheds when the pump at S25B or in the C4 Emergency Detention Basin turn on, 3) and flexibility in defining the control elevations of the watersheds.



Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Improved operations for S380 to keep water west		Western (Rock Mines)	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For the current conditions, it was concluded that the C4 watershed can handle up to the 10-year storm event. The C4 Canal embankments (PM#1) were overtopped for less than a mile for the current conditions 25-year storm and very few culverts were overtopped; however, the overland flooding (PM#5) suggests that more than 0.75 ft (or 9 inches) of flooding may occur in neighborhoods adjacent to the canal, and overland flooding duration is longer than 48 hours for some neighborhoods farther away from the canals, such as the region between SW 92nd Ave and SW 82nd Ave north of Bird Road.</p> <p>For the SLR1 condition, similar results to the current conditions 10-year storm were found for not only culverts and canal embankments, but also overland flooding depth and duration. The number of culverts overtopped doubles from SLR1 to SLR2. For SLR2 the length of canal embankment overtopped (PM#1) is similar to the SLR1 condition. In addition, the flooding depth and duration (PM#5 and PM#6) of the SLR2 5-year storm are similar to the SLR1 10-year storm.</p>	C4_3.1		<p>S380 is a five-barrel culvert located in the C-4 (Tamiami) Canal. Flow through the structure is controlled by single stem sluice gates mounted on a frame on the upstream side (west end of the structure). The purpose of S380 is to maintain stages to create and preserve nearby wetlands as well as enhance water supply by providing aquifer recharge. Additional water could be stored west of the structure for flood control purposes. The following recommendations should be considered:</p> <ol style="list-style-type: none"> 1) Adjusting the operations of the S380 gates to remain open if the C4 Detention Basin is not pumping and there is not a positive head differential across the S380 structure, and closed if the C4 Detention Basin is pumping and there is a positive differential across the S380 structure. 2) Potential upgrades for this purpose include installing a backflow pump and raising the structure elevation. In addition, the northern levee along the C4 Canal within the Pennsuco wetlands region could be degraded to be below the top of the S380 structure to provide additional overflow to the wetlands area with increasing normal discharge from the wetlands to the C4 Canal.
C4 Emergency Detention Basin Expansion			<p>SLR3 conditions and storm events showed significant increases in canal flooding, as discussed in PM#1, and direct flooding from the canals to the overland, as discussed in PM#5 and PM#6. Therefore, the SLR3 condition does not pass any of the simulated storm events.</p>	C4_3.2		<p>As part of the Tamiami (C-4) Canal Flood Protection Project that was launched in response to local flooding from Hurricane Irene in 1999 and the "No Name Storm" in 2000, a 900-acre Emergency Detention Basin was constructed north of 8th Street, in the C4 Watershed. During the 100-year/72-hour current condition simulation the detention basin reaches capacity (i.e. max water level of 8.44 ft-NAVD or 10 ft-NGVD), and during the 25-year/72-hour the</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>detention basin reaches capacity for the future SLR conditions, as shown Figure 4-8. Once the basin reaches capacity, no additional flood relief can be achieved with this facility alone, therefore additional storage options will be required for providing additional stormwater detention.</p> <p>It is suggested that the area east of the existing C4 detention basin and west of NW 137th Avenue be acquired to increase the size and capacity of the detention basin (see location in Figure 4-9). This could also provide flexibility for other watersheds, such as the C2 and C3W, to use the C4 Detention Basin for emergency storage and would add up to 740 acres of storage area (potentially 4,000 ac-ft of storage volume at maximum capacity).</p>
Acquire storage areas in western mining lakes (Central Lake Belt Storage Area)				C4_3.3		<p>Another option to provide more storage in the C4 Watershed is to connect and utilize the mining lakes west of the Turnpike as storage and emergency detention. Within the C4 Watershed, there is over 6,000 acres of existing mine lakes that have completed their operations and are currently serving no additional purpose. These open pits could be utilized as additional storage by constructing embankments and seepage walls to contain additional flood waters pumped in from adjacent canals such as Mud Creek Canal, Snapper Creek Extension Canal, etc.</p> <p>Central Lake Belt Storage Area (Figure 4-10) was identified by the SFWMD and USACE as a CERP project. This project includes a combined above and in-ground 5,200 acre reservoir. The initial purpose of this reservoir is for water supply but it could also be used for storage during the wet season. An STA is also proposed on the western side of the storage area. During storm events, water can be routed to the Central Lake Belt Storage Area, that will be kept at low levels during the wet season, and can be managed to</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>include pre-storm drawdown. Following the storm event, water from the storage area can be routed through the STA to increase the water quality prior to discharge to WCA3 or Biscayne Bay. This can work in coordination with the current structures located along the Northwest Wellfield Canal, or additional structures can be considered along the Snapper Creek Extension Canal that runs parallel to the Turnpike. As mentioned in the CERP plan, this would require seepage barriers to prevent horizontal losses to the groundwater.</p>

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Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
S25 replacement (Remove culvert and construct spillway in same location with tie-back levees/floodwalls)	C-5	Eastern (Tidal)	Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. This watershed experiences flooding over the land surface in two ways: 1) due to tertiary drainage issues for low-lying basins far away from the canal and 2) due to stages in the primary canal rising above the land surface elevation. When stages in the canal exceed the land surface elevation for extensive areas of the watershed, this constitutes a no-pass condition for associated design storm. In this way, we must conclude that the C5 Watershed passes the 10-year design storm for current conditions and the 5-year storm for SLR1 conditions. Due to the fact that the majority of the Comfort Canal Southfork embankment (PM#1) was overtopped for all design storm events for SLR2 and SLR3, these conditions do not pass any of the evaluated design events.	C5_1.1		<p>Structure S25 is a single barreled, corrugated metal pipe (CMP) culvert with a reinforced-concrete headwall, located in the Comfort Canal (C5 Canal). The discharge from the structure is controlled by one remotely operated gate. The S25 tidal structure is operated with the intention to maintain water levels in the C5 Watershed and pass the design discharge without impacting upstream flooding. In addition, the structure is used to restrict flows to decrease stages and velocities that may cause damage to downstream areas, while preventing saline intrusion during high tides. Figure 5-1 shows a picture of the structure, located near NW 27th Ave. Table 5-1 provides the design parameters for structure S25 as provided in the Water Control Operations Atlas.</p> <p>During current conditions, S25 is able to pass the design flowrate for all modeled design storms, however, the HW elevation is more than 2 ft over the design value. With 1 ft of SLR, the 5-year event is unable to reach the design discharge even with HW conditions exceeding the design value. With 3 ft of SLR, only the 100-year design storm is able to reach the design discharge. The maximum TW at S25 exceeds the water level which will bypass/overtop the structure for the 100-year current conditions (no SLR) simulation and all future SLR scenarios, except for the 5-year and 10-year SLR1 scenarios.</p>
S25 replacement (Remove culvert and construct spillway in				C5_1.2		<p>In order to increase flows from the basin during storm events, without impacting upstream flooding, and prevent saline intrusion during high tides and storm surge, especially with increasing sea levels, the following are recommended:</p> <ol style="list-style-type: none"> 1. Demolish the current S25 structure and replace it with a gated spillway

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
location with higher elevation and with tie-back levees/floodwalls)						2. Install a forward pump station in combination with the new gated spillway to help reach the design discharge capacity while gravity discharge capacity is limited under storm surge and SLR conditions
Forward pump station						C5_1.3
Raising canal embankments in problem areas		Central (Upland)	Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. This watershed experiences flooding over the land surface in two ways: 1) due to tertiary drainage issues for low-lying basins far away from the canal and 2) due to stages in the primary canal rising above the land surface elevation. When stages in the canal exceed the land surface elevation for extensive areas of the watershed, this constitutes a no-pass condition for associated design storm. In this way, we must conclude that the C5 Watershed passes the 10-year design storm for current conditions and the 5-year storm for SLR1 conditions. Due to the fact that the majority of the Comfort Canal Southfork embankment (PM#1) was overtopped for all design storm events for SLR2 and SLR3, these conditions do not pass any of the evaluated design events.	C5_2.1		Raising canal levees will help reduce overtopping of embankments from the canals to the overland elevations during the peak of the storm events. For the C5 Watershed, the entire Comfort Canal Southfork has low embankments where there are residential units. Figure 5-3 shows the low embankments for the comfort canal for all locations with the canal stage profile for the 25-year/72-hour storm. Analysis has shown that while the low embankments present an immediate threat to the neighboring streets and houses during a high-intensity storm, the proximity to the canal also provides faster drainage and a quick retreat of water levels after the storm has passed. Therefore, to retain this drainage capacity, while providing protection against higher canal stages, the canal embankments must be raised in coordination with adding municipal pumps to the areas that would be lower than the canal stages, and therefore could not gravity drain.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>Additionally, increases to the peak stages are mainly due to tidal influence with +2 and +3 ft of SLR, and improvements to the tidal control structure S25 may decrease stages in the canal by reducing overtopping and backflow into the watershed from tide. This means that the minimum design height of the canal embankments should be re-evaluated under future conditions with the improvements to S25 implemented.</p>
Municipal pump stations				C5_2.2		<p>Most of Miami-Dade drains via gravity drainage from the neighborhood and street level culverts out to a secondary or primary canal. However, when stages in these canals increase due to sea level rise and storm events, there is less opportunity for water to drain out via gravity and the duration of storm events can increase significantly. To counter these effects, subbasins where gravity drainage will be less possible can implement a municipal pump or wet well to pull the water out of these stormwater drainage infrastructure and pump into the canals. Similar municipal pumps have been implemented in such municipalities as Sweetwater, the City of Miami, and unincorporated Miami-Dade County in the C4 Watershed, as well as in the City of West Miami in the C3W Watershed and can be repeated for other low-lying subbasins in the C5 watershed. Physical requirements of the pump station must be achievable for the sub-basin, this includes the retrofitting or construction of an adequate collection system and the available space required for a wet well with pump station housing located near the primary canal. In addition, the implementation of any municipal pump discharging to the primary canal would require that a) the canal levees are raised to meet the minimum appropriate elevations, and b) that there are future connections to planned storage areas or the C4 Impoundment. These requirements will be addressed in subsequent studies if municipal pumps are selected</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>as an alternative for flood mitigation. Several locations in the C6 Watershed may benefit from municipal pump stations. A list of suggested locations is provided in Table 5-2, with reference numbers and figure numbers that refer to map locations outlined with a yellow dashed line. This table also provides an estimated lowest design storm event with which overland flooding depths and durations may be higher and/or more extensive than the surrounding area (where CC refers to Current Conditions and SLR refers to sea level rise conditions simulations). Because the drainage network (pipes shown in red) is already extensive throughout the C5 watershed, implementing a municipal pump station with effective drainage capabilities would likely not require much additional infrastructure aside from the pump, assuming the existing infrastructure is in good condition.</p>
<p>Improvements to S25A to allow inter-basin connection with C4 Canal</p>		<p>Western (Rock Mines)</p>	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. This watershed experiences flooding over the land surface in two ways: 1) due to tertiary drainage issues for low-lying basins far away from the canal and 2) due to stages in the primary canal rising above the land surface elevation. When stages in the canal exceed the land surface elevation for extensive areas of the watershed, this constitutes a no-pass condition for associated design storm. In this way, we must conclude that the C5 Watershed passes the 10-year design storm for current conditions and the 5-year storm for SLR1 conditions. Due to the fact that the majority of the Comfort Canal Southfork embankment (PM#1) was overtopped for all design storm events for SLR2 and SLR3, these conditions do not pass any of the evaluated design events.</p>	<p>C5_3.1</p>		<p>Currently, the S25A structure is kept closed during the wet season and is opened in the dry season when water levels in Comfort Canal recede, in an effort to control salinity. The structure is a single-barreled, manually operated, gated culvert located at NW 45th Ave, as shown in Figure 5-5.</p> <p>Analysis has shown that the effects of pumping into the C4 Impoundment can have far-reaching impacts throughout the system. Flows have been shown to reverse direction from the C2 Watershed at Snapper Creek and SW 132nd Ave, as well as in the C3W Watershed at the connection between the C4 Canal and Coral Gables Canal. This effect on the system may increase with additional stormwater storage capabilities that may be implemented in the future in both the C4 and C2 Watersheds, for example expanding the C4 Impoundment.</p> <p>Allowing the connection with the C5 Watershed to open under certain conditions may alleviate some of</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>the higher stages in the canal that are impacting the low-lying basins. This project would require the creation of a new gated structure with remotely operable gates and a larger flow capacity. Alternatively, uni-directional flap gates can be utilized to reduce operational procedures and keep the flow direction out of the C5 Watershed.</p>

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Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
S26 Hardening (Raise the overtopping and bypass elevations, add tie-back levees/floodwalls)	C-6	Eastern (Tidal)	<p>Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For current conditions it was determined that this watershed experiences flooding primarily due to tertiary drainage issues due to distance from the canal system. Some flooding due to peak stages in the primary and secondary canals is present in some areas for all design storms except the 5-year, which allowed for a 5-year rating for the current conditions. While SLR will impact flooding in the area, no substantial increase above current conditions in embankment or road overtopping (PM#1) was found with the SLR1 5-year storm above.</p> <p>The SLR 1 condition, in general, did not significantly impact the watershed’s ability to discharge during the peak of the storm (PM#2), nor did it cause a significant increase in overland flooding depths and durations (PM#5 and PM#6) across the watershed for the lower storms. However, the SLR2 and SLR3 conditions caused significant increases in these areas for all storm events. Therefore, the SLR1 condition received the same LOS rating as the current conditions of a 5-year storm, while the higher SLR conditions did not pass any of the storms.</p>	C6_1.1		<p>Structure S26 Spillway (S26_S) is a two-bay, reinforced concrete gated spillway located northeast of the Miami International Airport in the City of Miami. The discharge from the structure is controlled by two hydraulically driven cable operated vertical lift gates. S26_S operates with the intention to maintain water levels in the C6 Watershed and pass the standard project flood without impacting upstream flooding. In addition, the structure is used to restrict flows to decrease stages and velocities that may cause damage to downstream areas, while preventing saline intrusion during high tides. Figure 6-1 shows a picture of the structure. Table 6-1 provides the design parameters for S26_S as provided in the Water Control Operations Atlas.</p> <p>The peak flow at S26 for current and future conditions falls significantly under the design discharge of 3,470 cfs. This correlates with Canal Conveyance Capacity Project – C6 Canal Study (C6 Report) which is discussed further in Section 6.2.2. The HW at S26 exceeds the water level that will bypass the structure for the 100-year current conditions scenario and all future SLR scenarios (SLR1, SLR2, SLR3) except for the 5-year SLR1 scenario. The TW also exceeds this bypass elevation during the 100-year current conditions scenario and all future SLR scenarios (SLR1, SLR2, SLR3) except for the 5-year and 10-year SLR1 scenarios.</p> <p>Suggested upgrades to mitigate the effects of SLR are as follows:</p> <ol style="list-style-type: none"> 1) Increase the existing structure elevation (including gates and platform) to prevent overtopping. 2) Add tieback levees and floodwalls to prevent flooding of the area and short-circuiting of the water around the structure.

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Adjust forward pump operations for SLR scenarios				C6_1.2		<p>To maintain flood protection for the C6 basin, a 600 cfs pump station (S26_P) was added to the S26 spillway (S26_S) as part of the Miami Dade County Flood Mitigation Program in 2004. As per the structure sheet, S26_P allows additional discharge capacity during high tide or storm surge events when downstream water levels are elevated. Also, when the S25B forward pump station is operating, and the S26_S capacity is reduced, S26_P will be operated to maintain upstream flood control prevention. Table 6-2 provides the design parameters for S26_P as provided in the Water Control Operations Atlas.</p> <p>As discussed in the FPLOS scenario analysis, S25B_P remained off during future SLR conditions because of high downstream water surface elevations at MRMS4, which also forced S26_P to remain off, as this pump protocol requires that the S25B_P is running to turn on.</p> <p>As an immediate response to flooding and as sea level rises, the protocols for operations of the S25B_P, and S26_P in turn, forward pumps should be re-evaluated and higher downstream stages at MRMS4 should be used as the cut-off for pumping.</p> <p>Eventually, a potential retrofit of the existing forward pumps is also recommended at S26 to increase pump capacity and operability. If these recommendations are to be implemented, they would require additional hardening and canal embankment increases downstream of S26 to prevent flooding, as discussed in Section 6.1.3, below.</p>
Potential retrofit of existing forward pump stations				C6_1.3		

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Floodwalls, sector gate, and pump station at the mouth of Miami River				C6_1.4		<p>The Miami-Dade Back Bay Coastal Storm Risk Management Feasibility Study (Back Bay Study) was conducted by the USACE to examine the impacts of and potential responses to storm surge damage in Miami-Dade County. From this study, a surge barrier, floodwalls, riprap, and a pump station were recommended for the Miami River (C6 Canal). The report states:</p> <p>The current alignment of the floodwall begins on SW 15th Rd near the intersection of Brickell Ave. and continues east towards Biscayne Bay. The transition to the Biscayne Bay occurs and turns north and continues along the shoreline to the mouth of the Miami River Crossing the Miami River is where a proposed Sector Gate and possibly a Miter Gate will be configured to allow boat traffic. The wall continues north on land entering on Biscayne Blvd. The floodwall will follow Biscayne Blvd primarily on the east side to 13th St. where the floodwall will turn left and end at NE 2nd Ave. For the Tentatively Selected Plan, a pump station location either integrated with the Sector Gate or located off Brickell Ave. behind the First Presbyterian Church in the parking lot (USACE, 2020). A sector gate was considered for crossing the mouth of the Miami River because of the relatively easy and fast ability to open and close the gate, as well as its ability to span large widths and remain partially open for extended periods of time if needed. Based upon the navigable channel width of 150 ft, a 150 ft wide sector gate was examined as an option to cross the channel, as part of the Back Bay Study. The top of gate height was preliminarily estimated to be at Elevation 20.9 ft NAVD88 and the bottom of the gate foundation at -18.6 ft. NAVD88. These elevations were selected in consideration of equipment systems requirements and potential scour or accretion. The main disadvantages of the sector gate are the large footprint of the structure itself, especially with the</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						highly urbanized coast at the mouth of the Miami Canal, and the increased cost of construction.
Raising canal embankments in problem areas		Central (Upland)	Under critical consideration for this watershed is PM #1, PM #5 and PM #6, as these relate directly to flooding in canals and overland flooding depth and duration. For current conditions it was determined that this watershed experiences flooding primarily due to tertiary drainage issues due to distance from the canal system. Some flooding due to peak stages in the primary and secondary canals is present in some areas for all design storms except the 5-year, which allowed for a 5-year rating for the current conditions. While SLR will impact flooding in the area, no substantial increase above current conditions in embankment or road overtopping (PM#1) was found	C6_2.1		Raising canal levees will help reduce overtopping of embankments from the canals to the overland elevations during the peak of the storm events. For the C6 Watershed there are several locations where raising the embankments can provide immediate relief during extreme rainfall and surge events with high canal stages. To review the deficiency of these embankment heights, a comparison was made with the 2022 Miami-Dade County Flood Criteria map, which is based on a 10-year, 24-hour storm event, 2060 scenario with SLR. Figure 6-3 shows the difference of the modeled embankment elevations minus the Miami-Dade Flood Criteria (MDFC) map

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
			<p>with the SLR1 5-year storm above.</p> <p>The SLR 1 condition, in general, did not significantly impact the watershed’s ability to discharge during the peak of the storm (PM#2), nor did it cause a significant increase in overland flooding depths and durations (PM#5 and PM#6) across the watershed for the lower storms. However, the SLR2 and SLR3 conditions caused significant increases in these areas for all storm events. Therefore, the SLR1 condition received the same LOS rating as the current conditions of a 5-year storm, while the higher SLR conditions did not pass any of the storms.</p>			<p>elevations. In the figure, embankment elevations that are less than a foot above the MDFC are colored with greens and blues, and therefore less urgent in their potential upgrades. Reds and oranges are more urgent, as these embankment locations are much lower than the MDFC. The following areas may benefit from embankment improvements:</p> <ol style="list-style-type: none"> 1. C6 Canal (Miami Canal) <ol style="list-style-type: none"> a. Low sections in Hialeah Gardens b. Low sections at W 21st St (or 934) c. Low sections on south side of canal near East Dr d. Low sections near S26 structure 2. NW 97th Ave Canal and extension – full canal 3. NW 87th Ave Canal – full canal 4. NW 58th St Canal – full canal 5. Dressels Dairy Canal West – canal east of the Doral Park Country Club 6. Dressels Dairy Canal – full canal 7. Northline Canal – full canal 8. Melrose Canal – full canal (Embankments within the golf course should remain low for additional floodplain storage)
Widen canal to improve conveyance capacity				C6_2.2		<p>As discussed in Section 6.1.1, the peak flow at S26 for all current and future conditions falls significantly under the design discharge of 3,470 cfs. This correlates with Canal Conveyance Capacity Project – C6 Canal Study (C6 Report) which found that the design flows could not be conveyed through S26 while satisfying the water surface elevation criteria set by the original C&SF project (SFWMD, 2020). According to the C6 Report, the original design of the C6 Canal</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>was not implemented completely, and continued urbanization now limits the scope of further implementation of the original plan, limiting the ability to discharge the design flow through S26. In the C6 Report, the District evaluated the current canal performance under current design storm conditions and similar to the results seen in the FPLOS effort, they observed that the C6 Canal could not pass the original design discharge and that water surface elevation design standards were violated at several locations for the 25-year storm. An additional hypothetical scenario was explored that found that increasing canal cross sections in the undeveloped area upstream in the C6 Canal helped decrease water surface elevations to meet the design guidelines. Additional investigation is needed to assess the improvement in canal capacity and bank overtopping with modifications to target channel cross sections.</p>
<p>Construct municipal pumps for Hialeah and Doral</p>				<p>C6_2.3</p>		<p>Most of Miami-Dade drains via gravity drainage from the neighborhood and street level culverts out to a secondary or primary canal. However, when stages in these canals increase due to sea level rise and storm events, there is less opportunity for water to drain out via gravity and the duration of storm events can increase significantly. To counter these effects, subbasins where gravity drainage will be less possible can implement a municipal pump to pull the water out of the stormwater drainage infrastructure and pump into the canals. Similar municipal pumps have been implemented in such municipalities as Sweetwater, the City of Miami, and unincorporated Miami-Dade County in the C4 Watershed, as well as in the City of West Miami in the C3W Watershed, and can be repeated for other low-lying subbasins in the C6 watershed. Physical requirements of the pump station must be achievable for the sub-basin, this includes the retrofitting or construction of an adequate collection system and the available space required for a wet well with pump station housing located near the primary</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>canal. In addition, the implementation of any municipal pump discharging to the primary canal would require that a) the canal levees are raised to meet the minimum appropriate elevations, and b) that there are future connections to planned storage areas. These requirements will be addressed in subsequent studies if municipal pumps are selected as an alternative for flood mitigation.</p> <p>Several locations in the C6 Watershed may benefit from municipal pump stations. A list of suggested locations is provided in Table 6-3, with reference numbers and figure numbers that refer to map locations outlined with a yellow dashed line. This table also provides an estimated lowest design storm event with which overland flooding depths and durations may be higher and/or more extensive than the surrounding area (where CC refers to Current Conditions and SLR refers to sea level rise conditions simulations).</p>
Temporary Storage in parks/golf courses				C6_2.4		<p>To provide additional storage within the watersheds, Miami-Dade County parks or golf courses can potentially be used as emergency temporary storage. A majority of these parks are at lower elevations. Green infrastructure can be implemented at these parks to allow for recreational use during dry periods while also being able to provide storage during storm events. The C6 Watershed has many non-urban areas and recreational areas that may be considered for use as temporary storage areas during extreme rainfall events. A map of the Miami-Dade County Parks, municipal parks, and golf courses are provided for the C6 watersheds in Figure 6-4.</p> <p>Golf courses that are in-line with the secondary canals may already have naturally lower embankments or may require embankment degradation to promote overbank spilling in controlled areas.</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>4. Doral Park Country Club – greens along the Dressels Dairy West Canal</p> <p>5. Doral Golf Course – greens do not align with the canal, but the canal could be routed through the golf course or released during storm events into the lakes</p> <p>6. Miami Springs Golf Course – greens are along the Melrose Canal and would require degradation in some locations.</p> <p>Parks can also be used for temporary floodplain storage during large storm events by degrading the canal embankments and creating what is essentially a dry detention area connected to the canal.</p> <p>7. Doral Central Park – not adjacent to a canal, but could be used for overflow (potentially in connection to the Northline Canal through the Southern Command field)</p> <p>8. Miami Springs Dog Park and fields at Miami Springs Senior High School – adjacent to C6 Canal</p> <p>9. Spring view Elementary School fields - adjacent to FEC Canal</p> <p>In either strategy, topography in these golf courses or parks must be reviewed to ensure that new connections to the canal floodplain do not create new paths to structures or residences nearby.</p> <p>Additional natural areas in this watershed include the cow pasture and agricultural area in the southwest corner of NW 41st St and NW 107th Ave in Doral, which remains largely undeveloped and is naturally low-lying, and the Hialeah Park Casino located at Palm Ave and E 21st St. The Hialeah Park about 200 acres and is elevated several feet above the surrounding neighborhood to the west, as shown in the topographic profile in Figure 6-5. These higher elevation areas are largely natural parks and paved parking lots. The potential for this parcel could be to provide controlled storage using the naturally high landscape as levees, or to simply degrade the natural</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						areas to provide additional floodplain storage during high rainfall events.
Evaluating undersized culverts				C6_2.5		<p>Some culverts within secondary canals may not be sufficiently sized for conveying flows during extreme rainfall events and may need to be upsized. At an initial review, culverts that impacted upstream stages may include those located at:</p> <ul style="list-style-type: none"> • NW 58th St Canal <ul style="list-style-type: none"> o NW 87th Ave o NW 74th Ave • Dressels Dairy Canal West <ul style="list-style-type: none"> o NW 81st Ave o NW 79th Ave
Improvements and operational changes to G72 to discharge to C7 Canal during storm events				C6_2.6		<p>The connection between the C6 and C7 Watersheds is controlled at the G72 structure. However, this structure has limited controls, is known to leak, and is currently being by-passed by canals going up SW 87th Ave, around to W 68th St and back down along the Turnpike, connecting back to the C7 Canal. While no immediate benefits to flood protection or mitigation are available at this time, additional control between these two watersheds would open up options for inter-basin transfers, in particular when considering western storage options in the Lake Belt Storage Area, as discussed in the following section. In addition, monitoring at this location and bypass reduction will help understand flows between the basins and how they can exchange during large storm events.</p> <p>At this time, Inter-basin transfers for flood control in the C6 watershed cannot be possible to the C7 watershed unless there is canal capacity in the C7 canal to receive such flows, which has limited drainage capacity. However, future planned storage</p>

Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
						<p>options to the west may be implemented to also relieve drainage to the C7 Canal, which would require upgrades to this connection. Any such alternative plan will require analysis in conjunction with the C7 watershed.</p>

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Project Name	Basin	Sub-Basin	Sub-Basin Current FPLOS Condition	Mitigation Strategy ID	Total Cost	Comment
Acquire storage areas in western mining lakes (North Lake Belt Storage Area) with conveyance structures connecting to C6 Canal		Western (Rock Mines)	<p>Under critical consideration for this watershed is PM #1, PM#5 and PM#6, as these relate directly to flooding in canals and overland flooding depth and duration. For current conditions it was determined that this watershed experiences flooding primarily due to tertiary drainage issues due to distance from the canal system. Some flooding due to peak stages in the primary and secondary canals is present in some areas for all design storms except the 5-year, which allowed for a 5-year rating for the current conditions. While SLR will impact flooding in the area, no substantial increase above current conditions in embankment or road overtopping (PM#1) was found with the SLR1 5-year storm above.</p> <p>The SLR 1 condition, in general, did not significantly impact the watershed’s ability to discharge during the peak of the storm (PM#2), nor did it cause a significant increase in overland flooding depths and durations (PM#5 and PM#6) across the watershed for the lower storms. However, the SLR2 and SLR3 conditions caused significant increases in these areas for all storm events. Therefore, the SLR1 condition received the same LOS rating as the current conditions of a 5-year storm, while the higher SLR conditions did not pass any of the storms.</p>	C6_3.1		An option to provide more storage in the C6 Basin is to connect the mining pits west of the Turnpike and south of the C6 Canal to the C6 Canal. This project was identified by the SFWMD and USACE as a CERP project, referred to as the North Lake Belt Storage Area (Figure 4-10). This project includes a combined above and in-ground 4,500-acre reservoir. The initial purpose of this reservoir is for water supply but can be used for storage during the wet season. An STA is also proposed on the northern side of the storage area. During storm events, water can be routed to the North Lake Belt Storage Area, that will be kept at low levels during the wet season and can be managed to include pre-storm drawdown. Following the storm event, water from the storage area can be routed through the STA to increase the water quality prior to discharge to WCA3 or Biscayne Bay. Additional structures can be added to the C6 Canal to provide operational flexibility.

6

Appendix B.
Water Supply Vulnerability Assessment

South Florida Water Management District

Water Supply Vulnerability Assessment Approach

Planning Assumptions and Scenario Recommendations for the Lower East
Coast Region



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Abbreviations

AFSIRS	Agricultural Field Scale Irrigation Requirements Simulation
AG	Agricultural (Demand)
ASR	Aquifer Storage and Recovery
BEBR	Bureau of Economic and Business Research
C&SF	Central and Southern Florida
CERP	Comprehensive Everglades Restoration Plan
DSS	Domestic Self Supply (Demand)
ECFM	East Coast Floridan Aquifer System Model
ECSM	East Coast Surficial Groundwater Model
ET	Evapotranspiration
FDACS	Florida Department of Agriculture and Consumer Service
FEB	Flow Equalization Basin
FIU	Florida International University
FPLOS	Flood Protection Level of Service
FSAID	Florida Statewide Agricultural Irrigation Demand
GCM	Global Circulation Model
GW	Groundwater
ICI	Institutional, Commercial, and Industrial (Demand)
LEC	Lower East Coast
LOSOM	Lake Okeechobee System Operating Manual
MGD	Million Gallons per Day
NOAA	National Oceanic and Atmospheric Administration
PCUR	Per-Capita Use Rate
PWR	Power (Demand)
PWS	Public Water Supply (Demand)
RAA	Regional Allocation Areas
REC	Recreation and Landscape (Demand)
RSM	Regional Simulation Model
SFWMM	South Florida Water Management Model
SLR	Sea Level Rise
STA	Stormwater Treatment Areas
SW	Surface Water
SWM	Surface Water Management
TAZ	Traffic Analysis Zones
USGS	United States Geological Survey
WCA	Water Conservation Area
WSP	Water Supply Plan

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Executive Summary

The South Florida Water Management District (SFWMD or District) is conducting a Water Supply Vulnerability Assessment (WSVA) aimed at understanding how future development and climate conditions impact our regional water supply. SFWMD is developing a density-dependent groundwater model – the East Coast Surficial Model (ECSM) – which will initially be run with Sea Level Rise (SLR) scenarios. Additionally, SFWMD is developing future conditions rainfall, evapotranspiration (ET), and temperature datasets to support climate change scenario formulation for follow up ECSM simulations and other regional modeling.

The District created an internal workgroup with representation from various organizational units to develop an approach for identifying and assessing vulnerabilities. Initial scenarios, modeling assumptions, input data selection and limitations, scope, time, and cost were considered in the development of the proposed approach. Table 1 summarizes the majority of the initial recommendations and assumptions that are being integrated into the proposed approach.

To properly analyze the effects of climate change, including SLR, water demand and climate projections will be estimated, and each of the water availability sources will be analyzed as independent “buckets”, using selected metrics to assess vulnerability. Initial scenario formulation includes less and more conservative estimate ranges, with degrees of warming, dryness, and sea level rise, along with 2045 and 2075 growth scenario ranges. The outputs of these scenario runs should allow for SFWMD to understand how future conditions may impact overall water resources availability. Future iterations beyond this WSVA may include the analysis of adaptation strategies and their effects.

The WSVA will be build on the 2023 Lower East Coast Water Supply Plan (WSP) update, and other upcoming WSP efforts. Scenario runs A through C are planned to be included in the 2023 LEC Plan Update while the other scenario runs will be conducted after the 2023 LEC Plan Update as part of the WSVA. The assessment will be based on WSP methodologies by independently analyzing the effects of future climate conditions on growth rates, withdrawal rates, and availability of water supply sources. Public supply and domestic self-supply’s 20-year BEBR growth rates will be extrapolated to 50 years and their withdrawal rates will be calculated using the WSP per capita use rate. Agriculture, landscape, and recreational withdrawal rates will include projected temperature, rainfall, and ET rates at 50 years in the future. The ECSM will incorporate SLR as a boundary condition, and future temperature, rainfall, and ET conditions.

Table 1. Summary of recommendations in the report.

WS Vulnerability Assessment Future Conditions Recommendations		
Water Demand Projections		
Water Use Category	Growth Rate	Withdrawal Rate
Public Supply	Extrapolate BEBR Med growth to 2075	PCUR at 50 years
Agriculture	LEC WSP 2045 Rate	AFSIRS with Climate Change Datasets
Landscape and Recreation	Proportional to Population Growth	Use rate at 50 years
Domestic Self Supply	Proportional to Population Growth	PCUR at 50 years
Institutional, Commercial, and Industrial	LEC 2045 WSP Rate	LEC 2045 WSP Rate
Power	LEC 2045 WSP Rate	LEC 2045 WSP Rate
Climate Projections		
Climate Conditions	Rainfall, Temperature, Evapotranspiration	Sea Level Rise
Datasets	Downscaled GCMs	2022 NOAA Inter Low, Inter High
Existing Availability Source Segmentation		
Availability Sources	Metrics	Assumptions
Surficial Aquifer	GW Levels, TDS, Flow Vectors, Zone Budgets	Canal Stages, Flows from RSM, Tidal
Shallow Impoundment	Storage, Water Depth, Overland Flow	
Unsaturated Zones	Storage	
Canals	Storage, Stages	Conveyance, Quality, Structure Operations
Lakes	Storage, Inflows/Stages	
Reservoirs	Storage	Seepage, Level of Service
Scenario Formulation		
Scenario Run	Growth Variable	Climate Variable
A (LEC WSP)	Base Condition	Current Climate
B (LEC WSP)	BEBR Med 2045	Current Climate
C (LEC WSP)	BEBR Med 2045	SLR1
D (WS Vuln)	BEBR Med 2045	Warmer and Drier
E (WS Vuln)	BEBR Med 2045	Warmer, Drier, & SLR1
F (WS Vuln)	BEBR Med 2045	Hot, Driest, & SLR2
G (WS Vuln)	BEBR Med 2075	Current Climate
H (WS Vuln)	BEBR Med 2075	SLR1
I (WS Vuln)	BEBR Med 2075	Warmer and Drier
J (WS Vuln)	BEBR Med 2075	Warmer, Drier, & SLR1
K (WS Vuln)	BEBR Med 2075	Hot, Driest, & SLR2

Water Supply Vulnerability Assessment Approach

Introduction and Background

The South Florida Water Management District (SFWMD or District) is conducting a Water Supply Vulnerability Assessment (WSVA) aimed at understanding how future development and climate change, including sea level rise, impact regional water supply, and how improvements to water management, water allocation rules, and to the regional system infrastructure can be prioritized to increase resilience.

The purpose of this report is to provide a summary of planning assumptions and scenario recommendations to serve as guidance to the WSVA implementation process for the LEC Planning Area, establishing an internally agreed upon approach, and assessment intention. The report is also intended to serve as a documented process for developing a vulnerability assessment that can be replicated in other planning regions and also by other agencies and stakeholders.

The report is structured into four main sections based on the proposed assessment approach: Water Use Category Growth and Withdrawal Rates, Future Climate Conditions, Availability Sources, and Scenario Formulation. The appendix contains additional details to support understanding of the thought process behind the summarized assumptions and recommendations.

Global and Local Context

Changing climate conditions impact water supply and demand across the region, at micro and macro scales. The District has incorporated qualitative summaries of the potential effects of climate change and future conditions on water supply as part of its Water Supply Plans (WSP) and other related initiatives to provide sustainable water supply for reasonable-beneficial water users while not causing harm to water resources and related natural systems. To improve upon these efforts, the District will be conducting a WSVA that will use advanced modeling to analyze the water supply vulnerability as a result of future climate conditions, including sea level rise (SLR) and increasing demands on those systems beyond the current WSP 20-year planning horizon.

The first WSVA will incorporate the SFWMD's Lower East Coast (LEC) water supply planning area, which includes Palm Beach, Broward and Miami-Dade counties and portions of Monroe, Collier, and Hendry counties.

The WSVA will look at how changes to temperature, rainfall, evapotranspiration (ET), SLR, and growth projections affect availability of various water sources for human uses while not harming water resources and related natural systems. The proposed assessment will help the District make informed decisions on its many water management responsibilities and support partner agencies in their planning needs.

South Florida's unique hydrogeologic, meteorological, and supply/demand system requires a dedicated vulnerability analysis to properly plan for future conditions. However, there are many interdependent complexities between management practices, stakeholder needs, and current and future physical conditions that present challenges to the completion of a comprehensive vulnerability assessment. Therefore, as a preliminary approach, the proposed assessment is intentionally limited in scope and purpose to allow for future iterations based on lessons learned.

This is the first time that a dedicated South Florida water supply assessment will look at the combined effects of SLR, climate change variables and future growth in demands. Hence, there are no best practices or standardized procedures to rely upon. Additionally, due to the complexity and requirements of the models initially identified to conduct the proposed assessment, the criteria for success, as well as the modeling approach, were carefully considered in the assessment planning process. This report summarizes initial recommendations for the above-mentioned considerations and will serve as the basis for the concurrent assessment scoping. These considerations and recommendations are a result of eight-months of internal workgroup discussions, with representation from Water Supply, Water Use, The Office of Counsel, Resiliency, and Hydrology & Hydraulics bureaus.

What follows is documentation on processes as well as the initial workgroup recommendations regarding approaches for assumptions for growth rates, withdrawal rates, climate variables, water availability, and model scenarios and plan for assessment execution.

The Need for an Assessment

Florida statutes requires that WSPs be based on at least a 20-year planning horizon and updated at least every five years. WSP provide a roadmap on how projected water demands can be met without causing harm to the water resources within the planning horizon. While 20-year planning periods serve as an adequate planning horizon to provide guidance to various water use studies, such as utility master planning, regional water resources development and natural resource protection studies, the 20-year planning horizon is not sufficient to evaluate the longer-term effects of climate change and SLR and anticipated potential adaptation and mitigation needs. WSPs consider climate change and SLR possible impacts, but are not formulated yet to adapt to the impacts of longer-term projected climate and growth.

The current WSP 5-year updates being developed by the District have a planning horizon of 2045. WSP, in general, base their emphasis and technical process on the paradigm of how water users can meet current and future demands for at least a 20 year planning horizon. For example, WSP use historic data and observations with 20-year demand projections in their scenarios. Consequentially, this categorizes availability of sources as entities to meet demands based on existing conditions rather than as systems with vulnerabilities that have evolving characteristics over longer time periods. As a result, there is a need for the development of an assessment outside of the WSP process that takes a dedicated look at each source's inherent vulnerabilities and understand the nature of and effects caused by each source's vulnerability characteristics as they change over longer time periods.

The proposed WSVA will look at the vulnerabilities inherent within each source as a function of its interactions with the hydrological system and using its features, demands, and climate parameters as inputs. This allows the District to assess vulnerability as an independent parameter, which can then be addressed through targeted adaptation and mitigation strategies that can increase the relevant source's resilience. Furthermore, the concept of water supply resiliency is best approached from a regional perspective, beyond the distinction of boundary lines -- either agency, permittees, or otherwise. The WSVA, like the WSPs, can provide an integrated systems perspective to vulnerability and resiliency.

Lastly, it's important to note that the assessment will be designed around usefulness for water supply planners, managers, and water users. For instance, given that infrastructure investments and their engineering designs are typically based on a 50-year lifespans as part of future planning efforts; a 50-year time horizon is being recommended.

Internal Workgroup

To incorporate input from the many organizational units within the Districts, an internal workgroup was created with representation from Resiliency, Water Supply, Water Use, Office of Counsel, and Hydrology & Hydraulics bureaus to develop the approach, decision variables, scope, and recommendations that will be used in the assessment. This group was selected and identified to ensure that all relevant business areas were represented, and their inputs were included in initial considerations for the proposed assessment. As part of these discussions, in-depth research was conducted, and the latest science and methodologies used by industry, academia, and similar agencies were presented. The workgroup met for a period of eight months to finalize its initial recommendations and discuss major assumptions.

The discussions were segmented into the following categories: Water Use Category Growth Rates and Withdrawal Rates, Climate Change Variables, and Sources of Water Availability. These categories were intentionally selected to match those referenced in the WSP to leverage existing modeling demands and assumptions and to serve as a supplement to the analysis conducted to support the WSP. However, these categories differ from the WSP in that they were discussed in relation to climate change. For instance, the workgroup discussed how the growth of Public Supply might be affected by climate change in a way that is not already captured using current WSP methodology.

Every additional changing variable introduces the need for further comparative model runs, which requires additional resources and scoping. Therefore, when possible and appropriate, the option of no change from WSP procedures was selected as the recommendation. It should be noted that all the variables discussed for this initial iteration of the WSPA are based on and applicable to the LEC planning area. Future iterations of a WSPA may necessitate different assumptions.

Figure 1 presents a schematic that highlights the overall approach taken by the District to incorporate climate change effects such as SLR and changing rainfall and ET patterns, and future growth conditions in the WSPA for the LEC planning area. The details of the discussions, the research presented, and the explanation for the recommendations that were made are documented below. The following sections are intentionally written as a documentation of the technical discussion process and initial proposed recommendations rather than conclusive suggestions. The process will adapt based on best available information and the knowledge gained as the WSPA progresses.

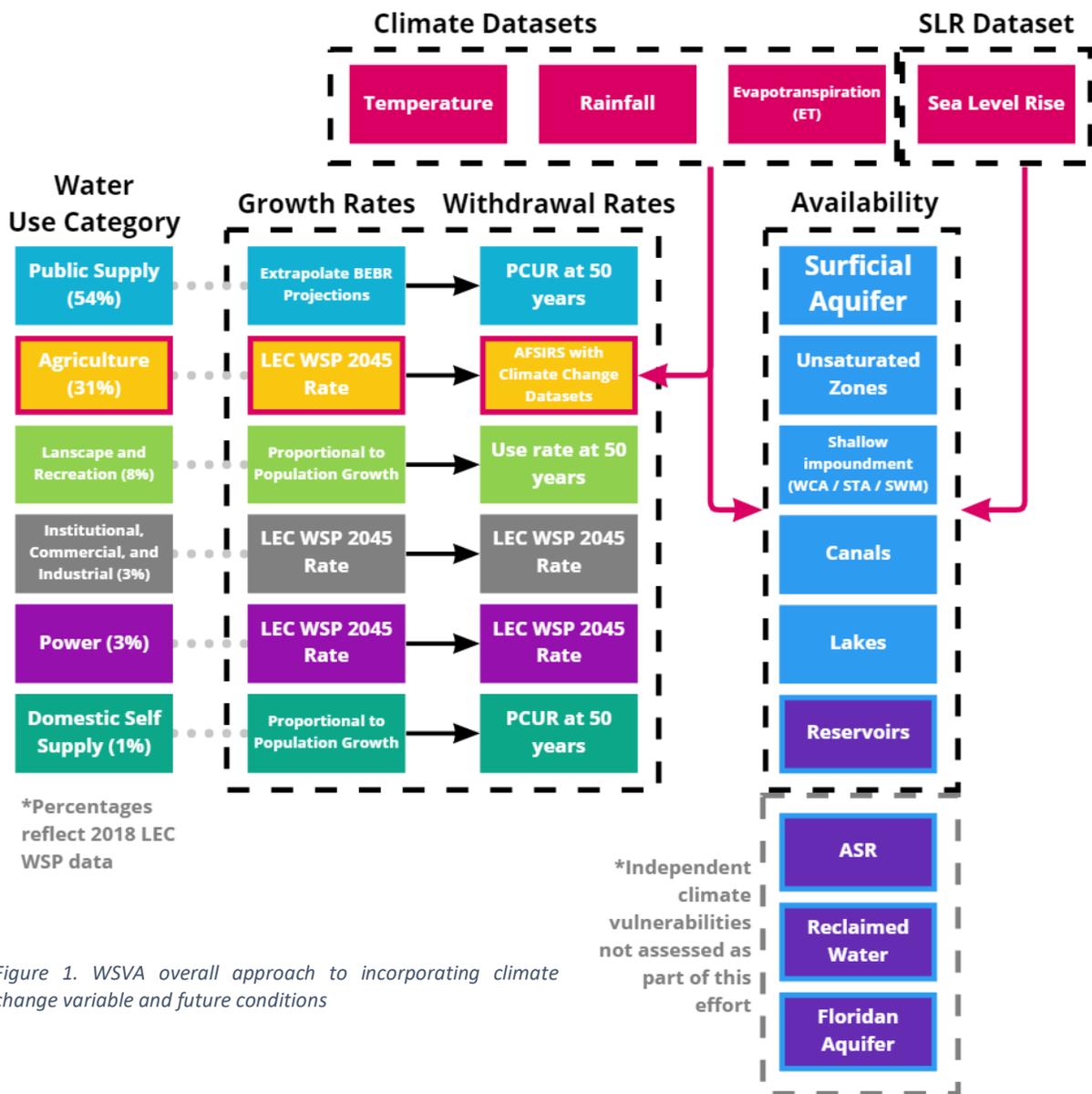


Figure 1. WSWA overall approach to incorporating climate change variable and future conditions

Water Use Category Growth and Withdrawal Rates

Projected water use demands are determined as a function of each water use category's projected growth rate and their projected per unit withdrawal rates. The recommended approaches to project future growth and withdrawal rates for each of the water use categories - Public Supply, Agricultural, Landscape and Recreation, Institutional, Commercial, and Industrial, Power, and Domestic Self Supply – are summarized below. These water use categories, and overall proposed approach to estimate demands, leverage the methodology developed for the LEC WSP. See Appendix A: Water Use Category Growth and Withdrawal Rates for detailed workgroup discussion, relevant research, and major assumptions used in developing the approach for each water use category.

Public Supply Demand

Public Supply (PS) is defined as potable water supplied by water treatment plants with average gross (raw) pumpage of 0.10 million gallons per day (mgd) or greater. In the LEC, PS accounted for 49% of total demands in 2016, of which 94% came from fresh surface water and groundwater sources. In the LEC WSP, population growth and distribution is derived from multiple sources of information, including county-level data from the University of Florida Bureau of Economic and Business Research (BEBR), sub-county data from traffic analysis zones, local data from local government comprehensive plans, and United States census data. This population is further divided into utility service area by using utility service area GIS coverages.

The PS withdrawal rate is calculated by applying a utility-specific per-capita use rate (PCUR), which is calculated in the LEC WSP by taking the monthly and yearly utility-specific finished water data reported to Florida Department of Environmental Protection (FDEP) and dividing it by the utility's estimated population (permanent residents) utility-served service area population. The most recent 5 years PCURs are averaged to develop an average utility-based PCUR, which is then applied to the utility-served population projections to calculate the projected demand at five-year increments for a 20-year planning horizon.

For the PS water demand estimation in the proposed WSVA, it is recommended that BEBR's 20-year county level Medium projection be extrapolated out to 2075 to account for population growth, and that the PS withdrawal rate methodology adopted in the current WSP approach, as summarized above, is replicated for the 2075 estimated growth.

Agricultural Demand

Agricultural demand (AG) is defined in the LEC WSP as self-supplied water used for commercial crop irrigation, greenhouses, nurseries, livestock watering, pasture, and aquaculture. In the LEC, AG accounts for 37% of total demands in 2016 of which approximately 99% comes from sources considered in the proposed WSVA.

The WSP methodology for projecting agricultural growth is based on the irrigated agriculture growth maps generated by Florida Department of Agriculture and Consumer Services (FDACS) in the Florida Statewide Agricultural Irrigation Demand (FSAID) report. These reports are generated annually and contain parcel-level polygons of statewide agricultural lands (ALG) and agricultural irrigated lands (ILG) including crop type projected out to 25 years.

The AG water withdrawal rate is determined in the WSP using the Agricultural Field Scale Irrigation Requirements Simulation (AFSIRS) model (Smajstrla 1990). The FDACS irrigated crop acres, soil types, growing seasons, and irrigation methods are used as input data for the AFSIRS model. AG withdrawal rate estimates and projections are based on the typical commercially grown crop categories developed by the FDEP and water management districts for use in water supply plans. The demands of these crops are then calculated for an average rainfall year and a 1-in-10-year drought.

For the AG water demand estimation in the proposed WSVP, it is recommended that the AG growth rate adopts the current LEC WSP approach and utilizes the same estimated acreage. Although it is likely that these acreages will change as a result of climate change, there isn't an established process for projecting that change beyond the 25 years developed in FSAID. For the AG withdrawal rates, it is recommended that the AFSIRS approach adopted in the LEC WSP is applied with the simulation of future climate conditions.

Landscape and Recreational Demand

Landscape and Recreation demand (REC) is defined in the LEC WSP as self-supplied and reclaimed water used to irrigate golf courses, sports fields, parks, cemeteries, and large common areas such as land managed by homeowners' associations and commercial developments. In the LEC, REC accounts for 8% of total demands in 2016 of which approximately 71% comes from sources considered in the proposed WSVA assessment.

In the LEC WSP, growth in REC demands were increased proportionally with population growth. However, because golf is a unique use case that accounts for a significant portion of REC demand and is influenced by different parameters than other recreation and landscape uses, its growth is segmented from other REC demands and increases/decreases are done on a case-by-cases basis based on local best-available information.

While in the past REC withdrawal rates have been calculated using AFSIRS, the 2023 update to the LEC WSP will use water use data from the District's Estimated Annual Water Use Report. This methodology will likely follow a similar approach to PCUR developed for PS noted above.

For the REC water demand estimation in the proposed WSVP, it is recommended that the REC growth rate adopts the current LEC WSP approach and utilizes the same projected REC withdrawal rates.

Institutional, Commercial, and Industrial and Power Demands

Industrial, Commercial, and Institutional (ICI) demand is defined in the LEC WSP as self-supplied water associated with the production of goods or provision of services by industrial, commercial, or institutional establishments. In the LEC, ICI accounts for 3% of total demands in 2016 of which approximately 65% comes from sources evaluated in the proposed WSVA assessment.

Power Generation (PWR) demand is defined in the LEC WSP as self-supplied and reclaimed water used for cooling, potable, and process water by power generation facilities. In the LEC, PWR accounts for 2% of total demands in 2016 of which approximately 0% comes from sources considered in the proposed WSVA assessment (2018 LEC WSP). Power Generation facilities primarily use seawater, brackish groundwater, and reclaimed water to meet 100% of the demands.

ICI growth is captured on a case-by-case basis with the addition of known permits and population projections while PWR growth is captured exclusively on a case-by-case basis in consultation with power

utilities, principally Florida Power and Light. Withdrawal rates are captured by WUP annual reports and not projected for WSPs.

For the ICI and PWR water demand estimation in the proposed WSVP, it is recommended that the ICI and PWR growth rate adopts the current LEC WSP approach and utilizes the same projected ICI and PWR withdrawal rates.

Domestic Self Supply Demands

Domestic Self Supply (DSS) demand is defined in the LEC WSP as potable water used by households served by small utilities (less than 0.10 mgd) or self-supplied by private household wells. In the LEC, DSS accounts for 1% of total demands in 2016 of which 100% comes from sources evaluated in the proposed assessment. It is assumed that approximately 50% of DSS wells are also used for irrigation. DSS projections are developed simultaneously with PS population estimates and projections and uses the same PCUR as PS.

For the DSS water demand estimation in the proposed WSVA, it is recommended that the DSS growth rate adopts the current LEC WSP approach and utilizes the same projected DSS withdrawal rates.

Future Climate Conditions

50-year Time Horizon

As stated above, the purpose of the WSVa is to understand how climate change may affect water supplies. The gradual nature of climate change makes it difficult to see its effects in the short term and at the same time it is in the short term that the most effective mitigation can take place. The proposed assessment is therefore looking beyond the typical 20-year planning horizon and modeling a water future that exists when the expected consequences will likely be felt and measurable. For this reason, the proposed WSVa will look at conditions in 50 years, or 30 years beyond that reviewed in the LEC WSP.

Similarly, adaptation and mitigation strategies that may be simulated as part of long-term modeling should not be evaluated beyond 50 years due to high levels of uncertainty. Infrastructure lifespans are usually 50 years and outputs of the model runs will be informative and helpful to infrastructure planners. Furthermore, regional water supply projects, such as the C-51 reservoir, required permit applicants to submit 50-year demand estimates, which were required to financially justifying the development of the reservoir.

Sea Level Rise

Sea Level Rise (SLR) will likely be one of the most critical effects of climate change on the region. While the effects of SLR on flooding are being studied as part of the District's Flood Protection Level of Service (FPLOS) program, the effects of SLR on water supply in South Florida have yet to be modeled and analyzed. To investigate these effects, the ECSM – a density-dependent groundwater model of the Surficial Aquifer System (SAS) is being developed, which will allow us to explicitly simulate saltwater movement, including that associated with SLR. The SLR projections will be included into the model application for the 50-year scenario.

There are many SLR projections based on different methodologies, data, and potential application. Section 380.093.(3).(d).3.b., F.S. associated with the Resilient Florida Program and the FDEP Sea Level Impact Projections (SLIP) assessments state, at a minimum, assessments should include the NOAA 2017 Intermediate High and Intermediate Low curves. In February 2022, NOAA published their latest update to the Sea Level Rise Scenario projections (NOAA Technical Report NOS 01), which is based on updated data and the latest methodologies. Table 2 and Figure 2 shows a comparison of the two projections, highlighting the 2022 projections lower ranges of uncertainty.

Table 2. The difference in the SLR projected height for Virginia Key, FL between NOAA 2017 and 2022 projections.

NOAA Curve/SLR (ft)	2017 (2040)	2022 (2040)	2017 (2060)	2022 (2060)	2017 (2080)	2022 (2080)
Intermediate Low	0.69	0.36	1.08	1.21	1.44	1.67
Intermediate	1.05	0.82	1.8	1.44	2.72	2.36
Intermediate High	1.41	0.92	2.56	1.87	4.1	3.38
High	1.77	1.02	3.38	2.3	5.61	4.46

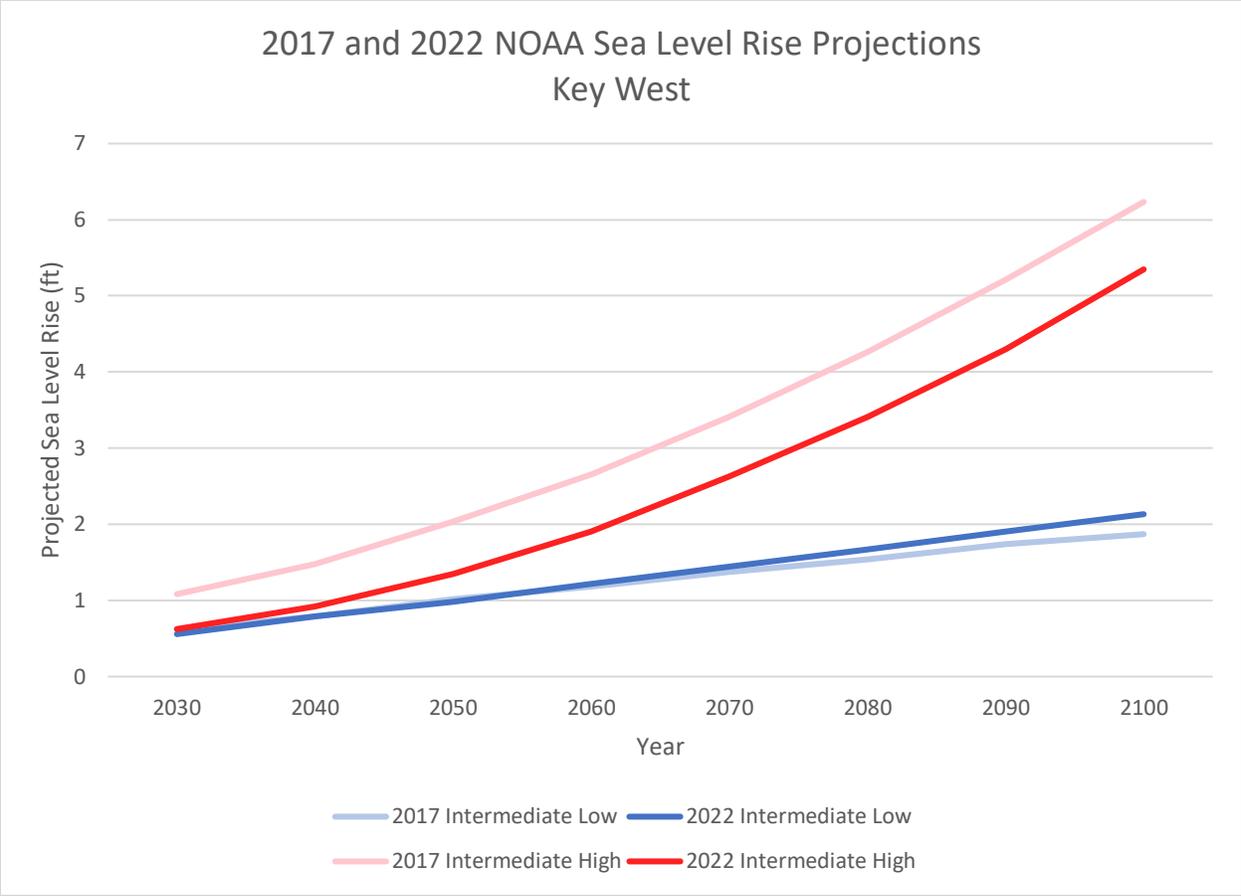


Figure 2. 2017 and 2022 Intermediate Low and High NOAA Sea Level Rise Projections for Key West.

Based on the updated 2022 NOAA projections, this vulnerability assessment will use the 2022 NOAA Intermediate Low and Intermediate High curves as the initial projected SLR scenario. The Florida Flood Hub, in coordination with FDEP Resilient Florida Program, is currently coordinating and leading a scientist workgroup in charge of proposing statewide SLR projections. To maintain approach consistency, the District will adopt Resilient Florida statewide recommendations, as applicable.

To incorporate SLR in the ECSM boundary conditions, a future conditions tidal dataset with daily maximum, minimum, and average elevations will be developed based on an observation dataset, offset per the selected 2022 NOAA curves. Figure 3 shows an example of how a tidal observation dataset may be offset to account for future SLR. The future conditions tidal dataset is currently under development and will undergo a thorough statistical analysis and review process before being incorporated into the WSVA modeling.

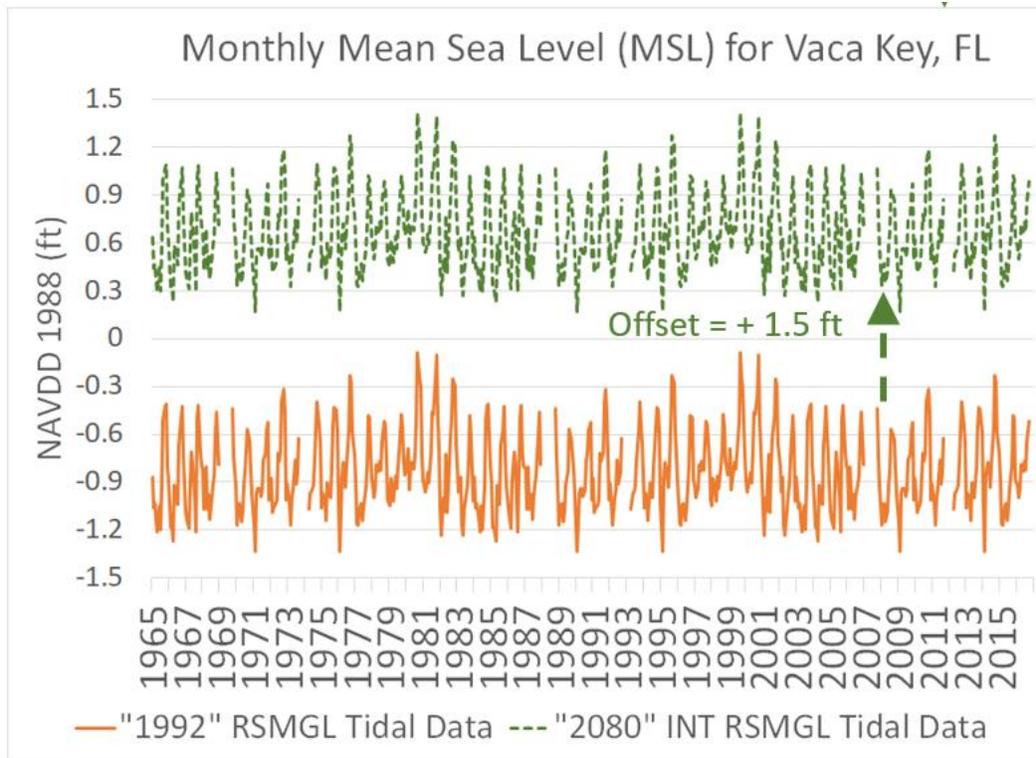


Figure 3. Example tidal observational dataset offset for future SLR.

Temperature, Rainfall and Evapotranspiration

Temperature changes and their effects on rainfall and evapotranspiration will likely have a major effect on water supply. In anticipation of this and other District resiliency efforts, the United States Geological Survey (USGS) and Florida International University (FIU) are partnering with the District to assess and develop suites of rainfall and ET datasets to be used for regional and subregional planning.

These datasets are designed around the premise that climate conditions are non-stationary and therefore incorporate evolving conditions. The non-stationary conditions use Global Circulation Models (GCM), which include empirical and physics-based models that incorporate elements of dynamics, chemistry, and biology of the atmosphere, biosphere, and the oceans as well as greenhouse gas emissions. These GCM have large scales (100km-250km) and therefore need to be downscaled to regional and subregional levels.

The preliminary projection ranges produced by FIU and USGS used statistically and dynamically downscaled datasets. Each of these downscaled datasets were statically analyzed and compared to each other and to observational data. The top ten best performing models with the highest correlation, low root means square error, and a Climate Performance Index (MCI) < 0 and a Model Variability Index (MVI) < 0 for each climate region were selected for the determination of scenario ranges. Figure 4 summarizes the approach used to develop the future climate datasets.

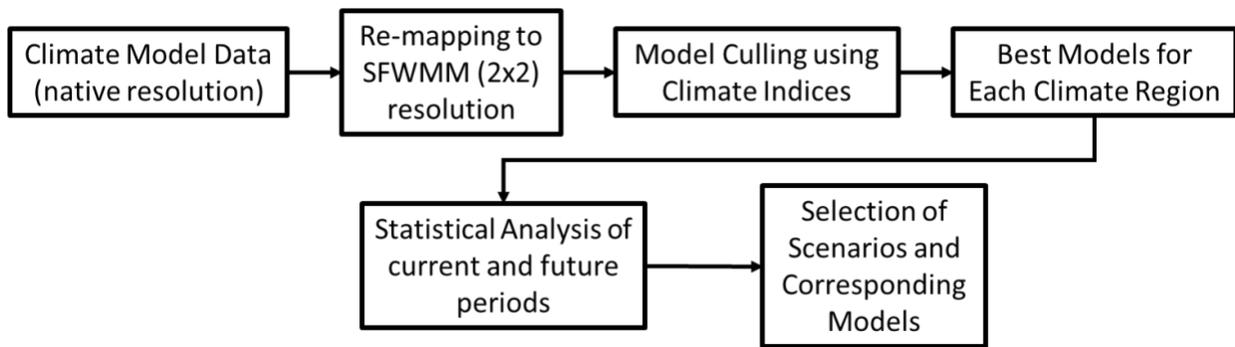


Figure 4. Summary of the adopted approach to modeling future climate scenarios.

While full ET projections require additional climatic variables such as wind speed and relative humidity, temperature is one of the primary drivers and an output of the produced datasets. Figure 5 shows that the average daily maximum temperature is expected to increase considerably. Higher temperatures especially at night result in greater water losses and therefore increased demands.

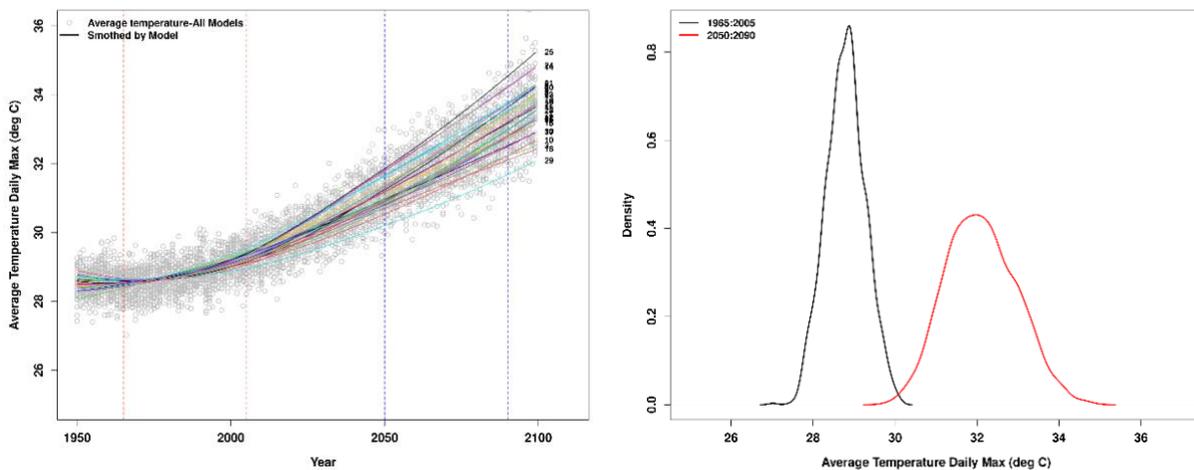


Figure 5. Time Series of gridded average tasmax for all climate models in the LOCA dataset, (b) Kernel Density Functions of tasmax for base and future periods.

Additionally, an overall decrease in annual total precipitation is initially predicted as shown in Figure 6 below.

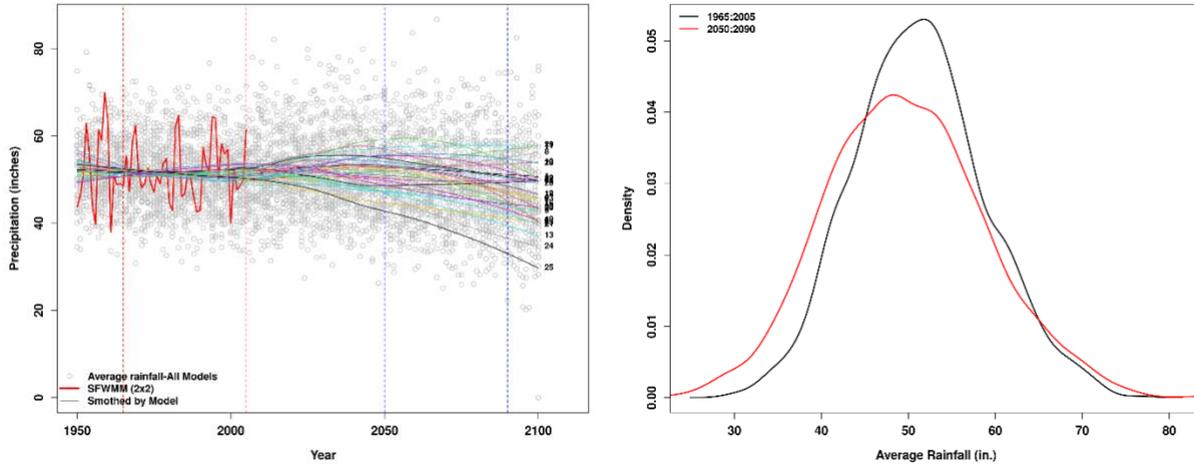


Figure 6. Time Series of gridded average rainfall for all climate models in the LOCA dataset. Also shown is the SFWMM (2x2) average rainfall and smoothed PRCPTOT for each model.

There will be further development and evaluations of the above summarized approach and their eventual datasets based on the model input needs. This development will likely result in future climate datasets that can be used throughout the District’s modeling efforts and will follow a thorough internal review process. Additional regional future conditions temperature, rainfall, and ET projections may be developed to fully address future climate scenario uncertainty and will depend on the regional groundwater and surface water model’s needs and outputs. The results will be updated and shared as they are developed.

Water Availability

System Overview

When assessing the vulnerability of water supplies due to climate change, there are many assumptions and simplifications that must be considered. By using the models and frameworks represented in the LEC WSP as a starting point, we can create an approach for how model outputs may be interpreted and used to understand system vulnerability. At the same time, we can analyze each element in the system as an independent entity with vulnerabilities related to its inputs, outputs, demands, management systems, and additional inherent characteristics.

The Block Diagram in Figure 7 shows how the interactions between the hydrologic system are modeled in the South Florida Water Management Model (SFWMM). For the proposed assessment, a similar simplified diagram was developed below to highlight the intricate hydrology of South Florida and how the influence of future climate conditions and demands will be analyzed and understood from a systematic vulnerability point of view. The System Vulnerability Block Diagram in Figure 9 and its legend in

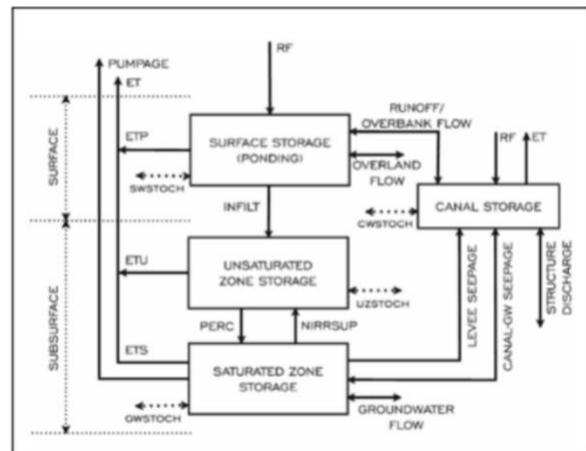


Figure 7. SFWMM Block Diagram.

Figure 8 is based on segmentation of the hydrologic characteristics as they are described in the LEC WSP. It should be noted that major assumptions regarding ecosystem demands and flood protection management are included in model development but not shown below.

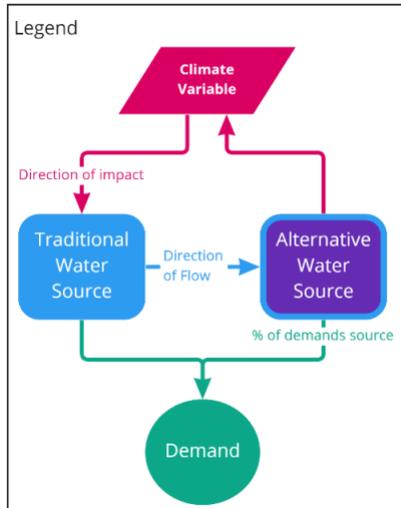


Figure 8. System Vulnerability Block Diagram Legend.

The parallelograms represent the climate vulnerability variables that will be changing in the proposed assessment. The rectangles with the rounded edges represent water sources with blue fill representing traditional water sources and purple fill representing alternative water sources. The circles represent demands, and each color corresponds to a different demand use case. The connections with arrows indicate flow of water with blue representing regular water flows, red representing climate variable, and multi-color demands representing each source of demand with the associated percentage from source as indicated in the 2018 LEC WSP Demands.

Note: Shallow impoundments, unsaturated zones, canals, lakes, and reservoirs are combined as surface water for simplification of demand allocation. Additionally, SLR may have numerous cascading impacts; however, we are still unsure of its effect on the overall supply and demand. SLR will be incorporated as boundary conditions and therefore doesn't have an arrow indicated direction of flow or impact.

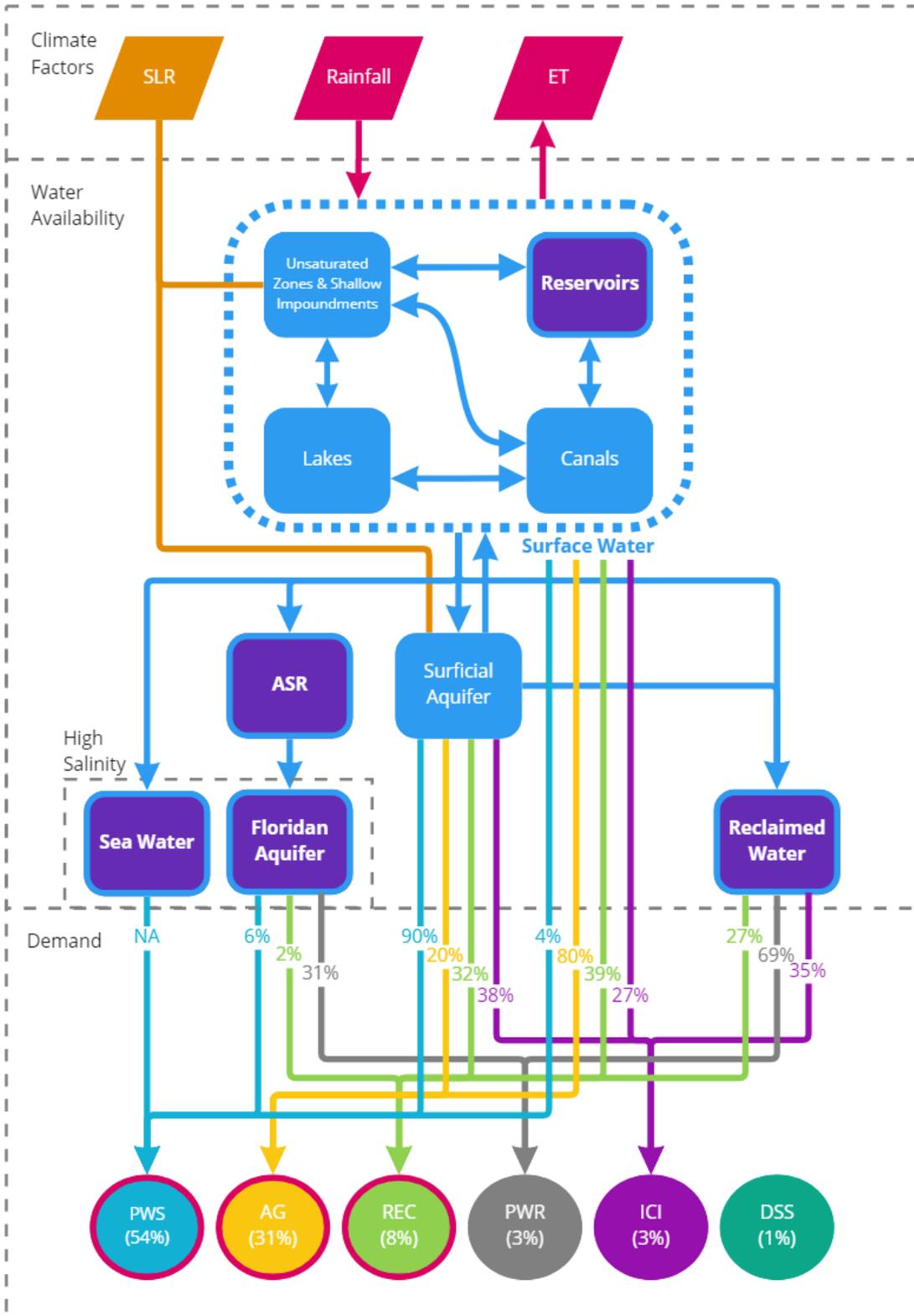


Figure 9. Vulnerability Block Diagram highlighting climate influences, supply sources, and demand.

Models

In the LEC, there are three major surface and groundwater water models to support the assessment of the regional water resources system: the East Coast Surficial Model (ECSM), the Regional Simulation Model (RSM), and the South Florida Water Management Model (SFWMM or 2-by-2). The ECSM, RSM, and SFWMM are all being recommended for the WSVA as they model different components of the system that need to complement each other to get comprehensive and accurate scenario runs. Various water sources and sinks, boundary conditions, and management systems may be captured in one model but not the other and so connections between them have to be established. As model simulations are developed, they need to be continuously checked and equilibrated. This iteration between models is a complex, time consuming, resource intensive, and essential process that ensures results are comprehensive and valid.

The ECSM is a regional model extending north to south from Vero Beach to Marathon and east to west from the Atlantic Coast to the L-2 Canal. While the ECSM is the primary model to be used for the WSVA, the RSM and SFWMM runs will be used to develop the boundary conditions for the ECSM including those related to structure operations and flows from Lake Okeechobee. The ECSM is a 5-layer model that uses daily stress periods with a 1,000 ft x 1,000 ft cell size grid to provide information on daily water levels, monthly total dissolved solids (TDS) concentrations, and 30-day average structure flows. The ECSM code is based on SEAWAT v 4.0 and uses specialized District packages among which are the wetland, routing, and data management packages. After calibration and peer review, ECSM will be used to simulate demands for the 2023 LEC WSP Update and then the WSVA.

The RSM simulates the coupled movement and distribution of groundwater and surface water in conjunction with the coordinated operation of canals and water control structures in South Florida. The RSM has two principal components, the Hydrologic Simulation Engine (HSE) and the Management Simulation Engine (MSE). These components allow for the simulation of management actions and their hydrologic responses. The HSE simulates natural hydrology, water control features, water conveyance systems and water control bodies. The HSE component solves the governing equations of water flow through both the natural hydrologic system and the man-made structures. The MSE component provides a wide range of operational and management capabilities to the RSM by implementing water control structure rules, canal stage maintenance levels and reservoir operating guidelines. Since there is not a single unique way that operations can be executed, the MSE is designed to provide a flexible, extensible expression of management simulation and optimization targets employing a suite of modern control algorithms.

The SFWMM is a regional-scale model that simulates the hydrology and the management of the water resources system from Lake Okeechobee to Florida Bay. It covers an area of 7,600 square miles using a mesh of 2x2 mile cells. In addition, the model includes inflows from the Kissimmee River, and runoff and demands in the Caloosahatchee River and St. Lucie Canal basins. The model simulates the major components of the hydrologic cycle in south Florida including rainfall, evapotranspiration, infiltration, overland and groundwater flow, canal flow, canal groundwater seepage, levee seepage and groundwater pumping. It incorporates current or proposed water management control structures and current or proposed operational rules. The ability to simulate water shortage policies affecting urban and agricultural water uses, and environmental needs in South Florida is a major strength of this model. The SFWMM simulates hydrology daily using observational climatic data periods which includes droughts and wet periods.

There are many other District models some of which are used for water supply purposes like the East Coast Floridan Aquifer System Model (ECFM). However, these models are not highlighted in this report as they will likely not be used to conduct the assessment.

Defining and Measuring Vulnerability

Defining and measuring water supply vulnerability are independent yet connected resiliency concepts. For this assessment, they are combined in that we are only able to measure the parameters that the models can capture, and therefore vulnerability is defined based on model output metrics. As the WSWA models are run, the assessment will further define the thresholds and perhaps additional metrics for each output. These thresholds will likely depend on various factors such as location, hydrologic context and impact, demand dependencies, or even the ease of implementing a particular adaptation or mitigation strategy. These vulnerability definitions and thresholds will be based on model outputs and were initially considered as part of workgroup selection of relevant recommended metrics.

To develop recommendations for analyzing source vulnerabilities, the workgroup segmented each of availability sources into “buckets” based on their hydrologic similarities, management systems, and modeling capabilities and to highlight the temporal and spatial stressors and stresses characteristic to each type of source. For example, the recommended outputs for the bucket representing canals are storage and stage. These are recommended based on the ability for the models to compute those metrics, their usefulness to water managers and planners, and their potential for assessing future demand and climate impacts among other considerations (see Canals). IDEF0 diagrams were developed for each source to facilitate workgroup discussion and their input assumptions and output recommendations are discussed below.

Figure 10 depicts how each bucket’s variables are defined. Blue arrows represent the flow of water and red arrows represent climate variables potentially impacting the respective source as part of the proposed assessment. Orange lines represent how each bucket is modeled and therefore potentially what its input requirements and output limitations are. Black lines represent District management systems that may be impacted as part of the vulnerability assessment. Lastly, the top right box contains the recommended output metrics that will be used to measure relative vulnerability and the bottom right box contains major model input assumptions identified by the workgroup.

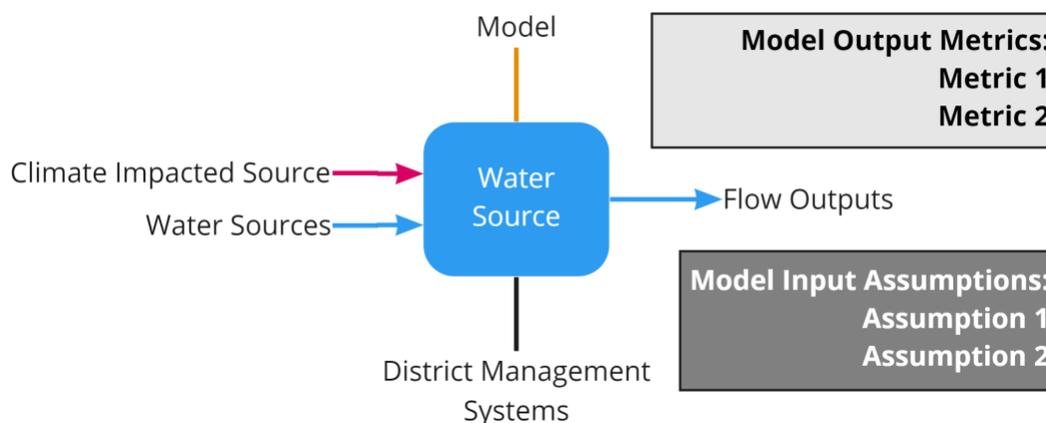


Figure 10. IDEF0 diagram legend for water availability sources.

Availability Sources

It is recommended that for the WSVA the following be analyzed as independent and combined availability sources: shallow impoundments, unsaturated groundwater, canals, lakes, reservoirs, and the surficial aquifer. Future assessments may include analyzing the Floridan Aquifer, reclaimed water, seawater, and Aquifer Storage and Recovery (ASR).

Note: Environmental (ENV) water needs including supply to Everglades National Park and other water conservation areas are met via different assumptions and related management strategies such as Minimum Flows and Minimum Levels (MFL) and Restricted Allocation Areas (RAAs). These assumptions may not be called out specifically; however, they are incorporated as the assumptions carried over from adopting WSP methodologies. Additionally, all approved future Comprehensive Everglades Restoration Plan (CERP) projects that are part of the Integrated Delivery Schedule and are currently being modeled as part of the CERP Update effort, are suggested to be included as future condition simulation assumptions.

Shallow Impoundments

Shallow impoundments are all confined and unconfined surface water accumulation that is not otherwise segmented in the block diagram in Figure 9. This category includes vast swatches of wetlands, such as the Everglades National Park and Water Conservation Area or the Arthur R. Marshall Loxahatchee National Wildlife Refuge, as well as dispersed water management projects. These features will be represented in the ECSM layer 1 and likely simulated through the Wetlands Package.

The major features included in shallow impoundments are Water Conservation Areas (WCA), Stormwater Treatment Areas (STA), and Surface Water Management Areas (SWM). This bucket is currently modeled primarily by the SFWMM and the RSM. The District regulates this bucket as part of MFL and Water Use Permits (WUP) for some AG and REC demands. In addition to precipitation, water flows into shallow impoundments via urban and rural surface runoff, as well as from groundwater, canals, lakes, and reservoirs. Water flows out of shallow impoundments to canals to AG and REC Demand and to the Surficial Aquifer via recharge into the unsaturated and saturated zones of groundwater. Shallow impoundments do have associated losses via ET. The climatically impacted input parameters are SLR, rainfall, ET and AG and REC demands. The effects of SLR on shallow impoundments may be a result of SLR effects on higher groundwater elevations however this bucket will likely not have a SLR component beyond the indirect effects of SLR boundary conditions in the various models. Figure 11 shows an overview of the bucket representing shallow impoundments.

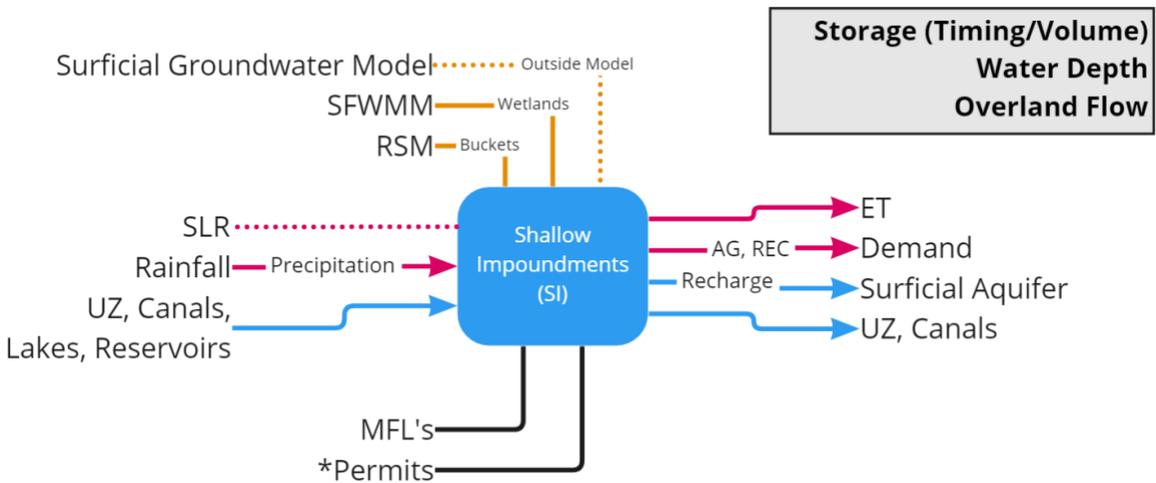


Figure 11. Shallow Impoundment IDEF0 Diagram.

Based on the above-mentioned inflows, outflows, and model constraints, and with a focus on how a vulnerability assessment may be used to assist with MFL and Permits, the following metrics were identified as model output variables: Storage, Water Depth, and Overland Flow rates. Storage will be assessed based on timing and volume and measuring what are the impacts of climate and demand input conditions. Pre-established threshold values will assist in determining vulnerability. Water depth and overland flow are related to volume but as they relate to MFL triggers require their own independent analysis. The proposed assessment will aim to answer the question of if and when might a given climate change future condition trigger an MFL violation and/or a pre-determined vulnerability condition in addition to other questions.

Unsaturated Zones

The unsaturated zone (UZ) is characterized by many parameters that will likely have climate effects not featured in the proposed assessment such as changes in soil capacity and transmissivity. Included in the unsaturated zones are Lake Flirt Marl, Pamlico Sand, Miami Limestone, Fort Thompson Formation, and Key Largo Formation among others that will be represented in the ECSM layers 1, 2, and 3.

Unsaturated zones are currently modeled by the SFWMM and RSM. The District indirectly regulates the unsaturated zone mostly through withdrawal permits for some PWS, AG, REC, and DSS. The majority of PWS, AG, and REC demand is permitted through the saturated zones represented as the Surficial Aquifer however there is a close relationship between both zones. In addition to rainfall, water flows into the unsaturated zones via urban and rural surface runoff infiltration, and as direct infiltration from ponded water sources including shallow impoundments, canals, lakes, and reservoirs. Water flows out of the unsaturated zones to PWS, AG, REC, and DSS demand to the Surficial Aquifer via recharge and as losses via ET. The climatically impacted parameters are SLR, precipitation, ET and AG and REC demand. The effects of SLR on the unsaturated zones will be analyzed through the models. Rainfall and ET will be incorporated as through the above-mentioned datasets directly incorporated into the model, along with AFSIRS input withdrawal rates. Figure 12 shows an overview of the unsaturated zones bucket.

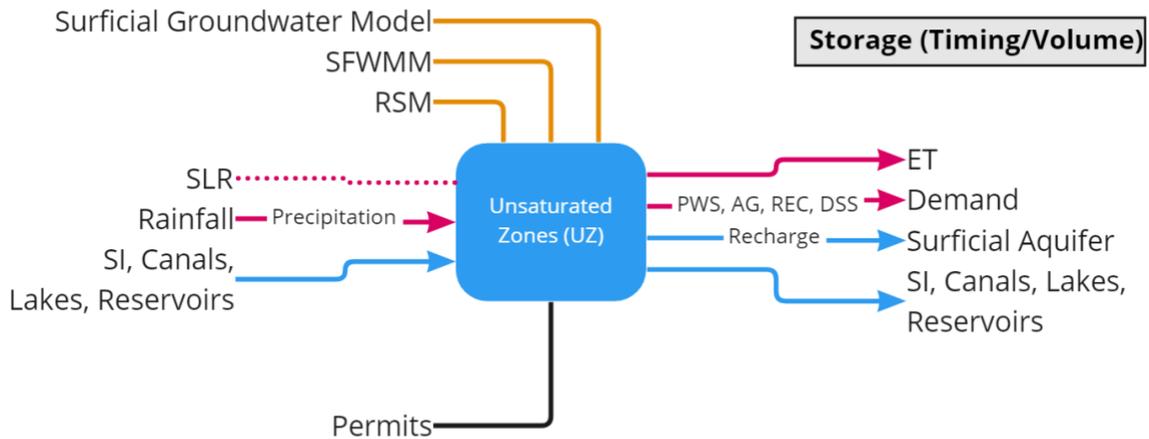


Figure 12. Unsaturated Zone IDEF0 Diagram.

Changes in storage, timing and volume were identified as model output variables based on the above-mentioned inflows, outflows, and model constraints and with a focus on how a vulnerability assessment may be used to support permitting. It should be noted that soil capacity changes both in terms of storage potential and through porosity recharge rates will likely be affected by climate change: however, due to the lack of scientific consensus, uncertainty in approach, and modeling difficulty this change factor will not be incorporated into the proposed assessment. There is an additional planning project highlighted in the 2022 Resiliency Plan that may look at the climate change effects on those parameters.

Canals

South Florida’s canals were primarily developed for flood protection and prevention of saltwater intrusion in 1948, as part of the Central and Southern Florida Project (C&SF Project) and act a major conduit of the regions’ fresh water. Canal operations are tied to water management operation goals, established in specific operation manuals.

Canals are currently modeled by the ECSM, SFWMM, and RSM as part of WSP and many other District modeling efforts such as CERP and FPLOS. Water levels in the canals are impacted by structures operation, RAAs, MFLs, and a few AG withdrawal permits. In addition to rainfall, water flows into the canals via urban and rural surface runoff, infiltration from groundwater, and flows from shallow impoundments, secondary canals, lakes, and reservoirs. Water flows out of canals to tide, AG demand, to the Surficial Aquifer via recharge, as losses via ET, and into lakes and reservoirs. Figure 13 shows an overview of the unsaturated zones bucket.

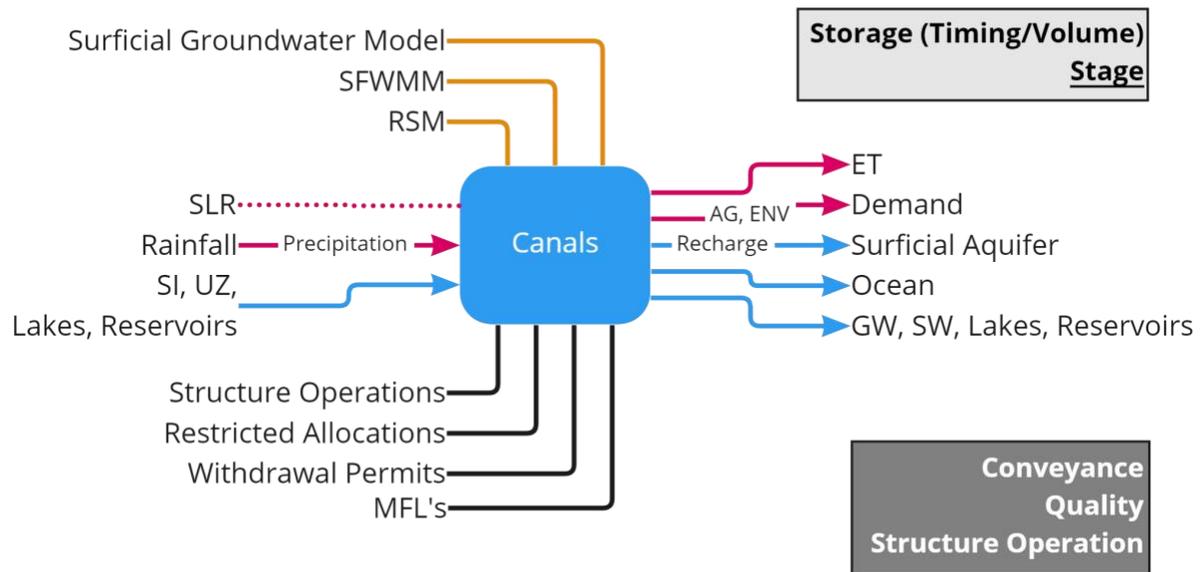


Figure 13. Canals IDEF0 Diagram.

The climatically impacted parameters are SLR, precipitation, ET, and AG demands and ENV needs. The effects of SLR on the canals is very important to consider as their stages are triggers from MFL and RAA. Additionally, they are used as withdraw limitation assumptions in the ECSM model runs. The effects of SLR will likely result in operational changes and structure enhancements first, which might have greater impacts than purely increasing or decreasing demand. Although unlikely, operations may also change because of water quality conditions to prevent downstream negative ecological affects. Furthermore, the canals are operated to prevent saltwater intrusion in addition to its primary flood protection objectives, as such their conveyance characteristics take precedent over storage and quality considerations. Therefore, maintaining conveyance and assumptions regarding quality and other structure operational decisions will be modeled as inputs rather than outputs.

To support decision making for operations, permits, and other regulatory procedures managed by the district, the stage of water in the canals as well as storage in terms of volume and timing are the expected vulnerability outputs. These outputs may take the form of time to trigger a particular structure operation, MFL, or RAAs.

Lakes

Small lakes and shallow impoundments may have similar functional and modeling characteristics, however, there are significant source demand differences such as the City of West Palm Beach's water supply from Lake Magnolia and Clear Lake, when compared to shallow impoundments, that are not a direct sources of water supply. Similarly, Lake Okeechobee's cubic mile of water is the heart of the surface water system in South Florida and its tributaries and distributaries are the supply and source for much of the regions fresh water. Many assumptions and modeling inputs are based on Lake Okeechobee's regulatory and hydrologic conditions.

Lakes, such as stormwater management lakes, are currently modeled by the ECSM, SFWMM, and RSM. Lake levels are impacted by operations of inflow and outflow structures, MFL, WUP and ERPs. Water flows into lakes via rainfall, urban and rural surface runoff, infiltration from groundwater, and through canals and outfalls. Water flows out of lakes via operation of outflow structures. For Lake Okeechobee, these operations will be simulated according to the 2023 Lake Okeechobee System Operating Manual (LOSOM) schedule, which includes sending water to Everglades National Park, estuaries, and other environmental and regional demands. Lakes additionally have components of PWS, AG, and REC demands. Water also flows to the Surficial Aquifer via recharge, as losses via ET, and into groundwater via infiltration. Figure 14 shows an overview of the bucket representing lakes.

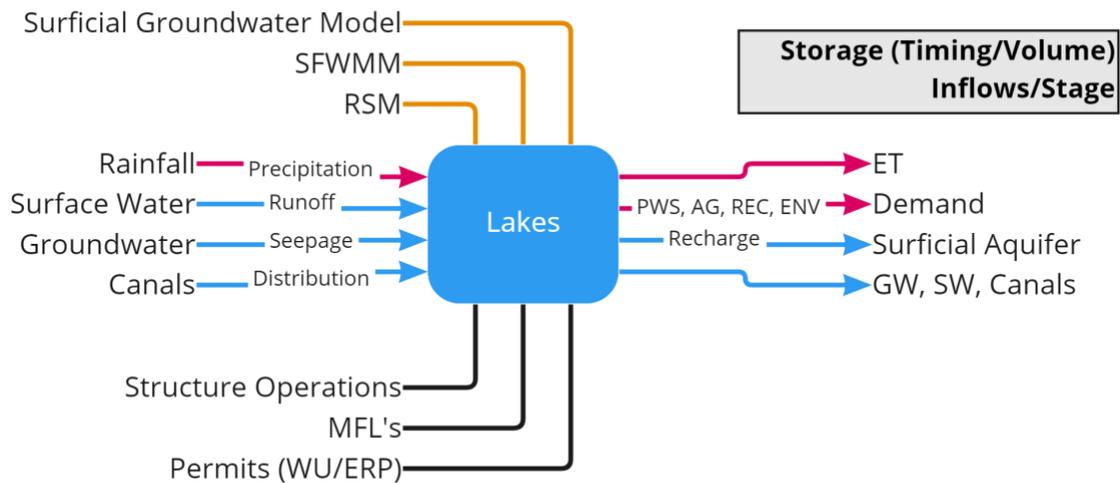


Figure 14. Lakes IDEF0 Diagram.

The effect of climate change on lake conditions will likely be caused by changes in rainfall, ET, and ecosystem and consumer demand. SLR's impact is expected to occur because of drainage and canal conveyance from downstream conditions. The major output metrics associated with lakes are the storage and inflow/outflow rates. MFL triggers and their timing will also likely be a threshold of interest just as they are with canals.

Reservoirs

Reservoirs in the region serve multiple purposes including flood protection and ecosystem water supply needs. The C-51 is a recent example of a reservoir developed for consumer water supply needs which, upon completion, will be operated and managed by the District and serve as supplemental water supply to eight local water utilities. Additionally, Flow Equalization Basins (FEB) whose primary design is for stormwater management purposes also serve as reservoirs.

Reservoirs are currently modeled by the ECSM, SFWMM, and RSM as well as individual and independent specific modeling for future reservoir development and other operational objectives like ecosystem restoration and flood protection. The District manages reservoirs through operations of structures, WUP, ERP (where District is the permittee), and Dam Safety permits. Water flows into reservoirs via urban and

rural surface runoff, infiltration from groundwater, and pumped in via canals. Water flows out of reservoirs to PWS, AG, and PWR demand, to the Surficial Aquifer via recharge, as losses via ET, and into other sources via pumping from canals. Figure 15 shows an overview of the unsaturated zones bucket.

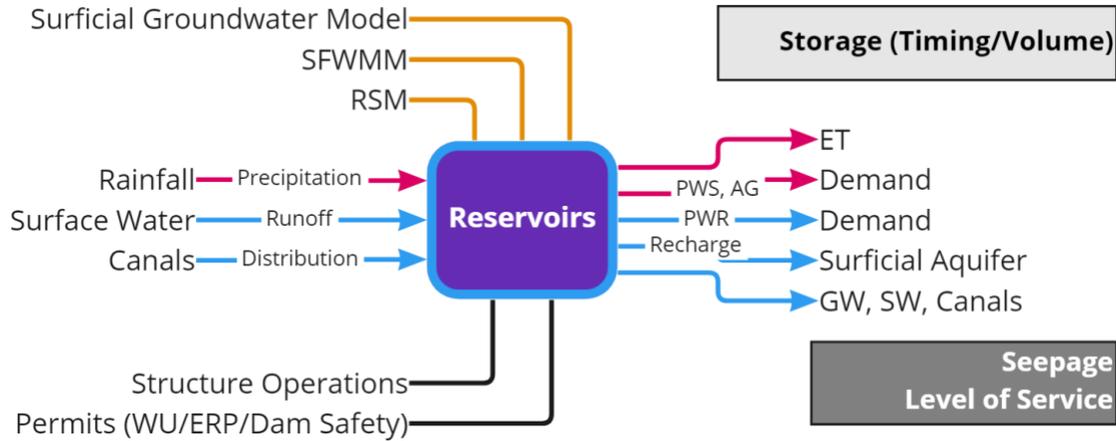


Figure 15. Reservoirs IDEF0 Diagram.

While reservoirs are intended to store water, they aren't fully impervious and therefore do contribute to groundwater via seepage which will be incorporated as a model assumption. Additionally, reservoirs act as storm water buffers and their flood protection level of service assumptions take precedent over storage and as such will be model input assumptions. Storage in terms of volume and timing will be the assessed vulnerability metric and threshold.

Surficial Aquifer

The surficial aquifer is the primary focus of the proposed assessment as it supplies 90% of PWS, 20% of AG, 32% of REC, and 38% of ICI, totaling 55% of the LEC water demands in addition to the portion of water that is later reclaimed. The surficial aquifer is fully encompassed in the ECSM model.

The surficial aquifer is currently modeled by the ECSM, SFWMM, and RSM. The District manages withdrawals from the surficial aquifer through WUPs, RAA, and storm water disposal. Water flows into the surficial aquifer via recharge from all surface water sources during the wet season. Water flows out of the surficial aquifer to PWS, AG, REC, ICI, and DSS demand, back to surface water sources, as losses via ET, and out to tide through the regional canal network. Figure 16 shows an overview of the surficial aquifer bucket.

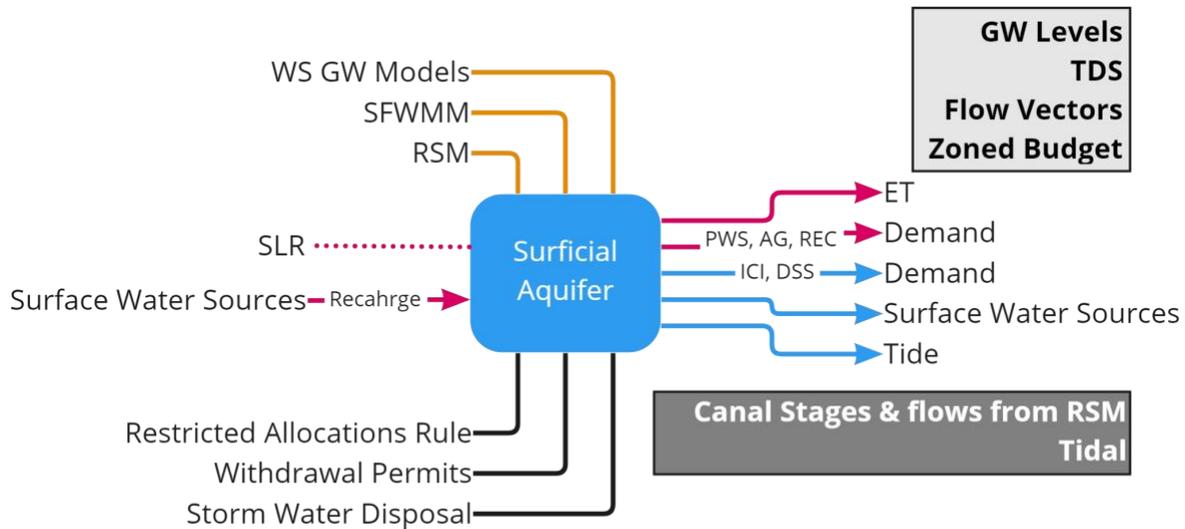


Figure 16. Surficial Aquifer IDEF0 Diagram.

The surficial aquifer is connected to all surface water sources and the effects of demand through surficial aquifer withdrawals cascade throughout other sources in the system. For instance, an inland PS well cone of depression can cause water levels to drop in nearby canal which can trigger an MFL violation related to Lake Okeechobee, especially in drier conditions. Similarly, PWS wellfield withdrawals and their future growth are limited by the RAAs in the LEC. Coastal wellfields will further be evaluated, as part of this assessment, to characterize vulnerability related to the migration of saline water/saltwater intrusion. Modeling and optimizing the responses to potential further demand restrictions will be included as assumptions, inputs, and rules and adaptation responses

Additionally, an assumption is placed on the limits of PS demands as maximum withdraws and the proposed assessment will help us understand what future conditions cause us to reach those limits and when. There are also assumptions made from flows done in the RSM that are inputs to the ECSM as boundary conditions. Lastly, as the ECSM is a density-dependent model, SLR will be modeled as tidal boundary condition that will likely not change with time throughout the model run.

The density-dependent ECSM allows for a more robust analysis of groundwater. Based on its capabilities, the vulnerability output will include groundwater levels, salinity concentrations via Total Dissolved Solids (TDS), flow vectors (direction and magnitude of flow), and zoned budget analysis i.e., how much volume, inflow, and outflow a particular area has. TDS concentrations output will allow for water quality degradation to be analyzed spatially. The flow vectors can show what is the cause various flows of water i.e., is withdrawal the cause for lower canal levels or is it the drier regional conditions. This can help planners and regulatory staff identify potential mitigation strategies or begin the process of updated guidelines based on what works and what drives vulnerability. The zoned budget analysis can provide agencies and planners with an understanding of what their future condition and supply may look like in terms of volume and provide them with guidance on how to plan and regulate accordingly.

Figure 17 contains the combined model input assumptions and model output metrics for each availability source that are initially suggested to go in the development of the assessment and model runs.

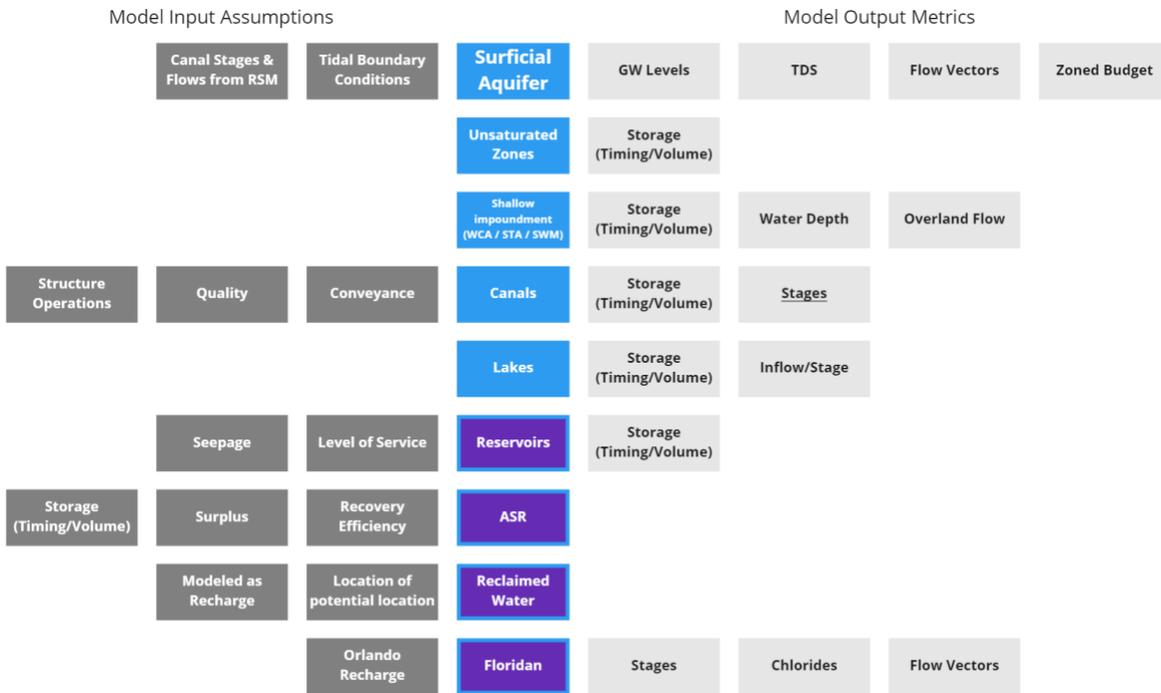


Figure 17. Diagram of the availability metrics and assumptions.

Scenario Formulation

Based on the above research and discussion and approaches identified by the workgroup, the scenario model runs were recommended based on less and more conservative climate change conditions and on a range of growth scenarios within the determined 50-year planning horizon. Selected individual runs are recommended to isolate effects independent of each other. Table 3 defines each of the independent variables that will change with each model run.

Table 3. Independent model variables and their definitions.

Name	Definition	Dataset
Current Climate	Observational data	1985 – 2016 (POR)
2020 Growth Scenario	Base Condition	1985 – 2016 (POR)
2045 Growth Scenario	20-year planning horizon	BEBR Median 2045
2075 Growth Scenario	50-year planning horizon	BEBR Median 2075
Sea Level Rise 1 (SLR1)	NOAA Intermediate Low	NOAA 2022 Update
Sea Level Rise 2 (SLR2)	NOAA Intermediate High	NOAA 2022 Update
Climate Change 1	Warm and Drier	FIU/USGS Future Conditions
Climate Change 2	Hot and Driest	FIU/USGS Future Conditions
Less Conservative	Warm, Drier, & SLR1	Combined
More Conservative	Hot, Driest, & SLR2	Combined

Growth will be evaluated as 2020 Growth Scenario, 2045 Growth Scenario, and 2075 Growth Scenario. 2020 Growth Scenario is defined as the current population at the time of the of the model run. 2045 Growth Scenario is defined as the population growth up to the end of the LEC WSP time horizon (2045) which is based on BEBR Median growth projections. 2075 Growth Scenario is defined as the extrapolation of BEBR Median growth projections out to the end of the 50-year time horizon (centered around 2075).

Sea Level Rise 1 (SLR1) is defined as the 2022 NOAA Intermediate-Low curve as the tidal boundary conditions which reflects the 17th percentile of the projected ranges. Sea Level Rise 2 (SLR2) is defined as the 2022 NOAA Intermediate-High curve as the tidal boundary conditions which reflects the 83rd percentile of the projected ranges.

Climate change will be evaluated on a scale of temperature and moisture (hotter and drier) conditions based on future temperature, rainfall, and ET models and datasets. The runs will be classified into four categories, Climate Change 1 & 2, and Less and More Conservative estimates. Climate Change 1 is defined as warmer and drier conditions which will reflect the respective percentile future condition (around 5-25 percentile: lower bottom of ranges) for temperature, rainfall, and ET in 50 years (centered around 2075). Climate Change 2 is defined as the respective percentile future condition (75-95 percentile: upper bottom of ranges) for temperature, rainfall, and ET in 50 years. Less Conservative is defined as Climate Change 1 with SLR 1, and More Conservative is defined at Climate Change 2 with SLR 2.

The first scenarios will be developed for the 2023 Update to the LEC WSP. These include the 2020 base condition (Current Climate and 2020 Growth Scenario), the 2045 future demand condition (Current Climate and 2045 Growth Scenario), and the 2045 Sea Level Rise Condition (SLR1 and 2045 Growth Scenario). These runs, designated A, B, and G in Figure 18 will serve as the basis for the information contained in the WSP. The climate period of record will use 1985 to 2016 and the SLR boundary conditions will be based on existing tidal conditions for A and B, and SLR 1 for C.

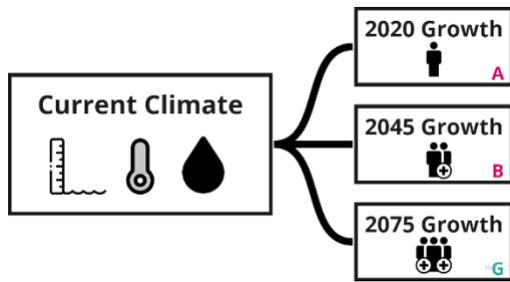


Figure 18. Current climate scenario diagram.

Following the initial LEC WSP scenarios, the first vulnerability scenarios to run will be the 2045 Growth with Climate Change 1, Less Conservative, and More Conservative conditions, designated as D, E, and F. These runs will build on run C by adding climate variables to previous runs and then comparing the effects. The second round of the vulnerability assessment runs are 2075 Growth with No Change, SLR1, Climate Change 1, Less Conservative, and More Conservative conditions, designated as G, H, I, J, and K. These runs represent the total future condition as they combine 2075 growth conditions with 50-year climate and SLR conditions. Figure 19 and Table 4 represent the vulnerability assessment scenario runs.

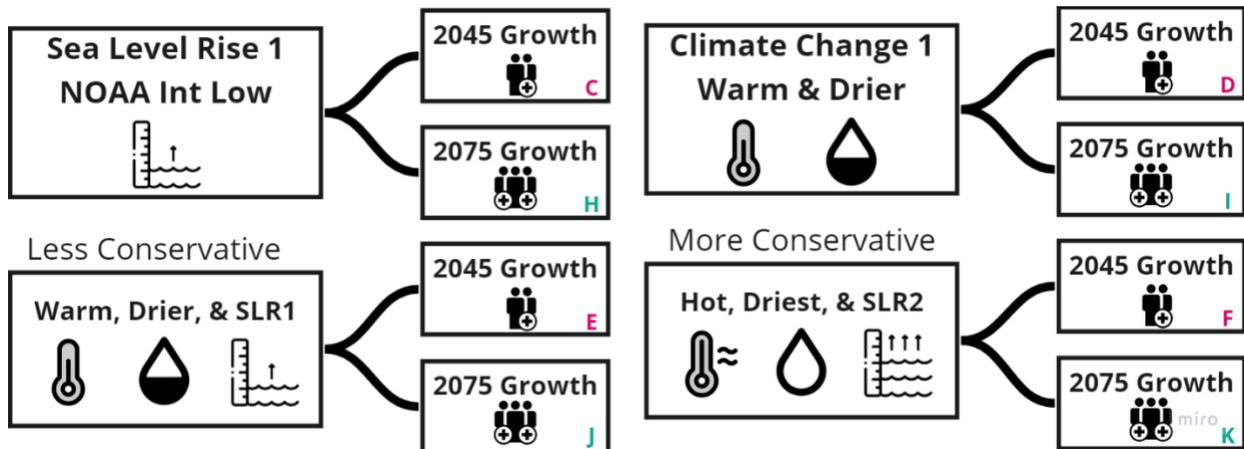


Figure 19. SLR1, Climate Change 1, Less Conservative, and More Conservative scenario diagram.

Table 4. Model run designation and associated independent variables.

Scenario Run	Growth Variable	Climate Variable
A (LEC WSP)	Base Conditions	Current Climate
B (LEC WSP)	BEBR Med 2045	Current Climate
C (LEC WSP)	BEBR Med 2045	SLR1
D (WS Vuln)	BEBR Med 2045	Warmer and Drier
E (WS Vuln)	BEBR Med 2045	Warmer, Drier, & SLR1
F (WS Vuln)	BEBR Med 2045	Hot, Driest, & SLR2
G (WS Vuln)	BEBR Med 2075	Current Climate
H (WS Vuln)	BEBR Med 2075	SLR1
I (WS Vuln)	BEBR Med 2075	Warmer and Drier
J (WS Vuln)	BEBR Med 2075	Warmer, Drier, & SLR1
K (WS Vuln)	BEBR Med 2075	Hot, Driest, & SLR2

Expected Outcomes

Based on the above scenarios and the availability thresholds and metrics discussed above, outputs can be used to determine how a particular sources availability behaves over time. This source behavior can be depicted in a variety of different outputs from geographic maps, tables, and graphs which can then be used to assist management and planning processes accordingly. For example, Figure 20 depicts an illustrative example output comparing a theoretical source volume and demand in model runs A, E, and F, No Change and No Growth and Low Growth with Less and More Conservative conditions. The source volume is shown in purple and grey and is plotted against its low growth demand in gold and green no growth demand in blue. This graph shows us when demand may exceed supply and how the timeline need to enact management practice changes with different conditions. (Note: This output is for illustrative purposes and is not representative of any source, condition, or actual expected outcome.)

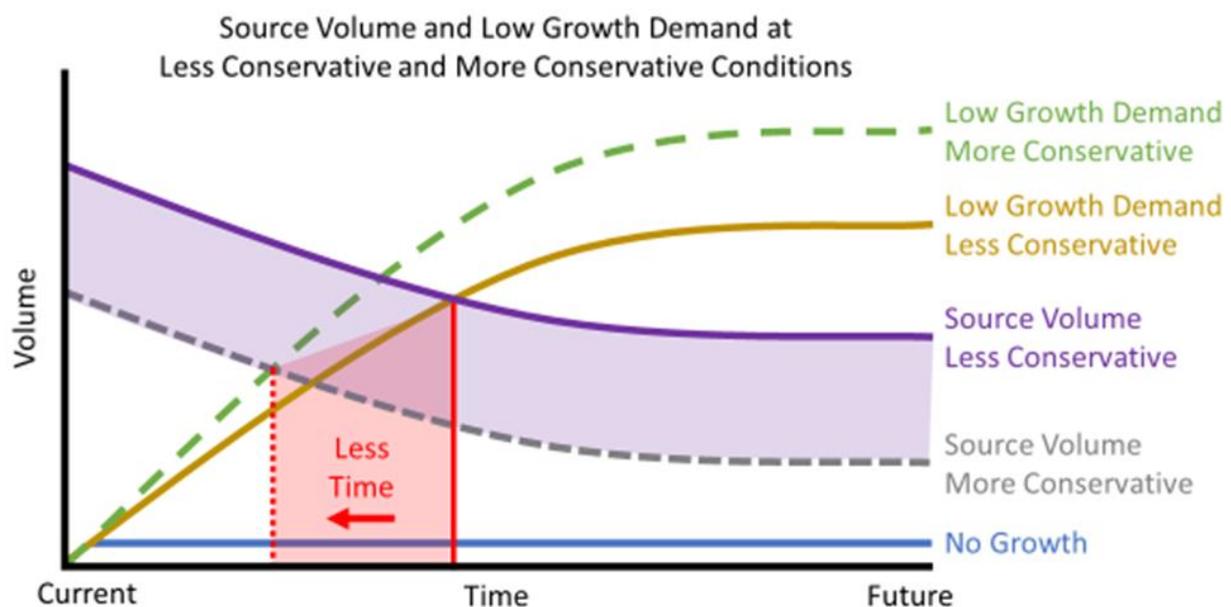


Figure 20. Example assessment output comparing a theoretical source volume and demand for model runs A, E, and F.

In addition to supporting planning efforts the outputs can be used to identify and define risk thresholds. For instance, a system or source can be defined as “at risk” when it’s within a certain timeframe from reaching a variable threshold. This can support various mitigation efforts such as grant applications to allow development of alternative water supplies or rule-making to further restrict use from at risk sources.

Scenario Limitations and Timeline

The time it takes to set up, troubleshoot, and run each model places limitations on the scope of the study. Once the ECSM has been calibrated, additional time is needed to set up the new scenario runs and execute these modeling runs. These challenges are compounded with the longer time horizon and the novelty of incorporating new elements such as density dependence, in addition to the above-mentioned need of equilibrating multiple models.

New datasets such as future temperature, rainfall, and ET and future growth projections will be developed as model inputs. The development of these datasets will require additional parallel efforts and increased

costs. In anticipation of these and other model requirements the scoping of necessary parallel efforts will begin immediately. Table 5 shows the anticipated timeline for the future condition development, model development, model runs, and analysis, leveraging the model development advanced as part of the LEC WSP.

Table 5. Anticipated timeline of the WSVA.

Water Supply Vulnerability Analysis (WSVA) Schedule		FY22				FY23				FY24				FY25
		Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1
WSVA Approach	Internal Workgroup	■	■	■	■									
	Report Draft and Review					■	■							
Future Conditions Dataset Dev.	Population Projection						■	■						
	Climate Dataset						■	■	■	■				
	Internal Data Processing									■	■			
Model Dev. & WSP Run	ECSM Update/ Calibration*				■	■	■	■						
	LEC WSP Scenario Runs*						■	■	■					
WSVA Run & Analysis	WSVA Scenario Runs									■	■	■	■	■
	WSVA Analysis and Report													■

* the LEC WSP model development, calibration and scenario runs are illustrated here for planning purposes only and are not dependent on any of the described WSVA tasks.

Future Work

“An ounce of prevention is worth a pound of cure” – Benjamin Franklin

In addition to the initial recommendations described above, which are being prioritized as part of the initial study recommendations, future efforts, as detailed below, were identified by the Workgroup, and will be further developed as part of future study phases. It is important to note that the first phase of the WSVA is to develop a series of base climate conditions on which to apply various mitigation and adaptation strategies. Like the FPLOS program, base conditions are first developed, which inform the appropriate mitigation and adaptation strategies to then be modeled.

Future Scenarios

Future scenarios should include the incorporation of alternative mitigation strategies into modeling. These mitigation strategies can help managers understand the resiliency strategies that may be attained to reduce vulnerabilities. While there are many potential mitigation strategies, Figure 21 shows a few potential mitigation strategies that might be organized as part of additional scenario runs roped in Mitigation Strategies Scenarios.

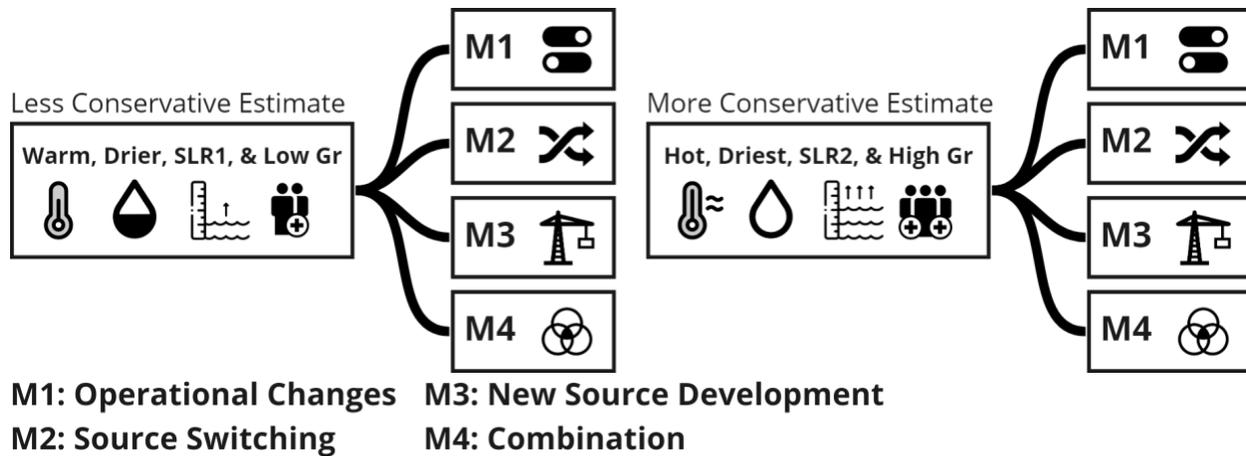


Figure 21. Mitigation scenarios runs.

M1 corresponds to operational change which in the above scenarios are input assumptions. These assumptions can be optimized with a given climate condition and requires no additional infrastructure investment. However, there are many objectives that determine the operational procedures of various structures which can compete with one another and have complex interdependent regulatory constraints. Therefore, modeling this mitigation strategy is not trivial and will require additional discussion. M2 corresponds to source switch which assumes that demands will be met with different sources throughout the model time frames. The scenarios above discuss the assumption that demand will be capped at the RAA limitation. M2 analyses would evaluate if some of the demands were met by sources like reclaimed water or via distribution from other utilities. M3 corresponds to the development of new sources such as additional Floridan aquifer or seawater. Historically, development of new sources has been a popular management practice for utilities who are approaching their RAA limitations or at risk of saltwater intrusion. M4 corresponds to a combination of all the above-mentioned strategies and may include projections for increased conservation.

These strategies can be combined with outputs mentioned previously and can assist with the identification of water supply priority resiliency investments. Figure 22 shows an illustrative potential output that shows the effect of M3 on source volume and highlights how that may increase the timeline for mitigation or adaptation to climate change. Similarly, it can also help define vulnerabilities based on the time it takes to implement various mitigation strategies, their likelihood of success, and potential impact. For instance, new source development may temporarily solve a supply shortage but may also be the only available mitigation strategy so that a particular source or location is therefore “at risk”.

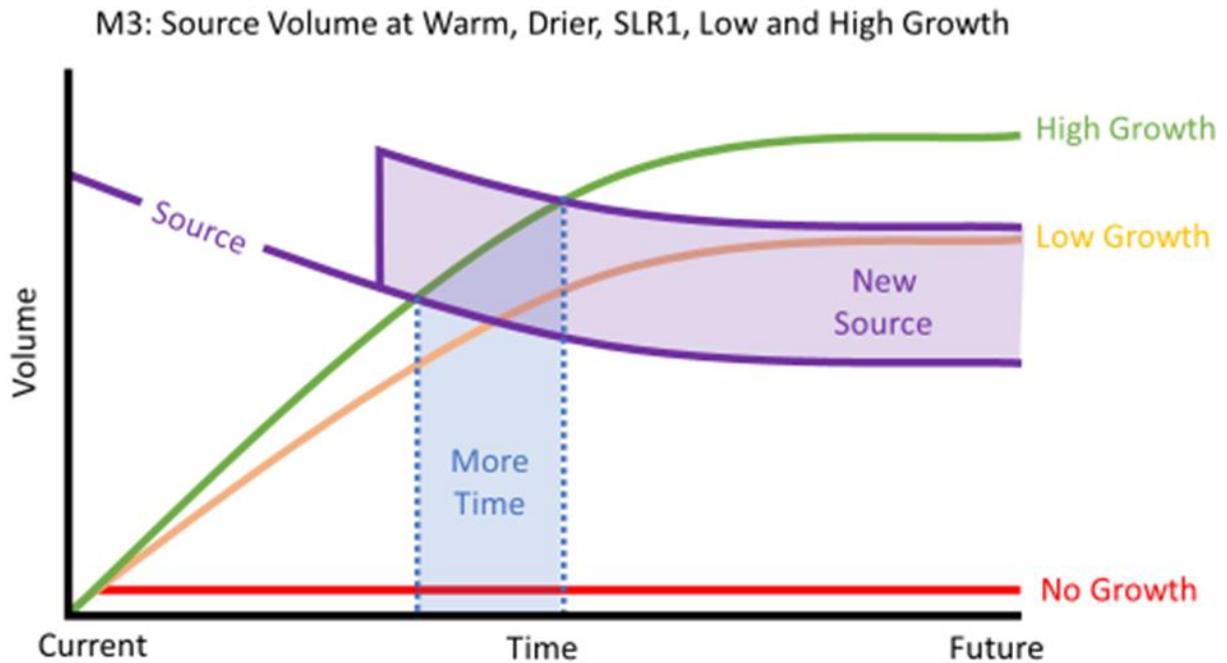


Figure 22. Example mitigation scenario output highlighting the effect of new supply sources.

Not Assessed Availability Sources

Reclaimed water, ASR and the Floridan Aquifer are sources whose vulnerability are not being recommended to be directly analyzed as part of the initial phases of the proposed assessment. While these sources play an essential role in the LEC water supply system, in the case of ASR and Reclaimed Water, they are potential mitigation and adaptation strategies, and in the case of the Floridan Aquifer are likely more affected by future demand conditions rather than the climate change conditions featured in the proposed assessment (SLR, temperature, rainfall, and ET). Future analysis may independently look at the climate vulnerabilities associated with each of these sources.

Appendix A: Water Use Category Growth and Withdrawal Rates Workgroup Discussion

How a particular water use category demand change over time is combination of its growth rate and withdrawal rate. The growth rate is a function of the projected growth of that industry such population increases, irrigated acreage increase/decrease or the square footage of industrial or commercial space. The withdrawal rate is the estimate water use per unit to calculate the overall demand for that water use category. Water use per unit can include per capita water use for public supply and domestic self-supply, water needs per acre of crop for agriculture, or water needs per acre of landscape or golf course. Changing climate can impact the water use per unit, especially for water use categories that include irrigation.

For the proposed assessment, growth rates are separated from withdrawal rates to allow for the application of an independent climate focused methodology where applicable and feasible. Each of these rate's variables may have important climate change components but their relationships and model inputs would have to be sufficiently established to be incorporated into the WSPA which may be beyond the scope of the proposed assessment especially for growth rates. Alternatively, the approach to apply the effects of climate change on withdrawal rates have a clearer methodology and the process of applying them is relatively straight forward.

The use categories follow the 2018 LEC WSP methodology and are segmented as Public Supply (PS), Agriculture (AG), Landscape and Recreation (REC), Institutional, Commercial, and Industrial (ICI), Power (PWR) and Domestic Self Supply (DSS). Below are the explanations, discussions, and research for the above use category growth rates. For each water use category, a series of boxes are presented showing options considered by the workgroup with the light green box indicating the option the workgroup suggests adopting.

A.1: Water Use Category Growth Rates

Public Supply Growth Rates

Figure 23 shows options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 23. Public Supply growth rate options.

In the WSP, PS growth is derived from multiple sources of information, including county-level data from the University of Florida Bureau of Economic and Business Research (BEBR), sub-county data from Traffic Analysis Zones (TAZ), and local data from local government comprehensive plans and United States census. BEBR 20-year projections are conducted at the county level. These county-level projections are distributed by District staff via TAZ and census data to utility service areas whose boundaries are updated annually. The BEBR projection serves as the control for the county-wide projection when combining individual utility service area populations. Estimates of DDS population within the utility service area is subtracted from the utility service area population to estimate the utility-served population. In addition, local government plans for providing utility service in current DSS areas are incorporated in the projections.

When projecting growth rates in PS, factors to consider include the projection methodology underlying the rates themselves and how they will be distributed spatially within utility service areas. While these are connected, climate influences may have different impacts on each aspect. For instance, increased coastal flooding due to climate change can change how population growth gets distributed within service areas and between utilities but may not have as consequential an effect on overall growth rates.

While there are uncertainties with population growth rates and distribution methodology even at 20 years, PS must be assessed with future conditions as it's the demand category that has the largest demands associated with assessed sources. Based on this need, similar scientifically or legally verified methodologies were researched that can either extrapolate BEBR projections or be applied to conduct independent projections for a 40-50 planning horizon.

As an example, the C-51 reservoir project required permittees to conduct long-term demand projections. While the methodology used in the permittees' projections varied across utilities based on their internal demand segmentation and fee-rate projection procedures, the overall approach was to extrapolate population growth rates through a moving average percent difference. This percent difference is then applied to future years until the end of the assessment period.

For the proposed WSWA, a similar extrapolation methodology is suggested to be applied to county populations and then spatially distributed according to current WSP methodology.

PS Growth Rate Assumptions

There are several assumptions and uncertainties embedded within the projections and methodologies, some of which are:

- All the assumptions and uncertainties within BEBR's projection methodologies are carried over into our extrapolation. BEBR's methodology is simplified as follows: $P_t = (H_t \times PP_{Ht}) + GQ_t$, where P_t is the population at time t , H_t is the number of occupied housing units at time t , PP_{Ht} is the average number of persons per household at time t , and GQ_t is the group quarters population at time t . Notably, seasonal residents and undocumented persons are not formally incorporated as part of the permanent population (however their withdrawal rates are likely captured in per-capita use rate). Additionally, birth rates, death rates, national and international migration rates, and other persons factors are simplified within the PP_{Ht} term.
- Spatial distribution of BEBR projections to utility boundary lines are accurate.
- The effects of Covid-19 have intruded additional uncertainties and growth rate extrapolations will not be modified accordingly.
- The significance factor and variability of each of the parameters with BEBR projections carry over to extrapolated numbers.
- The plateau effect of the population projection implies a leveling off of future growth.
- Climate change effects were not incorporated into projection methodologies or distribution.

PS Growth Rate Research

Below are relevant highlights from research conducted to supplement the workgroup's decision-making process.

- BEBR has conducted long-term population projections for the Florida 2070 project.

- Miami-Dade County conducted long-term projections for sewer flows.
- C-51 Reservoir Permit required long-term projections. Methodologies documented were Dania Beach Utilities, Hallandale Beach Utilities, The City of Sunrise, City of Margate, City of Ft Lauderdale, City of Pompano Beach, Miami-Dade Water and Sewer Department. and Broward County.
- State of Oregon conducted long-term projects and found population to be more influential than changes in use types.
- Washington State conducted long-term linear projections.
- Seattle Utilities did population forecast until 2040 and then a linear extrapolation until 2060.
- Thames Water used a cohort-component “industry standard” incorporating population, housing, and occupancy in long-term component and applied a percentage growth rate from government population data.

Agricultural Growth Rates

Figure 24 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.

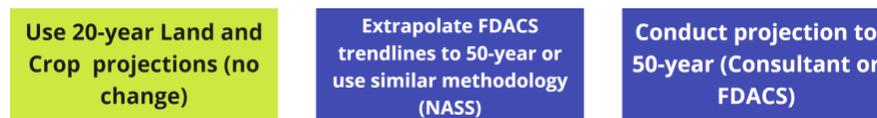


Figure 24. Agricultural growth rate options.

The WSP methodology for projecting agricultural growth is based on the irrigated agriculture growth maps generated by Florida Department of Agriculture and Consumer Services (FDACS) in the Florida Statewide Agricultural Irrigation Demand (FSAID) report. These reports are generated annually and contain parcel-level polygons of statewide agricultural lands (ALG) and agricultural irrigated lands (ILG) including crop type projected out to 25 years. These projections are based on USDA National Agricultural Statistics Service (NASS) using standard trend analysis with data from 1987-2017. County-level trends used an autoregressive procedure where the best functional fit was selected from logarithmic, linear, exponential, and power forms. Crop-type projections and their subsequent withdrawal rates are discussed in the Withdrawal Rates section.

Based on the current use of FSAID AG acreage projections in WSPs, the workgroup recommended use of 20-year growth rate projections rather than extrapolate FSAID trendlines using similar methodology conducted by FDACS to develop future land projections or to conduct new projections with a new methodology. The FSAID growth rates are tied to crop types and acreages and developing new procedures or attempting to project spatially distributed crop types extrapolated from the FSAID report is beyond the scope of the proposed assessment due to high uncertainty. These uncertainties while climatically relevant include elements such as long-term land use changes and future crop type demand which are unreasonable to assume at 50 years.

AG Growth Rate Assumptions

There are several assumptions and uncertainties embedded within projecting Agricultural growth rates using FDACS’s FSAID data, some of which are:

- FSAID geographic land use changes don't consider climate change factors such as the effects of increased drought or the shift from agricultural land to housing due to increased inland migration
- NASS statistics use census and survey information of which data is often voluntary and therefore incomplete.
- Land use change plans rarely exceed 10 – 20 years and therefore projection of potential land use changes beyond even up to 20 years is uncertain.
- Trendlines using various regressions rather than model-based approaches don't capture the reasons behind various changes and can therefore be less encompassing of future changes.
- The Coronavirus pandemic caused various changes that affected land use such as increased Florida migration and lower demand of restaurant produce. Incorporating these and other Covid-19 impacts may change future predictions.

AG Growth Rate Research

Below are relevant highlights from research conducted to supplement the workgroup's decision-making process.

- Oregon used acreages by land use by county, distribution by crop by county, crop specific irrigation demands. Did not project land use changes.

Landscape and Recreation Growth Rates

Figure 25 and Figure 26 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 25. Recreational growth rate options.



Figure 26. Landscape growth rate options.

In the LEC WSP, growth in REC demands were increased proportionally with population growth. However, because golf is a unique use case that accounts for a significant portion of REC demand and is influenced by different parameters than other recreation and landscape uses its growth is segmented from other REC demands and is added on a case-by-cases basis.

Golf growth rates have been minimal or declining in the past decade. As a result, increases in golf are added to a WSP on case-by-case basis where there are water use permits and/or planned growth documenting increases in golf but not projected. The golf industry had been seeing a steady decline until Covid-19 where the trend reversed; however, projecting future growth rates is too uncertain. To allow for the comparison to WSP -- and to balance scope with the additional uncertainties -- it is suggested that the proposed assessment maintain the same 20-year acreages and growth rates determined in the WSP.

REC Growth Rate Assumptions

There are several assumptions and uncertainties embedded in using the WSP current Landscape and Recreational growth rate methodologies, some of which are:

- Landscape growth within the PS utility service area is accounted for with the PS population growth rate, which implies irrigated landscape grows at the same rate as population. This is conservative but unlikely as the average household size in the LEC is increasing and there have been considerably more construction of apartments and multifamily homes than single-family homes, which translates to less lawns per capita.
- The projections are limited to known upcoming water use permits and only 10 years of expected land use changes.
- All parks and other recreation are assumed to grow proportionally to population.
- The effects of climate change will not be incorporated into REC growth. WSP use WUP and known new development to determine new REC locations and manually update associated demands on the WSP 5-year update schedule.

REC Growth Rate Research

Below are relevant highlights from research conducted to supplement the workgroup's decision-making process.

- ASCE found that different plot types (single, multifamily, commercial) have a considerable effect on predictive demand because of increased lawns.
- Municipal and industrial demand growth is most closely associated with population growth.
- Golf courses were on the decline and land use was often switching to housing development but picked back up during the Coronavirus Pandemic so future growth is more uncertain.

Industrial, Commercial, and Institutional Growth Rates

Figure 27 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 27. Industrial, Commercial, and Institutional growth rates options.

ICI is primarily differentiated from other business use cases by it being self-supplied and not sourced from a utility (PS). The largest ICI use cases are from agricultural produce processing and mining and the

majority of ICI growth is associated with mining for increased population. Currently, ICI growth is captured with the addition of known permits and population projections.

If both utility and self-supply Industrial, Commercial, and Institutional users could be segmented then independent growth variables could be associated with each segment and their impact and contribution to withdrawal rates could be more accurately planned. However, due to current data limitations from utilities, segmentation of users is not viable, and creating new data requirements is beyond the scope of this exercise. Additionally, extrapolating the growth rates of self-supplied ICI and applying climate dependent coefficients would likely introduce uncertainty. Therefore, maintaining the existing WSP methodology is suggested for the proposed WSVA assessment.

ICI Growth Rate Assumptions

There are several assumptions and uncertainties embedded within the WSP current ICI growth rate methodologies, some of which are:

- Various ICI uses and growth rates are embedded in PS and are therefore assumed to grow relative to population.
- WSP ICI additions are only done on a case-by-case basis and therefore not projected.
- Climate change considerations and industry influences are not incorporated; however, may have an effect especially as agriculture processing technology improves.

ICI Growth Rate Research

Below are relevant highlights from research conducted to supplement the workgroup’s decision-making process.

- A District economist found a correlation between water supply growth with the mining industry and population growth. This is likely related to the needs for construction materials as population increases.
- London segments water demand and growth rates by business sector and assigns a Gross Value Added as an informant factor in their modeling. This modeling uses individual growth rate coefficients per business sector.

Power Growth Rate

Figure 28 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 28. Power Generation growth options.

Current WSP methodologies incorporate PWR growth in an additive stepwise fashion as PWR demand is primarily associated with cooling requirements for power generating facilities. Additional growth is only incorporated with the development of new power facilities as defined and projected by those facilities in the utility’s 10-year work plans, principally Florida Power & Light. Furthermore, future demand is at least

partially expected to be met by renewable energy such as solar which has few to no water demand requirements.

There is a correlation between increased temperature and household cooling needs which may translate to increased demand on power producing facilities; however, the associated uncertainty is too high.

PWR Growth Rate Assumptions

There are several assumptions and uncertainties embedded within using the WSP current PWR growth methodologies, some of which are:

- Power growth is not projected in the WSP, unless provided by the utility’s 10-year work plans.
- Power growth does include climate related factors.

PWR Growth Rate Research

Below are relevant highlights from research conducted to supplement the workgroup’s decision-making process.

- Many studies show an increase in power consumption needs as the climate warms. This is particularly acute (increase in 25%) for warm tropical climates with cooling needs.
- A study found an increase of 11% in residential air conditioning cooling demand.
- A study found that increased temperatures of cooling water reduce cooling efficiency and thus requires more water. Additionally, increased salinity concentration limits the ability of cooling water to be re-used and may therefore increase water needs.

Domestic Self Supply Growth Rate

Figure 29 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.

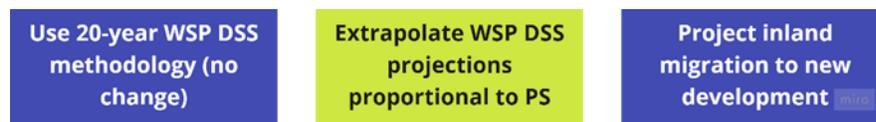


Figure 29. Domestic Self Supply growth options.

DSS projections are developed simultaneously with PS population estimates and projections. Although DSS is defined as self-supplied, often DSS users are within utility boundaries as it may be cheaper for the user to maintain an existing well or drill a new well rather than connecting to the utility. The WSP applies BEBR population growth to DSS. All permanent residents outside of PS utility service area boundaries are considered DSS population. Estimates of DDS population within the utility service area is subtracted from the utility service area population to estimate the utility-served population. In addition, local government plans for providing utility service in current DSS areas are incorporated in the projections, which result in decreases in DSS.

The increase in population is mostly closely associated with urban growth which is supplied by PS; therefore, the growth rates theoretically do not have to be proportional as DSS users may not necessarily be growing at that rate. However, even though the increase in demand may be due to additional urban growth, perhaps the lower cost to develop new DSS and its higher demand rates will end up being

proportional to overall demands caused by population growth. Because of these considerations, maintaining the population trendline increase applied to PS was recommended.

DSS Growth Rate Assumptions

There are several assumptions and uncertainties embedded within the WSP current DSS growth methodologies, some of which are as follows:

- Trends in land use changes are not incorporated
- Population served by PS grows at the rate as DSS
- DSS will not grow or shrink because of climate change impacts (such as drought and potentially lower water tables)

A.2: Water Demands and Withdrawal Rates

The following sections will discuss projecting future water needs as they relate to the growth recommendations highlighted earlier allocating these demands amongst sources. For instance, PS will incorporate an additional 30 years of population projections in its growth rate, and how demand will be distributed to each water source. The term “demand” throughout this section will refer to the withdrawal rate applied to the growth rate for each water use category.

Public Supply Withdrawal Rate

Figure 30 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 30. Public Supply withdrawal rate options.

In the 2018 LEC WSP, existing PS demands were met by the Surficial Aquifer (90%), the Floridan Aquifer (6%) and surface water sources (4%). The utility-specific PCUR is calculated in the WSP by taking the monthly and yearly utility-specific finished water data reported to Florida Department of Environmental Protection (FDEP) and dividing it by the utility’s reported utility-served service area population. The most recent 5 years PCURs are averaged to develop an average utility-based PCUR which is then applied to the utility-served population projections to calculate the projected demand at five-year increments for a 20-year horizon. This is also referred to as the net (finished) demands. Gross (raw) water withdrawals are the volumes needed from the water source(s) to produce the required net (finished) water volumes, considering water treatment process losses. Water use permit allocations for PS utilities are based on the gross (raw) water volume to meet service area demands. To determine gross (raw) water demand for each PS utility, net (finished) water projections were multiplied by raw-to-finished ratios, which are based on the treatment efficiency of each PS water treatment plant. For example, if a typical membrane softening treatment facility withdraws a gross (raw) volume of 10.00 mgd and produces 9.00 mgd of net

(finished) water, its treatment losses are 10%. Therefore, its raw-to-finished ratio would be 1.11 (10 mgd divided by 9 mgd).

Florida Statute specifies that the level of certainty planning goal associated with identifying demands shall be based upon meeting demands during a 1-in-10-year drought event (Section 373.709(2)(a)1., F.S. The increased PS demands during 1-in-10-year drought conditions are calculated using the method described in the Districtwide Water Supply Assessment (SFWMD 1998), which considers the increased demands on the irrigation portion of PS during droughts. The drought demand factors are 1.17 for Martin County, 1.09 for St. Lucie County, and 1.17 for northeastern Okeechobee County (within the UEC Planning Area) and 1.10 for Palm Beach and Broward counties, 1.07 for Miami-Dade County, 1.03 for Monroe County and 1.06 for Hendry County. Average water demands were multiplied by the drought demand factor to calculate demands during 1-in-10-year drought conditions. This demand is modeled with both an average rainfall year and a 1-in-10-year drought.

The average rainfall year is defined as a year having rainfall with a 50 percent probability of being exceeded in any other year and a 1-in-10-year drought is defined as a year in which below normal rainfall occurs with a 90 percent probability of being exceeded in any other year; expected return frequency of once in 10 years.

There are many variables that affect the uncertainties in future drought conditions which are mostly encapsulated in temperature, rainfall, and ET and as such it is suggested that drought be represented in the climate variables rather than as change in the withdrawal rate.

A potential consequence of applying a more conservative modeling approach is increases in water needs may be needed to ensure water supply in drying conditions than current needs, i.e., increased allocations and potentially more frequent water shortage restrictions. This can perhaps be explained by the local and regional nature of drought and the extreme hydrologic differences between various planning scenarios. It is therefore not suggested that for the purpose of the proposed assessment the definition of drought in terms of withdrawal rates be altered without regional consensus or state direction. Additionally, the SFWMD's permitting threshold and planning goal are both established with a 1-in-10-year level of certainty.

PCUR are defined essentially as moving averages and an option to apply an extrapolated version of PCUR is based on the similar extrapolation suggested for PS population growth rates. However, utility based PCUR are affected by many variables whose uncertainties would make it difficult to isolate their trends from their causes. For instance, a decreasing PCUR may be the result of plant treatment or distribution efficiency, increased water conservation, or distributed growth to housing with lower demands, all of which have may have a different management response. Additionally, there exists gaps with current utility service boundary and use rate data. Making additional assumptions and their subsequent uncertainties would not be accurately captured without first developing new utility data standardization procedures which is beyond the scope of this effort. This is further emphasized given that many utilities conduct existing standard conservation plans rather than goal-based plans and may not be looking at or have different methodologies for understanding the causes, effects, and trends of different use categories. As a result, it is not suggested that trends in PCUR be extended beyond the WSP methodology.

Segmenting out climate affected use cases such as landscape irrigation that uses water from a PS utility or various climate affected business sectors can make the vulnerability assessment more robust. This

segmentation would introduce the necessity for data that may not already exist; it would require the development of a new PCUR procedure and may not even have an applicable management consequence beyond the existing additional development of alternative water supplies or increased conservation. For instance, in certain areas, utility permit holders are intentionally limited by their withdrawal's ecological impacts and their ability to provide water for their customers as discussed in Restricted Allocation Area rules (RAA) and WSPs while others are limited by their projected demands. Because of source restrictions (RAAs), many utilities have developed or are planning to develop alternative water supplies beyond their current fresh groundwater allocations and are not planning an increase in permitted surficial aquifer or surface water withdrawals. Conservation is therefore incentivized by the utility to meet the demands limited by existing withdrawal limitations such as the increased costs associated with alternative water supply development or the changing of water supply treatment methodologies to more expensive desalination. Further incentive for alternative water supply development is encouraged through cost-share opportunities and longer permit allocations; for example, most wells using the surficial aquifer must renew their permits every 10 years unless they meet the conditions of assurance, in which case it can be as long as 20 years. As an additional incentive to switch to alternative water sources, wells on the Floridan aquifer must renew their permits at a maximum of every 30 years. However, beyond the incentive and implementation challenges, segmenting out climate use cases may inform the redevelopment of existing rules to ensure continual supply. Due to a lack of comprehensive data, the need for developing new procedures, and the existing limitations already incentivizing resiliency, it is not suggested that climate-related use cases in PWS be segmented.

Withdrawal rates would need to be altered to reflect a potential reduction in treatment efficiencies due to climate change. For instance, if modeling shows sea level rise exacerbating saltwater intrusion, then the treatment efficiencies of coastal utility may decrease, which may result in increased demand on the system. This, however, is not suggested to be included in the proposed assessment as there is not enough research nor clear methodology to adequately predict efficiency decline. Furthermore, utility responses to decreased efficiencies may result in the development of alternative water supply or other management actions that are difficult to model.

Lastly, a regional withdrawal rate could potentially be applied rather than through associated utility withdrawal rates. This idea was based on the concept of understanding vulnerability from a macro perspective with demand needs allocated as decision variables. However, this perspective ignores the reality of the demands caused by existing infrastructure, is extremely difficult to develop, introduces new uncertainties, and removes the ability to provide localized and therefore meaningful outputs. It is therefore not suggested that a regional withdrawal rate be utilized as part of the proposed assessment.

Based on the above discussion it is suggested that the proposed assessment utilize the current WSP approach of applying averaged PCUR determined for the 20/25-year WSP and then applying them to increased growth associated with future conditions. Additionally, utilizing the current approach would require fewer additional model runs and less time needed to analyze and develop a new methodology. Additionally, drought uncertainties would not be ignored but rather included in changing temperature, rainfall, and ET patterns.

PS Withdrawal Rate Assumptions

There are several assumptions and uncertainties embedded within using the WSP current PS withdrawal rate, some of which are as follows:

- PCUR includes households, landscape, and business uses in addition to losses and distributions efficiency. Many of these categories contain various climate affected use cases which are all included in the PCUR, increasing it uncertainty.
- Drought conditions are captured in 1-in-10 scenario runs. Increased drought uncertainties due to climate change are incorporated in temperature, rainfall, and ET changes. Future demand beyond RAA limits is assumed to be met by alternative water supply or conservation i.e., modeling will limit demands at RAA withdrawal limits.
- There are no econometric variables associated with growth or demand beyond those included in population projections.
-

PS Withdrawal Rate Research

Below are relevant research highlights.

- Seattle public withdrawal rates used price and other econometric variables.
- Washington State used and extrapolated per capita consumption withdrawal rate to 2075.
- Oregon uses a standardized data collection from providers and segments and applies different methodologies to various zones based on their expected growth.
- See research highlighted in PWS Growth Rate

Agricultural Withdrawal Rate

Figure 31 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 31. Agricultural demand options.

In the 2018 LEC WSP, existing Agricultural (AG) demands were met by surface water sources (80%) and the Surficial Aquifer (20%). The AG water withdrawal rate is determined in the WSP using the Agricultural Field Scale Irrigation Requirements Simulation (AFSIRS) model (Smajstrla 1990). The FDACS irrigated crop acres, soil types, growing seasons, and irrigation methods are used as input data for the AFSIRS model. AG withdrawal rate estimates and projections are based on the typical commercially grown crop categories developed by the FDEP and water management districts for use in water supply plans. The demands of these crops are then calculated for an average rainfall year and a 1-in-10-year drought. AFSIRS considers the parameters featured in the Figure 32 and illustrated in Figure 33.

Climate	Crop Data	Irrigation Efficiency	Soil Data	Land Use Data	Runoff
Daily Rainfall (NEXRAD)	Crop types [16 perennial (sugarcane, citrus, turf, etc) and 44 annual (vegetables)]	10 irrigation systems	773 detailed soil types by SCS (SSURGO)	Based on the ILG parcels	Runoff Curve Number (TR55, USDA)
Reference ET (RET) (USGS)	Crop coefficients (standard)	Percent irrigation efficiency	7 Generic Hydrologic Soil Groups (HSG)	Florida Land Use Cover Classification System (FLUCCS) Codes	
	Extinction depth/root zone depths (standard, crop based)	Percent area of soil surface irrigated	Infiltration: A - High, B - Moderate, C - Slow, D - Very Slow	Conversion table from FSAID ILG to AFSIRS detailed level crop codes	
	Growing seasons (for annual crops)	Percent fraction of ET from irrigated portion of crop root zone		at general use code level the categories crosswalk is direct 1 to 1	

Figure 32. AFSIRS parameters and data sources.

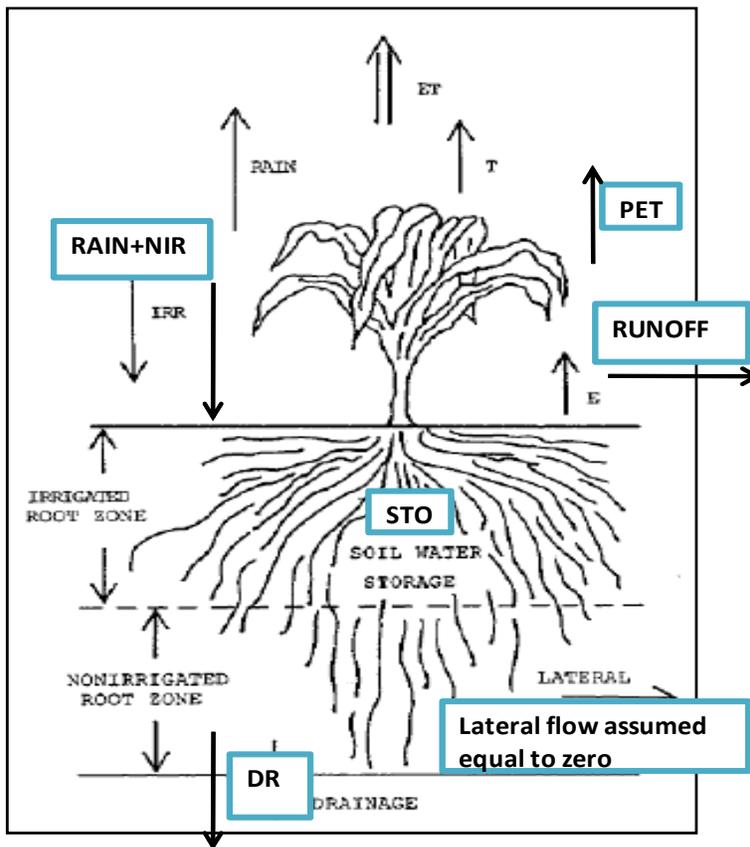


Figure 33. Illustration of parameters reflected in AFSIRS.

Within AFSIRS there are many parameters (beyond the growth rate parameters) that will be affected by climate change. For instance, climate change may cause soil to dry out, which can affect its storativity, transmissivity, and discharge characteristics. This change has a very influential effect both in practice and in modeling on the infiltration and recharge and will therefore the effect the demand and supply of availability sources. However, these effects and consequences of these changes are hard to anticipate. For example, if soils dry out then as infiltration rates increase so too does the irrigation demand, which can increase the agricultural production costs and may result in a change of crop type. Therefore, it is not suggested that new models or additional parameter changes be applied to the proposed assessment due to the increased response uncertainty.

The FSAID 7, 8, and 9 reports highlight a few of the potential effects of how climate change may impact agricultural demand; however, these effects are not included in the final estimates and are therefore not suggested to be applied to the proposed assessment.

It is suggested that 50-year temperature, rainfall, and ET conditions at be applied to AFSIRS (See red boxes in Figure 32) and applied to 20-year acreages and expected crop types provided by FDACS. This reduces the need for additional model runs, eliminates the time needed to develop a new methodology, and provides a means for comparison to WSP model runs.

AG Withdrawal Rate Assumptions

There are several assumptions and uncertainties embedded within using AFSIRS as the AG withdrawal rate, some of which are as follows:

- All the assumptions represented in AFSIRS model and FDAC acreage and crop type are embedded.
- Climate change will not be reflected in the following AFSIRS input categories: crop data, Irrigation efficiency, soil data, land use data and runoff curve numbers.
- Climate changes will only be reflected in temperature, rainfall, and ET rates.

AG Demand Research

Below are relevant highlights from research conducted to supplement the workgroup's decision-making process.

- FSAID 7, 8, and 9 reports conducted future demand with climate change scenarios of Representative Concentration Pathway 4.5 and 8.5 and looked at the following: changes in ETo, rainfall, temperature, warm night (effects ET), frost freezes, intensification of hydrologic cycle, shorter cold season.
- Oregon's major demand assumption are the following: not to project crop differences, crops are irrigated properly, existing and future shortages were not considered, losses are in efficiency rate at 80% conveyance and 66% in application. Important conclusion factors: Early spring may affect specific crops, higher ET means higher consumption and demand, increased demands are expected to outpace increase precipitation even in wetter scenarios.
- Irrigation withdrawal is likely to increase because of climate change effects on agriculture produced in Middle America. This withdrawal is associated with increase temperature and will outpace the expected increase in precipitation.
- Ghait et al. does a thorough review of various ET models that can be applied to crops. Additionally, there are several alternate withdrawal rate methodologies that can be applied.

Landscape and Recreation Withdrawal Rate

Figure 34 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 34. Landscape and Recreation demand options.

In the 2018 LEC WSP, existing Landscape and Recreation (REC) demands were met by various surface water sources (39%), the Surficial Aquifer (32%), Reclaimed Water (27%), and the Floridan Aquifer (2%). REC demands are calculated only for areas with water use permits issued by the SFWMD. In 2018 REC withdrawal rates were calculated using AFSIRS for areas supplied by surface water sources, and the Surficial and Floridan Aquifers and using quantities submitted to the FDEP for areas supplied by reclaimed water. The 2023 withdrawal rates will use rates determined from annual water use reports. The exact methodology is still under development but will likely follow a similar approach to PS.

There are three types of irrigated landscaped areas outside of those permitted by the SFWMD that are excluded from the REC demands. The first type includes landscaped areas irrigated with potable water provided by PS utilities, which are accounted for under PS estimates and projections. The second type is irrigated single-family or duplex residential landscaped areas served by individual residential wells permitted by rule [Rule 40E-2.061, F.A.C.] or local stormwater pond, ditch, or canal rather than with an individual water use permit. Demands associated with these small, residential wells and surface water withdrawals are not quantified as part of the WSPs due to the lack of water use and acreage data. The third type of irrigated landscaped areas are those served with reclaimed water that do not require a water use permit. This usually occurs where reclaimed water is used directly from a pressurized pipeline or delivered into a lined or unlined lakes.

The vulnerability assessment will be conducted using only what can be incorporated into and simulated with the groundwater model. Therefore, it is suggested that future climate conditions be applied to the spatial data from REC acreages in WUPs. It should be noted that these demands will have growth rates based on the population growth rates.

REC Demand Assumptions

There are several assumptions and uncertainties embedded with using AFSIRS on spatially distributed REC demands, some of which are as follows:

- Irrigation demands embedded within PS PCUR don't incorporate climate change withdrawal rate changes.
- Irrigation demands without spatial components will not be included and may account for a significant portion of the total demand.
- Irrigation demands associated with small residential wells and those supported by reclaimed water will not be included as they are not directly incorporated into the groundwater model. Application of reclaimed water will be incorporated in the model simulations.
- Locations associated with a WUP will be based on population growth rates to 2075.

REC Demand Research

Below are relevant highlights from research conducted to supplement the workgroup’s decision-making process.

- ASCE found that different plot types (single, multifamily, commercial) have a considerable effect on predictive demand because of increased lawns.
- “The effect of climate change on municipal and industrial water demand could be estimated through the evaluation of how the range of potential future climates would affect outdoor demands.”
- “Results show that groundwater pumping and recharge both will increase and that the effects of groundwater pumping will overshadow those from natural fluctuations. Groundwater levels will decline more in areas with irrigation-driven decreasing trends in the baseline.”

Industrial, Commercial, and Institutional Withdrawal Rate

Figure 35 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 35. Industrial, Commercial, and Institutional demand options.

In the 2018 LEC WSP, existing ICI demands were met by the surficial aquifer (38%), reclaimed water (35%), and various surface water sources (27%). Recirculated water used in closed-loop geothermal heating and cooling systems is not included in demand calculations. ICI projections assume demands for average rainfall years and 1-in-10-year drought conditions are the same and withdrawal demand is equal to user demand (no losses are assumed). The withdrawal rate for mining is connected to population growth and future demands are calculated accordingly.

Agriculturally focused ICI withdrawal rates such as those related to fruit cleaning will likely have impacts because of climate change; however, those impacts are too unpredictable and uncertain. For example, changes in withdrawal rates based on increasing processing efficiency will likely be inconsequential compared to those based on crop changes because of climate. Additionally, given that no additional business use cases are suggested to be segmented out and that drought conditions are accounted for in future climate conditions, it is suggested that the proposed assessment not deviate from the current WSP methodology.

ICI Withdrawal Rate Assumptions

There are several assumptions and uncertainties embedded within using existing WSP ICI withdrawal rate methodology, some of which are as follows:

- ICI withdrawal rate will not change because of climate change
- Demand rate associated with agricultural processing of different crop types and reductions to crop yield are not incorporated

- ICI demands include only those defined by the WSP and not business use cases incorporated into PS
- Future improvements to processing efficiency will not be incorporated
- ICI mining withdrawal rates will be applied to future population growth

Power Withdrawal Rate

Figure 36 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.



Figure 36. Power withdrawal rate options.

In the 2018 LEC WSP, existing Power (PWR) demands were met by Reclaimed Water (69%) and the Floridan Aquifer (31%). PWR demands do not include the use of brackish surface water and cooling water returned to its withdrawal source, or seawater. Demands under average rainfall and 1-in-10-year drought conditions are assumed to be equal for the PWR category, and no distinction is made between net and gross water demands. Baseline demands are estimated using utility-required reported water use. Additional demands are added on a case-by-case basis and projecting future demand based on climate change is not feasible. Additionally, increased power generation will likely be the result of renewables that require less demand such as solar power. Therefore, it is suggested that the proposed assessment apply existing WSP methodologies.

- Power water supply withdrawal rates will not include the effects of climate change

Domestic Self Supply Withdrawal Rate

Figure 37 shows the options presented to the workgroup based on research of the latest scientific methodology and strategies implemented by similar agencies.

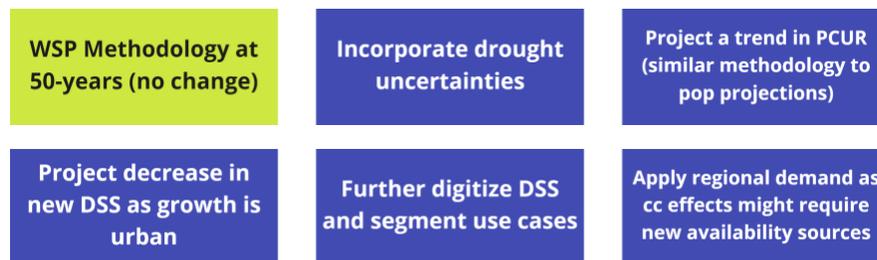


Figure 37. Domestic Self Supply withdrawal rate options.

Domestic Self Supply (DSS) demand accounts for 1% of total water supply demands in the LEC. It is delineated in the WSP as potable water used by households served by small utilities (less than 0.10 mgd) or self-supplied by private wells. The WSP applied the same PCUR to both PS and DSS. It is suggested that the same methodology used in WSP be applied to DSS in the proposed assessment. (See discussion in PS Growth Rate and Withdrawal Rate and DSS Growth Rate)

All PS PCUR assumptions apply.



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